



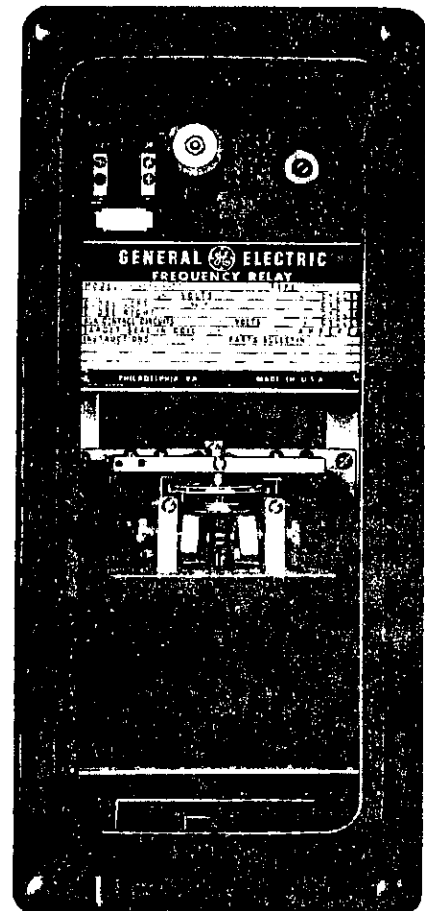
INSTRUCTIONS

GEK-27863

FREQUENCY RELAYS

TYPES

CFF12A47 & UP
CFF12C13 & UP
CFF12E3 & UP
CFF12F1 & UP



POWER SYSTEMS MANAGEMENT DEPARTMENT

GENERAL  ELECTRIC

PHILADELPHIA, PA.

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FREQUENCY RELAYS

TYPE CFF

INTRODUCTION

The CFF12 relays covered by this instruction book are underfrequency devices. All of the relays contain a high speed induction cup unit as the frequency sensing element, but include a six cycle time delay telephone type auxiliary relay.

The frequency sensing unit has both normally open and normally closed contacts. The normally open contact will close on underfrequency to energize the auxiliary relay which will seal-in around the contact that picked it up. When the system returns to normal, the auxiliary relay will be reset by the normally closed contact of the frequency sensing unit.

The CFF12A, CFF12E and the CFF12F use D-C to operate the auxiliary relay and the target seal-in unit. The CFF12C is designed so that all of the auxiliary components function from the same A-C supply that activates the frequency sensing unit.

The relays are contained in the medium size, M-1, drawout case.

Some of the relay models are equipped with zener diodes to improve the operating frequency vs. voltage characteristic.

The following models do not have these zeners:

12CFF12A47A through 12CFF12A60A
12CFF12C13A and 12CFF12C14A
12CFF12E3A and 12CFF12E4A
12CFF12F1A

Those models which are equipped with zeners are:

12CFF12A61A and up
12CFF12C15A and up

APPLICATION

The Type CFF underfrequency relays are applied where high speed detection of underfrequency conditions is required. Specifically they are applied in underfrequency load conservation schemes. If a system disturbance results in some loss of generating capacity such that the load exceeds the generation, the system is in danger of collapse. The underfrequency relay operates to disconnect non-essential load in order to balance load and generation in the affected area. Such action must be taken promptly and must be sufficient magnitude to conserve essential load and enable the rest of the system to recover from the underfrequency condition. By preventing a major shutdown, restoration of the entire system to normal operation is greatly facilitated and expedited.

The six cycle auxiliary time delay unit provides security against misoperation due to mechanical shock or the electrical transients which result from switching potentials to the relay or clearing a fault on the system.

Another application of the underfrequency relay is at industrial plants where it is necessary to trip the incoming breaker at the plant when the power company supply is tripped off. This will prevent damage to motors or local generation in the plant that could otherwise be incurred if the plant breaker were still closed when the power company automatically reclosed the supply line to the plant.

An overall load conservation scheme can be arranged to trip off non-essential or interruptible load as follows:

These instructions do not purport to cover all details or variations in equipment nor to provide for every possible contingency to be met in connection with installation, operation or maintenance. Should further information be desired or should particular problems arise which are not covered sufficiently for the purchaser's purposes, the matter should be referred to the General Electric Company.

- a. Trip off blocks of load in several steps with several relays set at successively lower frequency values.
- b. Trip off blocks of load in several steps on a time basis at one level of frequency, so that as each time step is reached additional load is dropped.
- c. A combination of a and b above.

A tapped subtransmission or distribution substation which has a heavy preponderance of motor load may require special consideration for proper time coordination. If the transmission sources to such a substation were tripped out for any reason, the motor loads would tend to maintain the voltage for a short time while the frequency decreased as the motors were slowing down. It will be necessary to delay the tripping of the underfrequency relay for 15 or more cycles to ride over this condition and avoid tripping breakers needlessly. The type CFF22 relays have a longer time delay feature, ranging from 6 to 60 cycles continuously adjustable.

In applying the underfrequency relay in a system load conservation program, it must be recognized that a low frequency condition does not begin to be corrected until a circuit breaker operation occurs to disconnect some load. The family of curves shown in Fig. 1 are constructed to show frequency vs. time to open the breaker after the disturbance starts for a number of different rates of change of frequency. These curves include:

1. An allowance of six cycles for total breaker clearing time.
2. The frequency relay minimum delay of six cycles.
3. Various frequency pickup settings on the relay.

If any of these factors change, then a new curve should be plotted. The curve can be read directly to determine the system frequency at which the load is actually removed.

Typical external connection diagrams are shown in Figs. 2,3, and Fig. 4.

RATINGS

INDUCTION CUP UNIT

The calibration of this unit is continuously adjustable from rated frequency down to 56 Hz, however, for reasons that will be explained under OPERATING CHARACTERISTICS, underfrequency settings higher than 59.5 Hz should not be used.

The calibration is under the control of a fixed resistor with taps, and a rheostat. Sections of the fixed resistor may be inserted in the circuit when the full value of the rheostat will not lower the operating frequency to the desired value.

The contacts of this unit require no specific rating since they in their function have the capacity to carry the currents called for by the auxiliary relay circuits.

AUXILIARY RELAY A

The coil circuit voltage ratings are on a continuous basis.

The contacts can carry three amperes continuously or 30 amperes for two seconds.

The current interrupting capabilities for either A-C or D-C are shown in Table A.

TABLE A

VOLTS	INDUCTIVE (*)	NON-INDUCTIVE
115 A-C	0.75 amps	2.0 amps
230 A-C	0.5 amps	1.5 amps
48 D-C	1.0 amps	3.0 amps
125 D-C	0.5 amps	1.5 amps
250 D-C	0.25 amps	1.0 amps

* Inductance based on average trip coil

TARGET AND SEAL-IN UNIT

The coil circuit of these assemblies when used in an A-C control circuit, such as the CFF12C, are also on a continuous voltage basis, equal to the voltage rating of the relay.

The D-C control circuits, however, normally use coils with current ratings as shown in Table B.

The contacts in either the A-C or D-C ratings are alike and have a capability of closing 30 amperes for tripping duty.

TABLE B

TARGET SEAL-IN COIL RATINGS		
Conditions	Nominal Tap Rating (Amps)	
	0.2	2.0
Continuous Rating	0.3 Amps	3.5 Amps
DC Resistance	7.0 Ohms	0.13 Ohms
Tripping Duty	5.0 Amps	30.0 Amps

BURDENS

The underfrequency settings on the CFF relays affect the burden imposed on the potential transformer. The maximum burden occurs at 59.5 Hz. The operating frequency is lowered by adding more resistance in the calibration control circuit, hence, the burden is reduced with lower frequency settings.

The burden of the CFF12C relay is greater than the CFF12A, CFF12E and CFF12F, because its auxiliary relay and target unit are A-C operated.

The maximum burden for the type CFF relays are listed in Table C.

TABLE C

TOTAL 60 HZ BURDENS				
RELAY TYPE	VOLTAGE RATING	CALIBRATION HZ	WATTS	VOLT AMPERE
CFF12A CFF12E CFF12F	115 AND 230	59.5	9.8	12.4
CFF12C	115 AND 230	59.5	15.3	21.5

CHARACTERISTICS

OPERATING PRINCIPLES

The frequency sensing unit is an eight pole induction cup assembly that responds to the magnitude and phase angle of the fluxes produced by the two sets of coil circuits each occupying 4 of the poles.

When the fluxes are in phase, the unit exhibits zero torque. Under normal conditions of rated voltage and frequency, the phase-displacement between the flux of one circuit with respect to the other produces torque to hold the lefthand (F.V.) contacts open. When an underfrequency condition appears, approaching the calibration frequency, the phase angle first decreases to zero, leaving only spring torque to hold the contact open. As the frequency continues to fall a phase displacement again appears this time to produce contact closing torque. When the frequency reaches the calibrated underfrequency setting, the magnitude of electrical torque is sufficient to overcome the control spring torque closing the left hand contact. The closing of this contact operates the six cycle time delay auxiliary relay called "A" in a so called "PICK UP AND KNOCK DOWN" circuit, that is "A" PICKS UP and seals around the contact that picked it up. The operation of "A" activates the target seal-in unit or the target auxiliary, in the case of the CFF12C, if the underfrequency condition persists longer than the six cycle time delay. Should the frequency restore to normal before the prescribed time delay expires, the right hand contact of the sensing unit will close shorting out relay "A" causing it to drop out to normalize the circuit for the next underfrequency condition.

The CFF relays operate to close their contacts when the applied source frequency is below the preset value. An operating frequency vs. voltage characteristic is shown in Fig. 5. The characteristics are shown with and without the use of zeners in one of the coil circuits. Fig. 6 is also a frequency vs. voltage characteristic combined with ambient temperatures as is Fig. 7, the latter characteristics are with relays equipped with zeners.

Fig. 8 is a so called "COLD PICKUP" characteristic. This characteristic endeavors to show the change in calibration on a relay de-energized for time long enough to have all its components return to the ambient temperatures indicated. The operating frequency at the first instant power is reapplied to the relay will be higher as shown by the curve, hence, there is the danger of a false trip in setting the calibration to close to the power system frequency.

CONSTRUCTION

The CFF12 frequency sensing unit (see Fig. 9) houses a cup and shaft assembly that carries the moving contact. This assembly is supported on the bottom by a non-magnetic and rust proof pivot resting on a synthetic spring mounted jewel bearing. The compression spring acts to prevent jewel damage should the moving system be subjected to mechanical shock. At the upper end of the shaft, a stainless steel guide pin rides in a polished bronze bushing assembly. This top bearing serves to keep the cup and shaft assembly properly aligned in the unit as well as controlling the desired end play.

The moving contact assembly is a molded hub, that supports the contacts and a spiral spring. The spiral spring assembly is affixed to an adjustable metal ring, which sets directly above the control spring. The ring, after adjustment may be locked in position in its molded assembly by a hex stud located directly behind the upper pivot.

Barrel type stationary contact assemblies are located on either side of the moving contact. These stationary contacts house a silver contact mounted on a flexible bronze disc which provides for the desired amount of wiping action. The assembly also houses a steel ball that rests against a metal disc, directly behind the contact. The presence of the ball minimizes contact bounce should torque levels exceed the forces to totally compress the flexible contact spring. The stationary contacts are held in position by a screw which holds the barrels secure in the contact support. The entire barrel may be removed by loosening the clamping screw.

The target-seal-in unit is located at the upper left hand side of the relay. It consists of a hinged armature type of assembly operated by either a voltage or current coil depending upon the rating of the relay. The operation of the relay caused the armature and its contact to complete the trip circuit and also to expose the target. The target is reset by a rod assembly located at the lower left hand corner of the cover.

Rheostat R-2 or RH-A are mounted to the right of the target seal-in units. The fixed resistor R-3 or in the case of the CFF12C relays, have leads which may be positioned to select any section of its resistance and is located in the rear of the relay.

These components are identified in the photographs shown in Figs. 11, 12, and 13.

The case is suitable for either surface or semi-flush panel mounting and an assortment of hardware is provided for either mounting. The cover attaches to the case and also carries the reset mechanism. Each cover screw has provision for a sealing wire.

The case has studs or screw connections at the bottom for the external connections. The electrical connections between the relay unit and the case studs are made through spring backed contact fingers mounted in the stationary molded inner and outer blocks between which nests a removable connecting plug which completes the circuits. The outer blocks, attached to the case, carries the studs for the external connections and the inner block carries terminals for the internal connections.

The relay mechanism is mounted in a steel framework called the cradle and is a complete unit with all leads being terminated at the inner block. This cradle is held firmly in the case with a latch at the top and the bottom and by a guide pin at the back of the case. The case and cradle are so constructed that the relay cannot be inserted in the case upside down. The connecting plug, besides making the electrical connections between the blocks of the cradle and case, also locks the latch in place. The cover, which is fastened to the case by thumbscrews, holds the connecting plug in place.

To draw out the relay unit the cover is first removed, and the plug pulled out. The latches are then released, and the relay can be easily drawn out. To replace the relay, the reverse order is followed.

A separate testing plug can be inserted instead of the connecting plug to test the relay in place on the panel either from its own source of voltage, or from other sources. Or, the relay can be drawn out and replaced by another which has been tested in the laboratory.

RECEIVING, HANDLING AND STORAGE

These relays, when not included as a part of a control panel, will be shipped in cartons designed to protect them against damage. Immediately upon receipt of a relay, examine it for any damage sustained in transit. If injury or damage resulting from rough handling is evident, file a damage claim at once with the transportation company and promptly notify the nearest General Electric Apparatus Sales Office.

Reasonable care should be exercised in unpacking the relay in order that none of the parts are injured or the adjustments disturbed.

If the relays are not to be installed immediately, they should be stored in their original cartons in a place that is free from moisture, dust and metallic chips. Foreign matter collected on the outside of the case may find its way inside when the cover is removed and cause trouble in the operation of the relay.

ACCEPTANCE TESTS

The following are recommended mechanical checks to insure that the relay is in proper working order.

THE INDUCTION CUP UNIT

The moving contact assembly should be resting against the right hand stationary contact. The contact gap should be approximately 1/16 inch. Each full turn of the contact barrel alters its position by 1/32 of an inch, hence, serves as a convenient means to check or set the contact gap.

The cup-shaft end play has been set to be between 0.015 inches and 0.020 inches. If resetting is necessary, keep the end play within these limits.

Check to see that there is some contact deflection or wipe in the flexible stationary contact. The deflection is in the order of the 0.005 inches to 0.010 inches.

TARGET SEAL-IN UNIT

Operate the armature by hand and note that the bridging contacts make at about the same time with some wiping action before the armature comes to rest against the pole piece. During this operation the target should come into view and latch in before the total travel is exhausted. The reset lever should reset the target.

AUXILIARY TELEPHONE RELAYS "A"

All normally open contacts should have a contact gap of at least 0.010 inches.

Operate the closing armature by hand and note that the closing contact make and deflect at least 0.005 inches before the end of the armature travel.

FREQUENCY CONTROL RHEOSTATS AND SLIDE BAND RESISTORS

The locking nuts for these resistors must be tight.

The following are the general procedures for checking the relay electrically:

TARGET SEAL-IN UNITS

The unit used in the relays with D-C ratings are current operated devices, rated 0.2/2.0 amperes. These seal-in units should pick up at a value equal to or less than the tap rating. Upon picking up, the contacts should wipe fully, and the target should drop. Both tap ratings should be checked. In the process of transferring to the other tap, do not remove the screw from the tap being used first, rather, remove one of the screws from the opposite stationary contact and insert this in the other current tap. Then replace it with the screw used in the first test tap. This procedure keeps the stationary contacts in their original position thereby preserving proper contact alignment.

The unit used in the Model 12CFF12C relays is an A.C. voltage operated device. The pickup voltage of this unit should be 70% or less than the voltage rating.

AUXILIARY UNIT "A"

These relays are voltage operated devices and should pick up at 70% or less than the control circuit voltage rating.

THE INDUCTION CUP UNIT

This frequency sensing unit has been calibrated at the factory to close its trip contact at the frequency stamped on the nameplate.

To check this value apply rated voltage and frequency to the relay as indicated in the Test Diagrams Fig. 13 and Fig. 14.

Permit the relay to heat up for at least one hour with rated voltage and frequency to stabilize the calibration before checking the operating frequency.

In the process of checking or setting the calibration of these relays, be sure that the relay is resting in a level position, i.e. as it will be when mounted on a relay panel.

The frequency setting of the unit is under the control of the rheostat R-2 and the tapped resistor R-3 for all models other than the 12CFF12C. The latter permits additional resistance to be added to the circuit as required, since resistance of R-2 is not sufficient to cover the rated range of frequency settings. In the CFF12C relays there is an additional slide band resistor called RA that works in conjunction with the rheostat called RH-A. The settings are made by placing the rheostat in a mid-position. The calibration is set to approximately the desired frequency by means of the slide band resistor, plus the fixed resistor R-4 if necessary. The calibration may then be set to the desired value by the rheostat. Carefully tighten the slide band and the lock nut on these units and recheck the calibration to be sure it has not changed during these tightening operations.

The test procedure for resetting the calibration should be as follows:

In this case it is assumed that the relay has not been energized for some time, hence, all its components are at room temperature.

1. Set leads on the tapped resistor for zero resistance.
2. Set R-2 or RH-A in its mid-position.
3. Apply rated voltage and frequency for about 10 minutes, then set the calibration to within ± 0.1 Hz of the required setting. This preliminary setting will place the calibration control resistance near its final value during the self heating period.

4. Permit the relay to self heat for at least one hour at rated voltage and frequency, then finalize the calibration to the desired value within ± 0.02 Hz, and lock the rheostat.
5. Check the operating value at other voltage levels.
 - a. The operating frequency on relays without zeners should not fall more than 0.3 Hz at 80 volts. If it does, reduce the control spring setting to just reach this level. The control spring wind-up must be great enough to be sure that the right hand contact will close when no power is applied to the relay, hence, do not weaken it more than necessary.
 - b. On relays that use zeners, check the operating frequency down to 60 volts in about 15 volt steps, to determine the flatness of the characteristic. With a minimum wind-up of the control spring the operating frequency will rise as the voltage is reduced due to the zeners. Increasing the control spring tends to flatter the curve. In general, making the 60 volt setting close to the rated voltage should yield a characteristic within $+0.05$ to -0.1 Hz from 60 to rated volts.

The control spring settings at 59 Hz calibration will be greater than at 57 Hz, hence, it is advisable to shoot this voltage characteristic if frequency changes in the order of 0.5 Hz or more is planned to keep the variation of the operating frequency with respect to voltage to a minimum.

INSTALLATION

LOCATION

The location should be clean and dry, free from dust and excessive vibration, and well lighted to facilitate inspection and testing.

MOUNTING

The relay should be mounted on a vertical surface. The outline and panel drilling for either surface or semiflush panel mounting is shown in Fig. 22.

One of the mounting studs or screws should be permanently grounded by a conductor not less than No. 12 B&S gage copper wire or its equivalent.

CONNECTIONS

Internal connection diagrams for the relays are shown in Figs. 15 to 21 inclusive.

ADJUSTMENTS

The relays are calibrated at the factory and should not require any further adjustment. If it is desirable to check the frequency characteristic, follow the procedure outline under MAINTENANCE.

INSPECTION

At the time of installation, the relay should be inspected for tarnished contacts, loose screws, or other imperfections. If any trouble is found, it should be corrected in the manner described under MAINTENANCE.

MAINTENANCE

The relays are adjusted at the factory, and it is advisable not to disturb the adjustments. If for any reason they have been disturbed, the following points should be observed in restoring them.

SHAFT AND BEARINGS

The lower jewel screw can be removed from the unit by means of an offset screw driver or an end wrench. The jewel may be tested for cracks by exploring its surface with the point of a fine needle.

The lower jewel bearing should be screwed all the way in until its head engages the end of the threaded core. The upper bearing should be adjusted to allow about 1/64 inch end play of the shaft.

To check the clearance between the iron core and the inside of the rotor cup, press down on the contact arm near the shaft, and thereby depress the spring mounted jewel until the cup strikes the iron. The shaft and cup should move about 1/6 inch.

CUP AND STATOR

If it is necessary to remove the rotor from the unit, the following procedure should be followed.

The leads should first be removed from the contact structure and tagged for identification in reconnecting. Then remove the three flat head screws which fasten the unit to the mounting plate from the back. Tilt the stator forward and remove the four corner screws which hold the contact head to the stator. The entire top structure with the rotor can then be lifted away from the stator to give access to the assembly. Care should be taken not to strain the leads entering the back of the stator. Unless there is reason for removing the stator from the cradle, these leads need not be disconnected.

To remove the shaft and rotor from the contact head assembly, the spring clip at the top of the shaft must be pulled out, and the clutch adjusting screw and spring taken out of the molded contact arm.

The rotor should be handled carefully while it is out of the unit, and the stator should be protected to keep it free from dust or metallic particles.

In reassembly, the rotor will fit into the air gap easily if the parts are held in proper alignment.

CONTACT CLEANING

For cleaning fine silver contacts, a flexible burnishing tool should be used. This consists of a flexible strip of metal with an etched roughened surface, resembling in effect a superfine file. The polishing action is so delicate that no scratches are left, yet corroded material will be removed rapidly and thoroughly. The flexibility of the tool insures the cleaning of the actual points of contact.

Fine silver contacts should not be cleaned with knives, files, or abrasive paper or cloth. Knives or files may leave scratches which increase arcing and deterioration of the contacts. Abrasive paper or cloth may leave minute particles of insulating abrasive material in the contacts and thus prevent closing.

The burnishing tool described is included in the standard relay tool kit obtainable from the factory.

CONTACT ADJUSTMENT

Should it be necessary to change the stationary contact mounting spring, remove the contact barrel and sleeve as a complete unit after loosening the screw at the front of the contact block. Unscrew the cap. The contact and spring may then be removed.

The moving contact may be removed by loosening the screw which secures it to the contact arm and sliding it from under the screw head.

The contact gap may be adjusted by slightly loosening the screw at the front of the contact block. It should be loose enough only to allow the contact barrel to rotate in its sleeve.

The right contact should hold the moving contact arm in a neutral position, i.e., with it pointing directly forward. Bring the left stationary contact up until it just touches the moving contact by rotating the barrel. Then back it away two full turns to obtain 1/16 inch contact gap. Tighten the screws which secure the contact barrels.

CLUTCH ADJUSTMENT

If for any reason the moving contact arm has been removed or loosened from the rotor shaft, it will be necessary to reset the clutch. The screw on the side of the contact arm should be tightened to bottom of the internal compression spring, then back off two full turns and with locknut secure.

CALIBRATION PROCEDURE

Refer to section under ACCEPTANCE TESTS.

PERIODIC TESTING

An operational test and inspection of the relay at intervals of six months is recommended. The calibration need not be checked, but operation of the auxiliary circuits should be tested.

In testing relay Types CFF using D-C auxiliary units an adjustable resistor should be substituted for the breaker trip coil. It should be set to draw current equal to 95 per cent of tap setting of the target seal-in unit. When testing relay Types CFF12C an indicating lamp should be used in place of the breaker trip coil.

To check operation of the auxiliary circuits follow the sequence tabulated on Table - D

TABLE - D

RELAY	OPERATE SUCCESSIVELY BY HAND			
	1. Close Left Contacts	2. Open Left Contacts	3. Close Right Contacts	4. Open Trip Circuit
	RESULT			
CFF12A, 12E and 12F	Telephone relay picks up, target seal-in picks up, trip current flows	No Action	Telephone relays drop out.	Target seal-in drops out. Target remains exposed.
CFF12C	Telephone relay picks up, target and auxiliary relay picks up, indicating lamp lights.	No Action	Telephone relay drops out, target and auxiliary relay drops out, target remains exposed indicating lamp extinguishes.	No Action

RENEWAL PARTS

It is recommended that sufficient quantities of renewal parts be carried in stock to enable the prompt replacement of any that are worn, broken, or damaged.

When ordering renewal parts, address the nearest Sales Office of the General Electric Company, specify quantity required, name of part wanted, and give complete nameplate data of the relay. If possible, give the General Electric Company requisition number on which the relay was furnished.

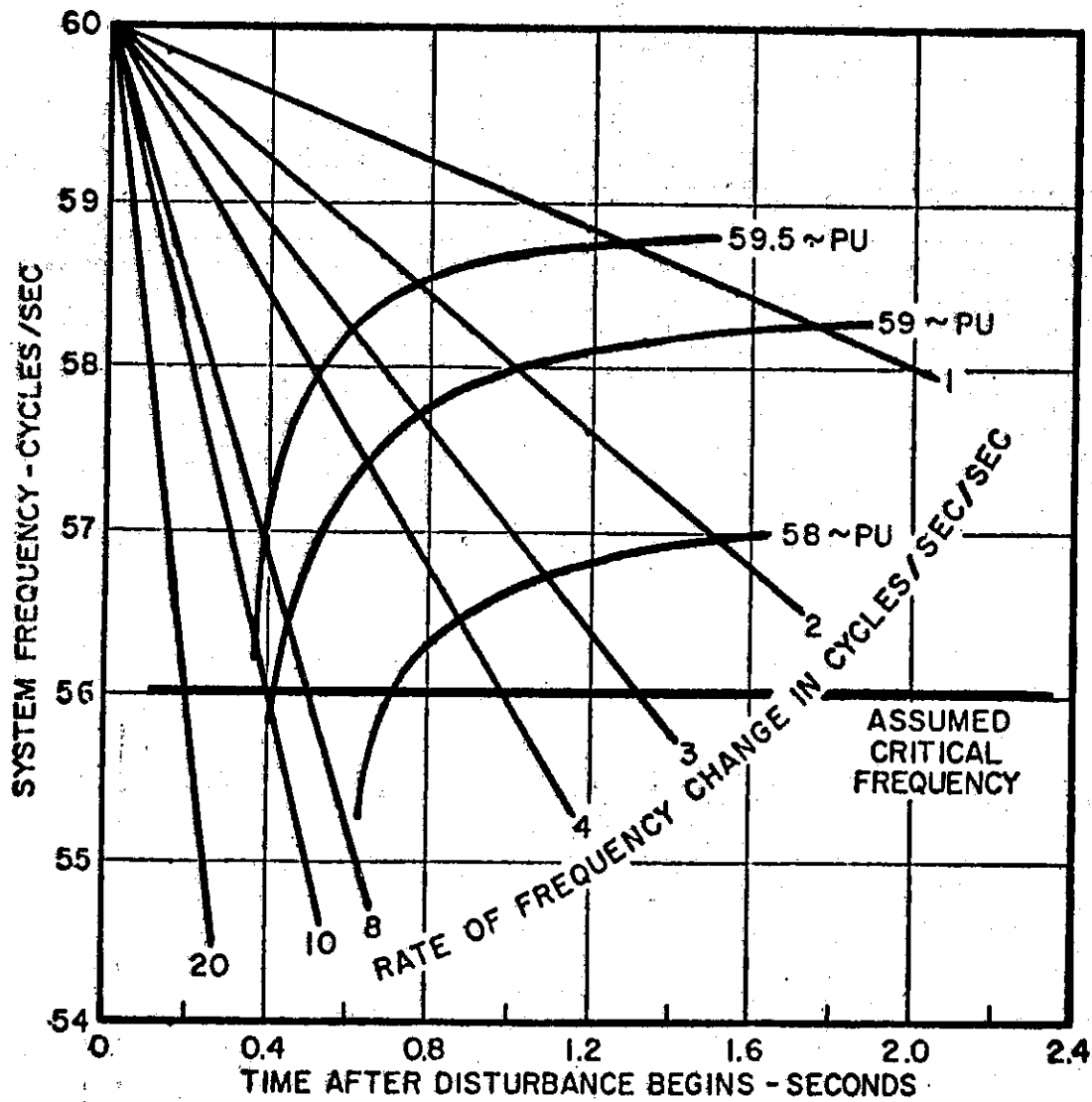
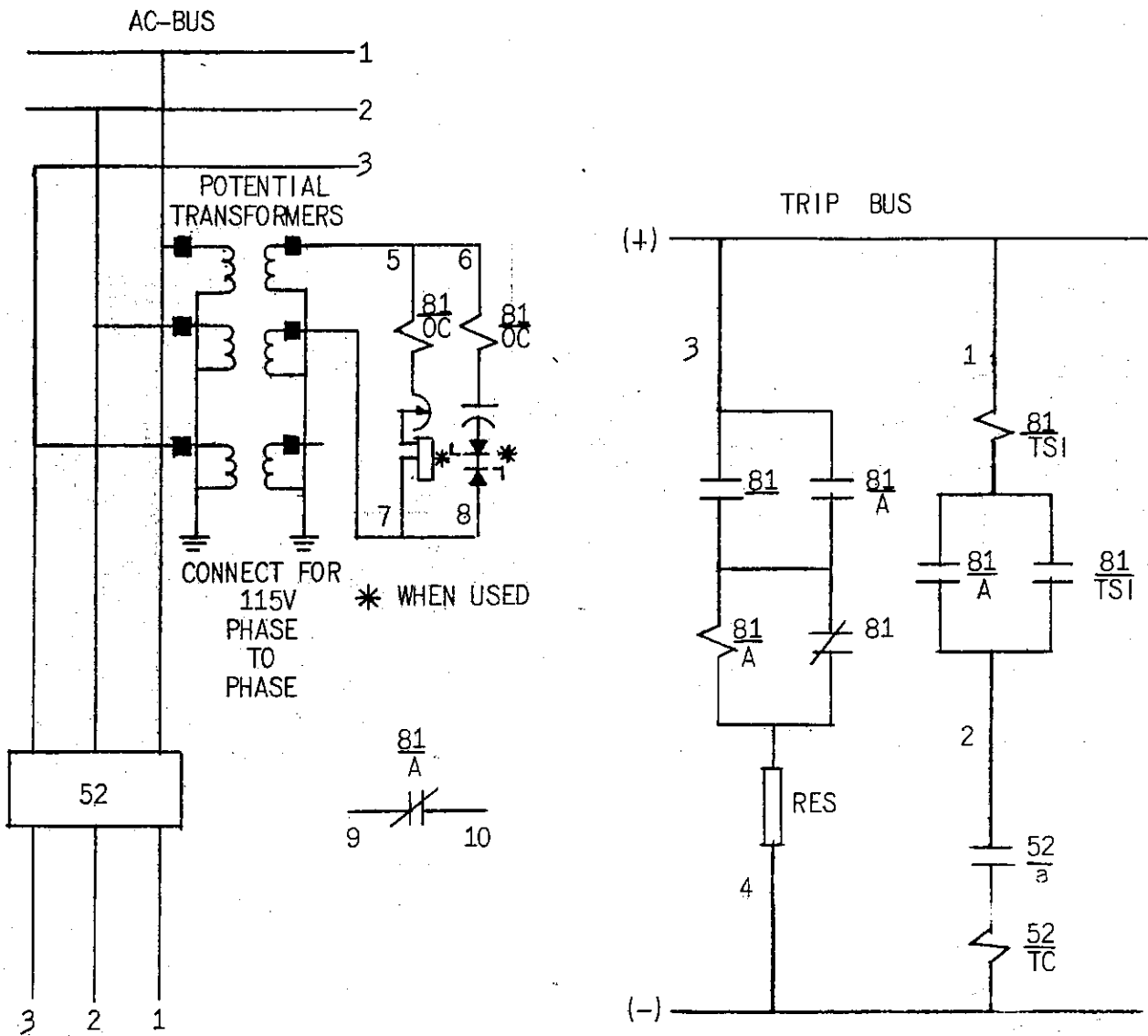


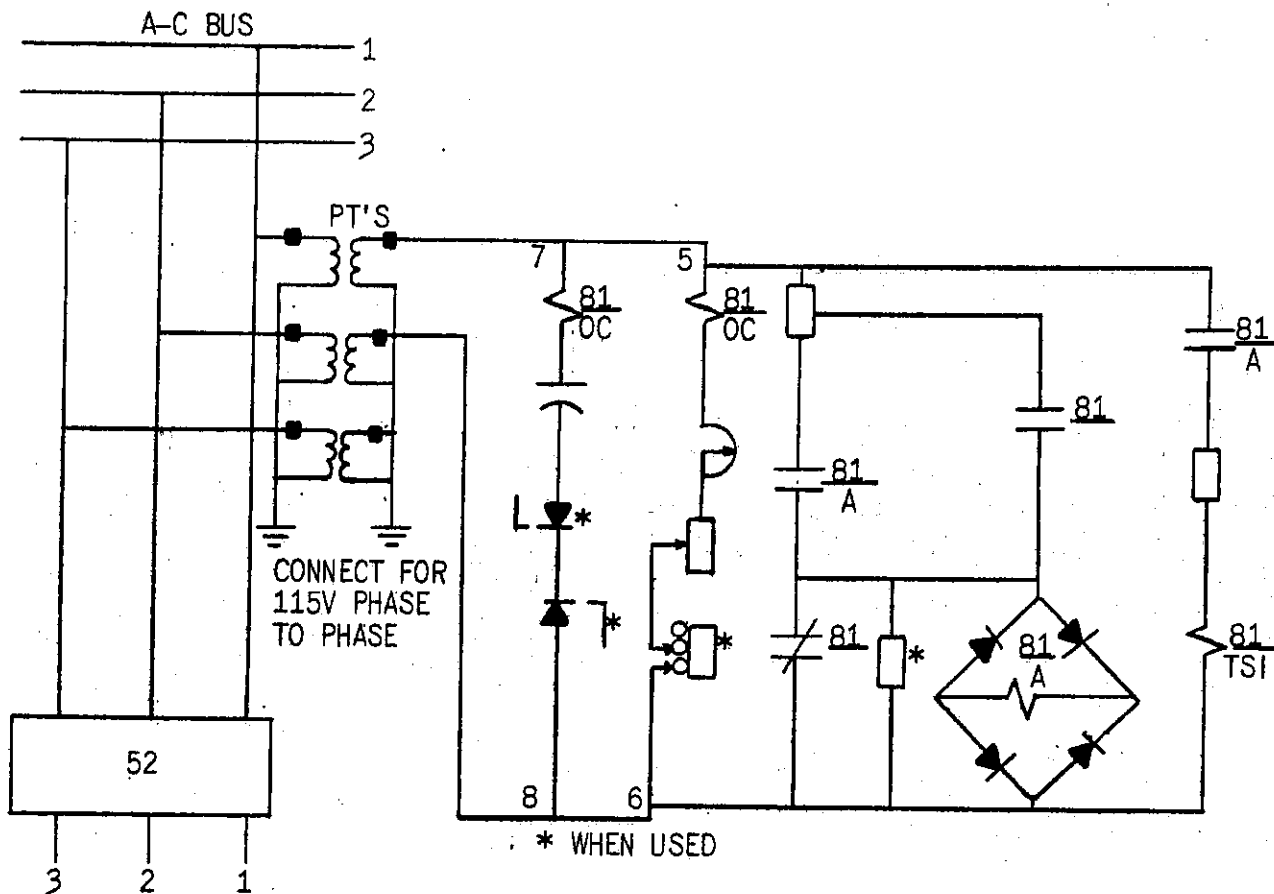
FIG. 1 (0208A2413-0) Frequency VS Time Characteristics For Total Clearing Time For CFF Relays



DEVICE FUNCTION NUMBERS

52 - CIRCUIT BREAKER
81 - FREQUENCY RELAY
TYPE CFF
A - AUXILIARY TELEPHONE RELAY UNIT
52/a - AUXILIARY CONTACT
CLOSED WHEN BREAKER IS CLOSED
OC - OPERATING COIL
TC - TRIP COIL
TSI - TARGET SEAL IN

FIG. 2 (0208A5506-1) External Connections Diagram For Relay Type CFF12A Form 41 And Up



81 - FREQUENCY RELAY TYPE CFF
 A - AUXILIARY TELEPHONE RELAY
 TSI - TARGET SEAL-IN UNIT
 OC - OPERATING COIL
 52 - CIRCUIT BREAKER
 TC - TRIP COIL

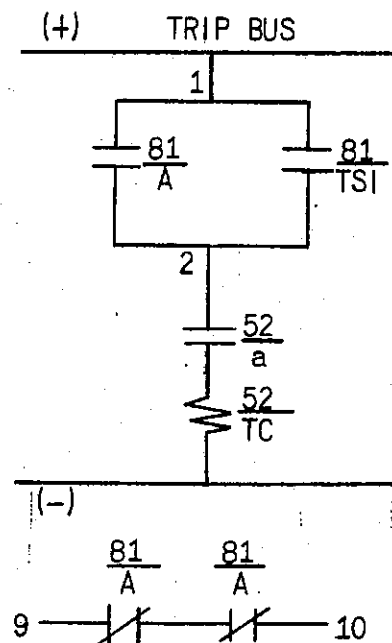
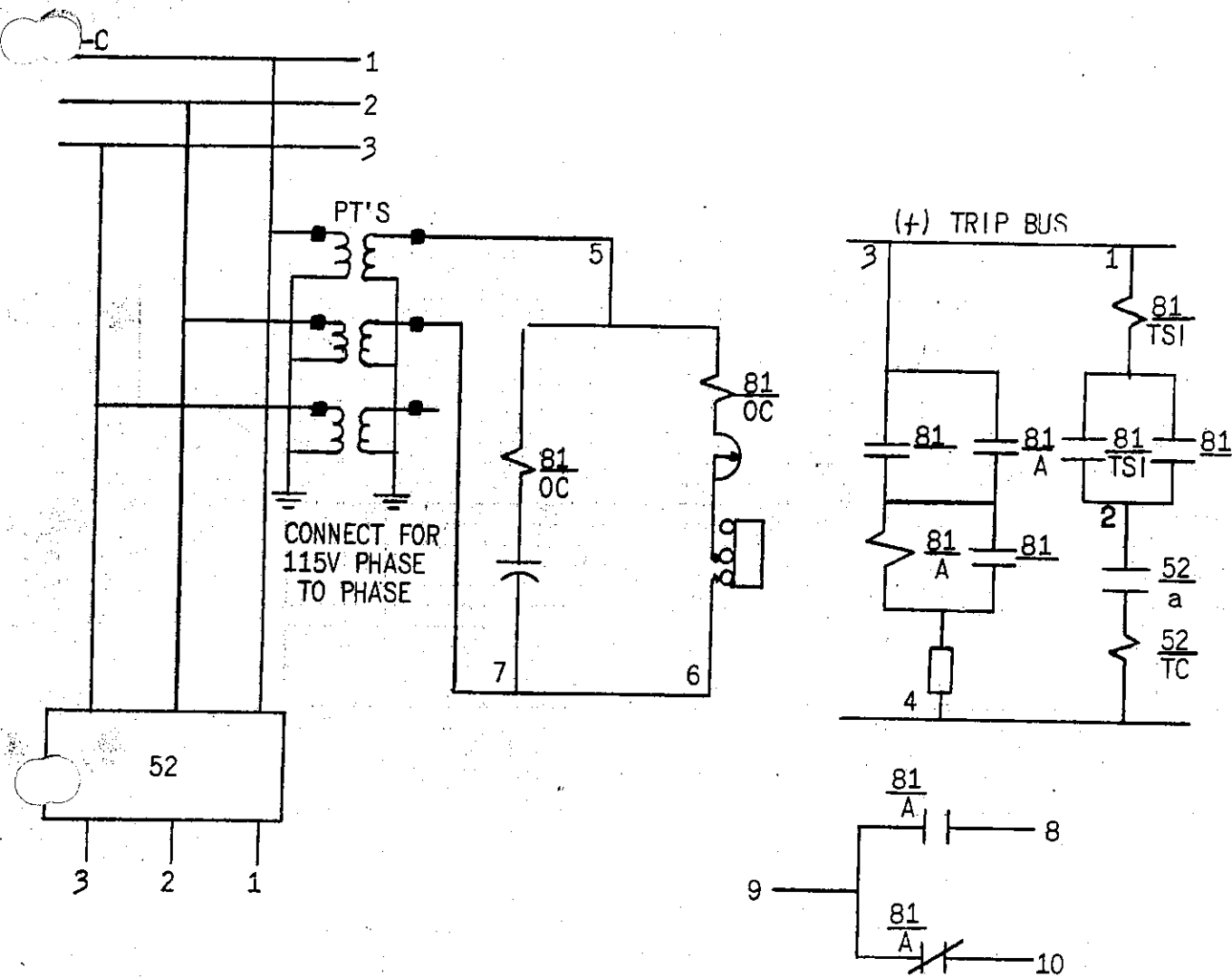


FIG. 3 (0226A7216-1) External Connections Diagram For Relay Type CFF12C



81 - FREQUENCY RELAY TYPE CFF
 A - AUXILIARY TELEPHONE RELAY
 TSI - TARGET SEAL-IN UNIT
 OC - OPERATING COIL
 52 - CIRCUIT BREAKER
 a - BREAKER AUXILIARY SWITCH
 TC - TRIP COIL

FIG. 4 (0226A7215-1) External Connections Diagram For Relay Type CFF12E

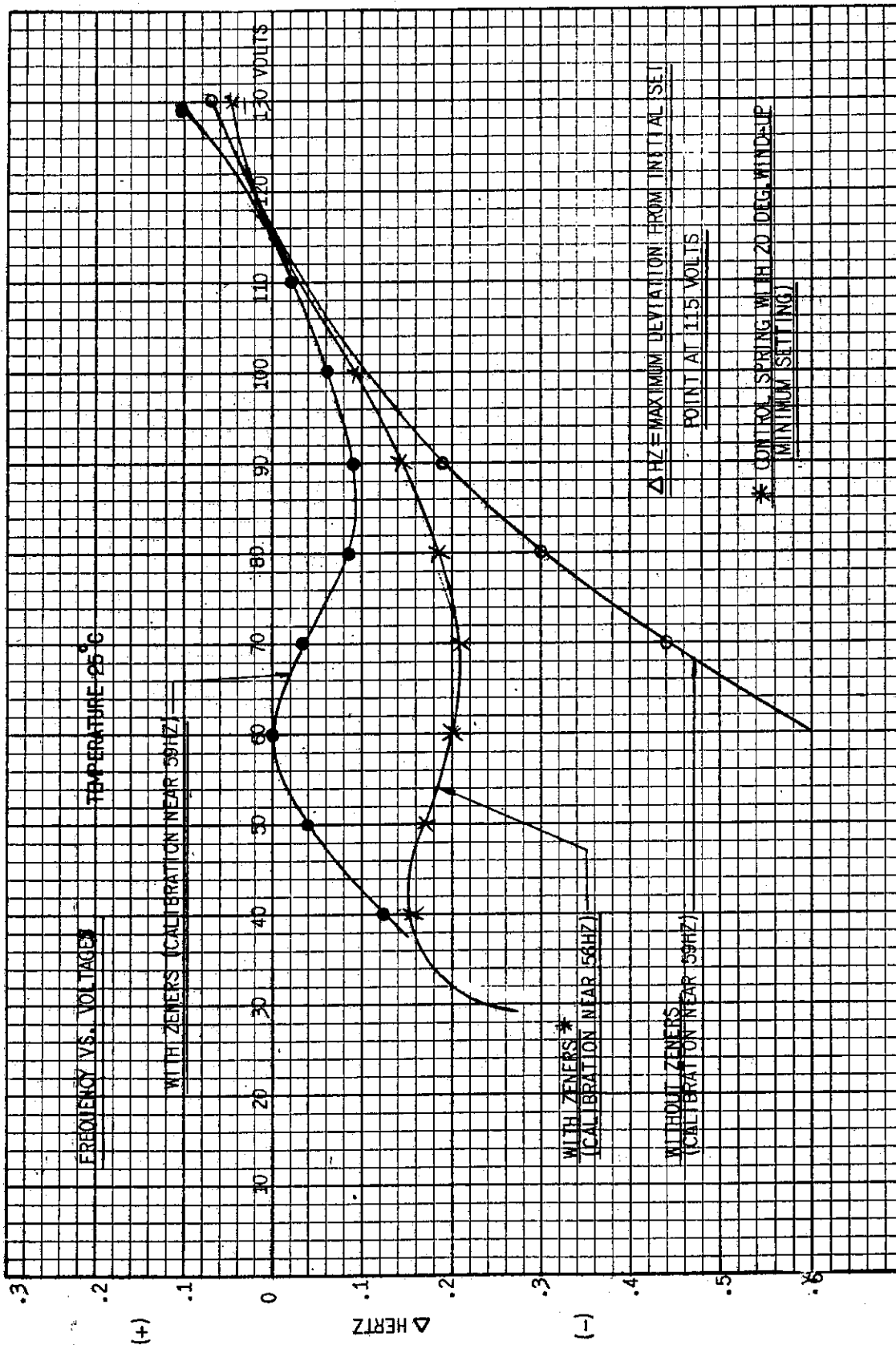


FIG. 5 (0226A6951-0) Typical Operating Characteristics Of Relay Type CFF

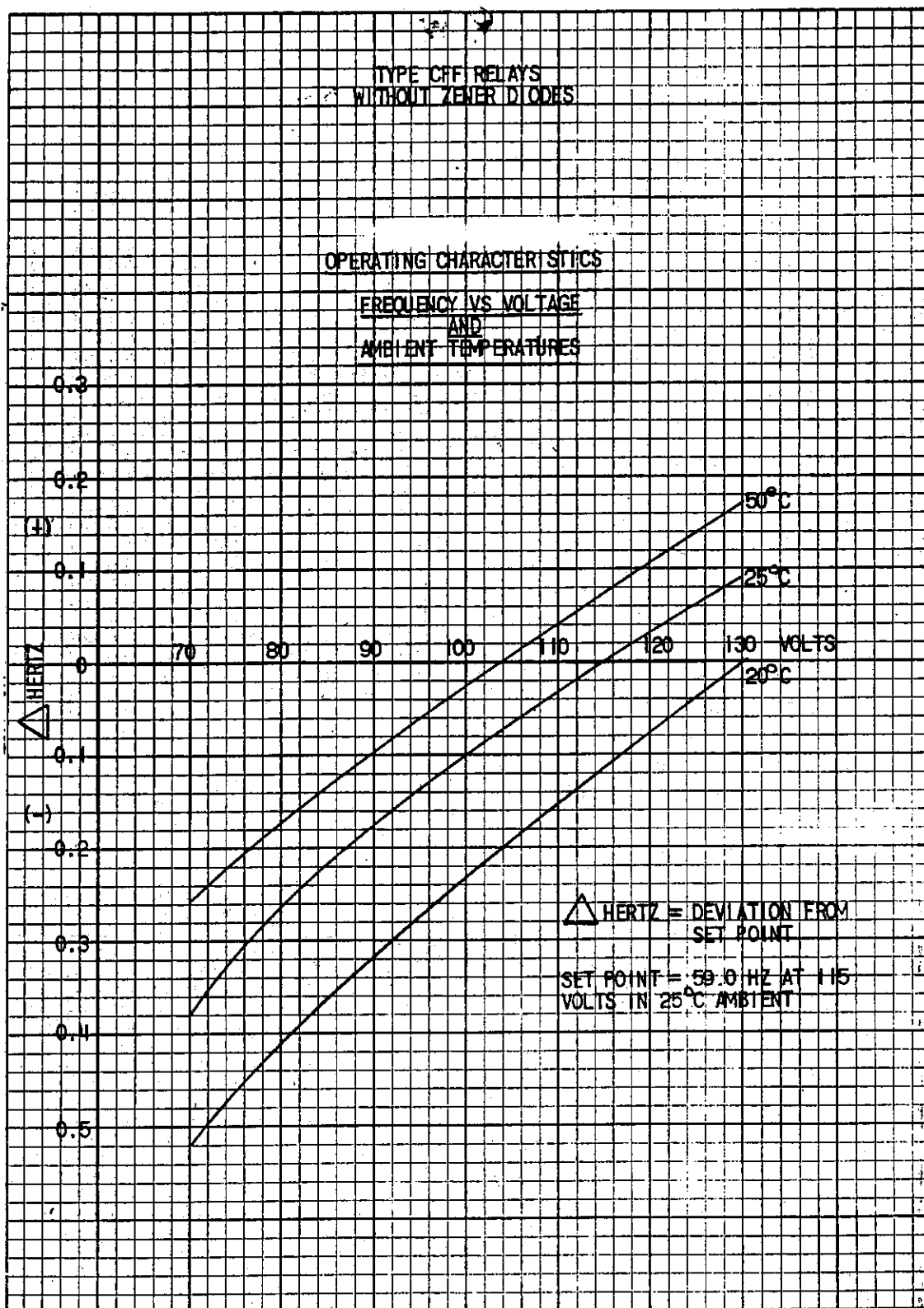


FIG. 6 (0226A6950-1) Typical Operating Characteristics Of Relay Type CFF

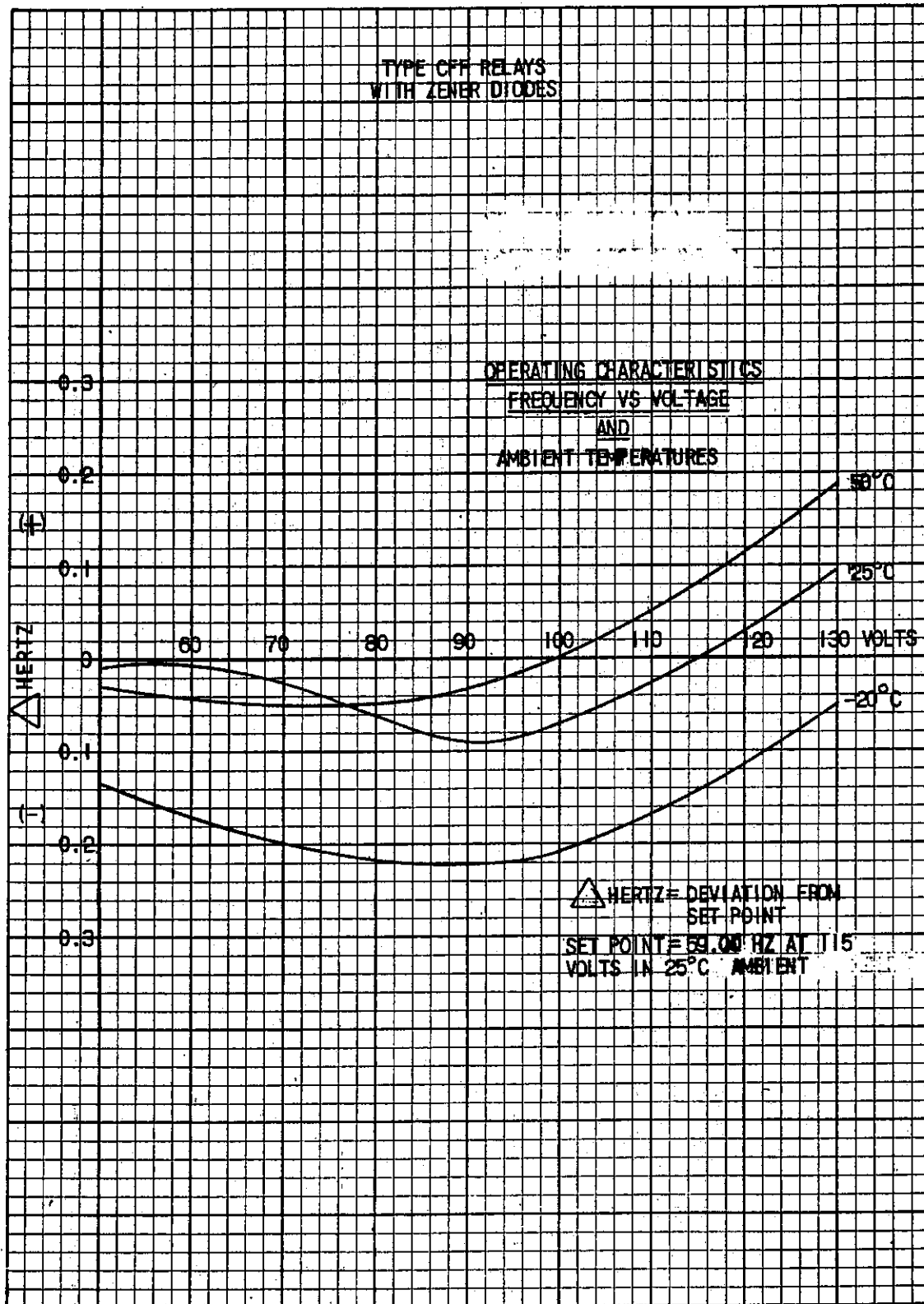


FIG. 7 (0226A6952-1) Typical Operating Characteristics Of Relay Type CFF

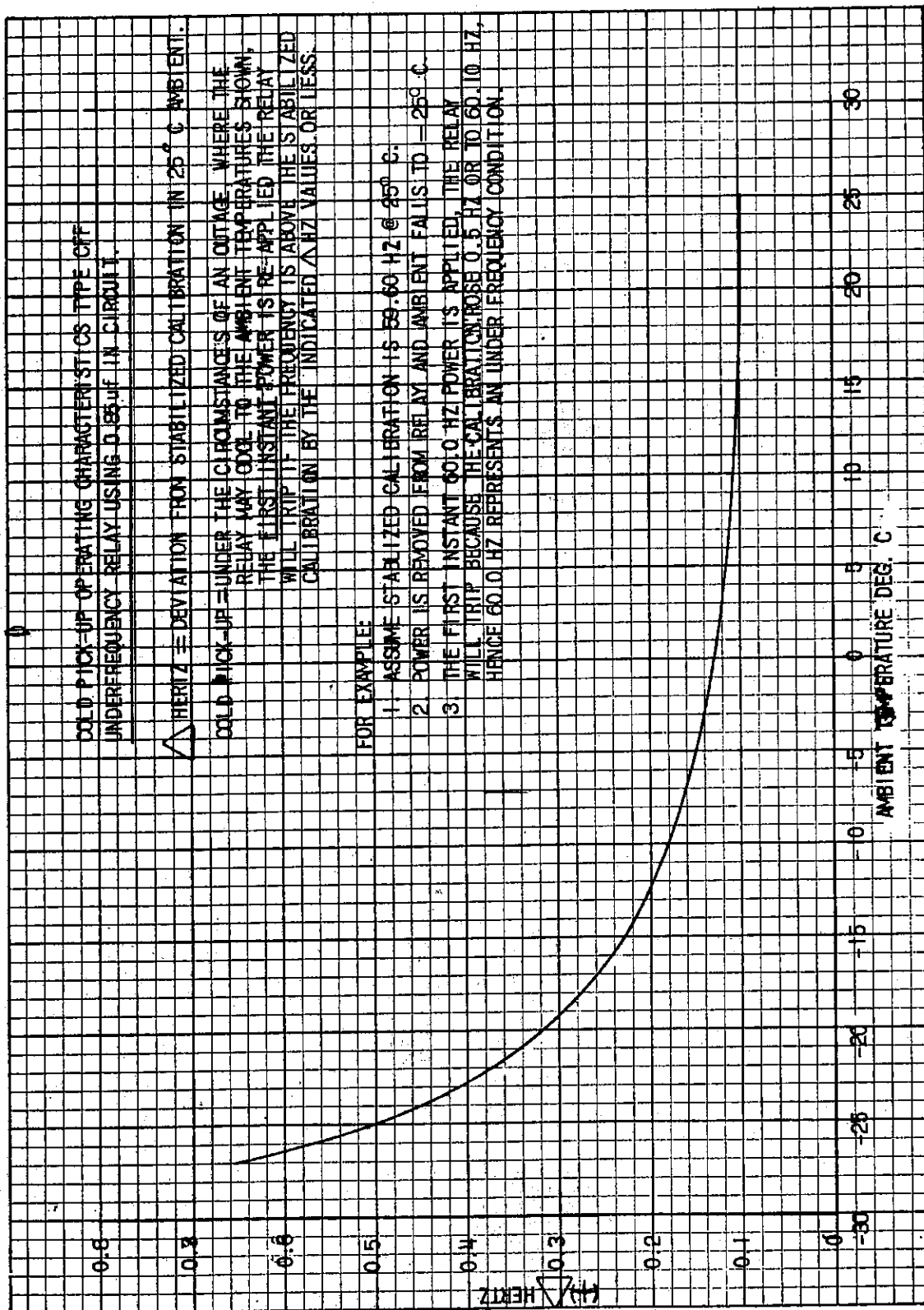


FIG. 8 (0208A5552-1) The Cold Pickup Operating Characteristics Of Relay Type CFF

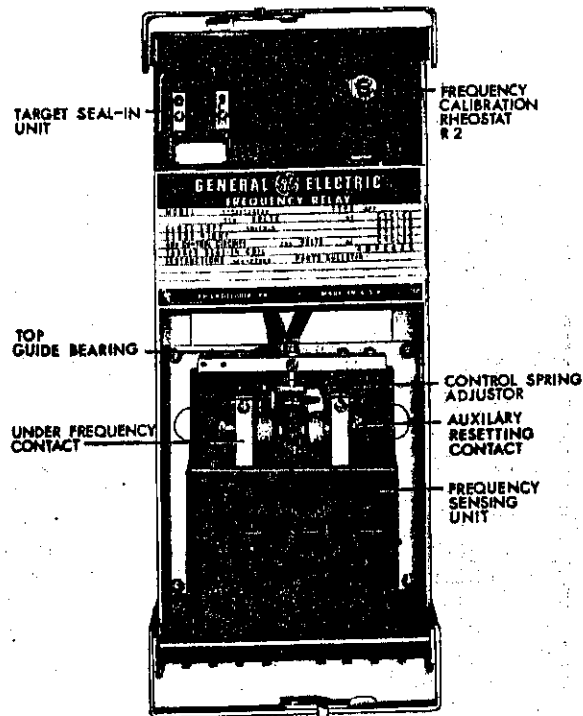


FIG. 9 (8040241) Relay Type CFF12A63A Out Of Case (Front View)

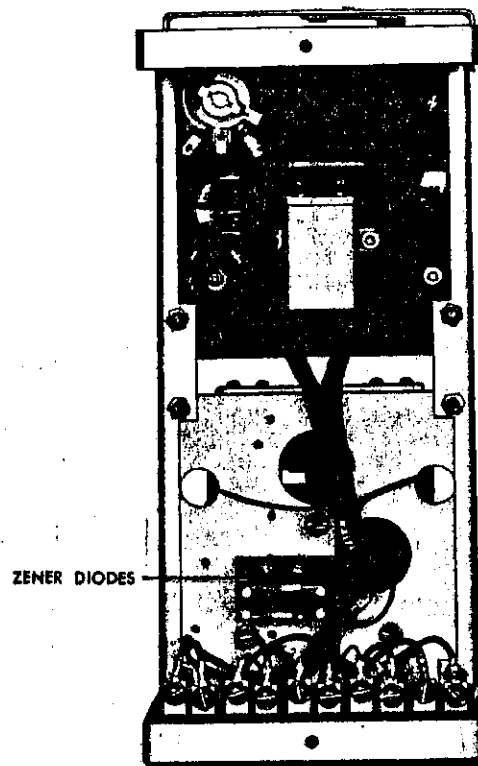


FIG. 10 (8040240) Relay Type CFF12A63A Out Of Case (Rear View)

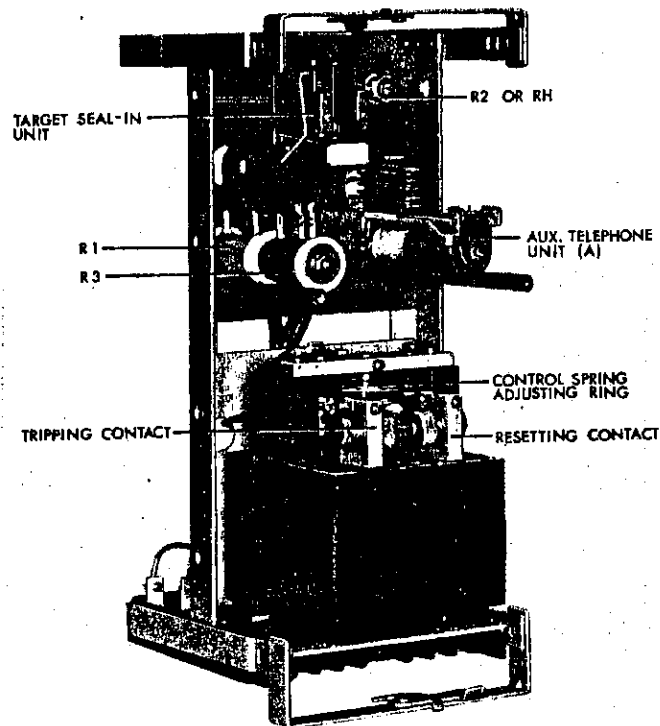


FIG. 11 (8040239) Relay Type CFF12A63A Out Of Case (3/4 Front View)

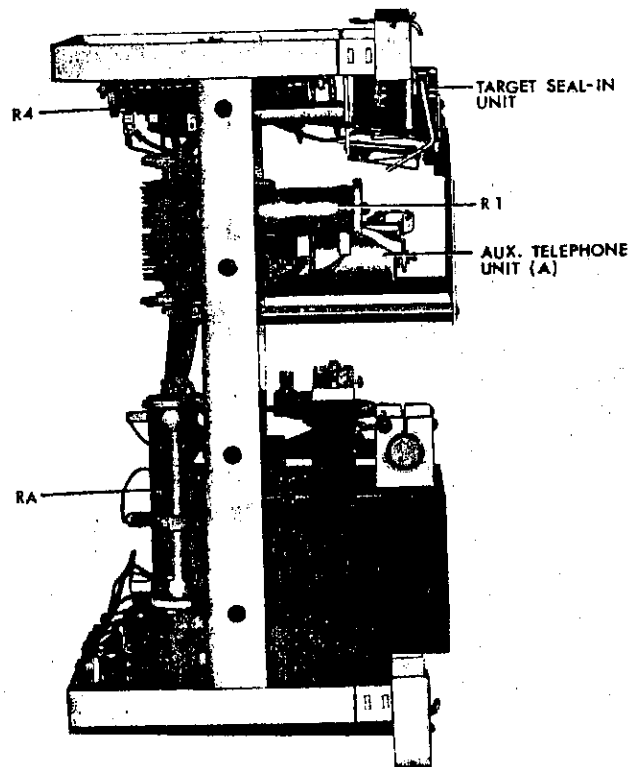


FIG. 12 (8040135) Relay Type CFF12C15A Out Of Case (Side View)

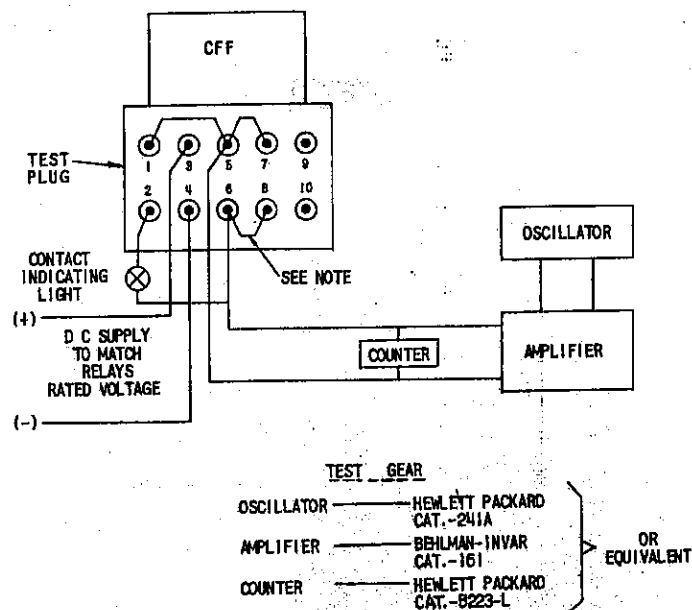


FIG. 13 (0208A5551-0) The Test Diagram For Checking The Frequency Sensing Unit In The CFF12A, CFF12E And CFF12F Relays

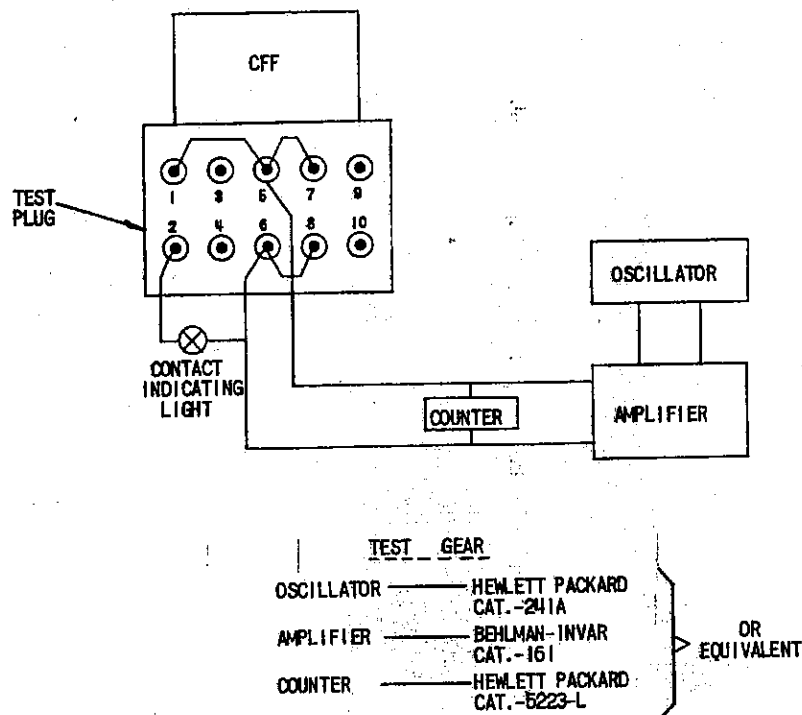
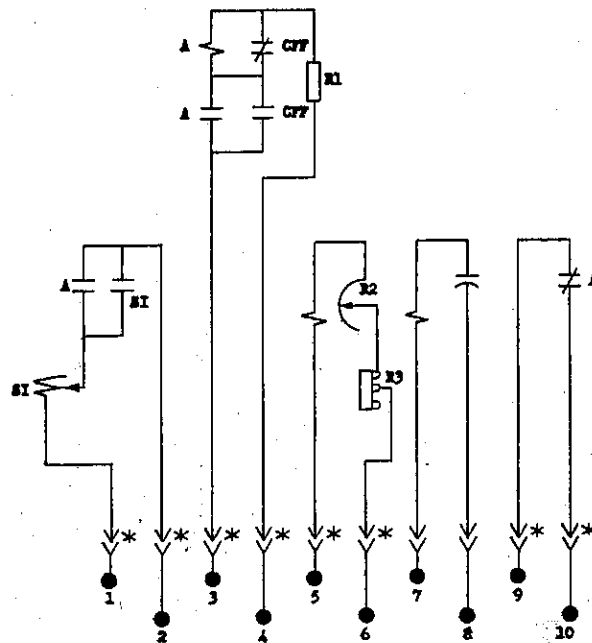
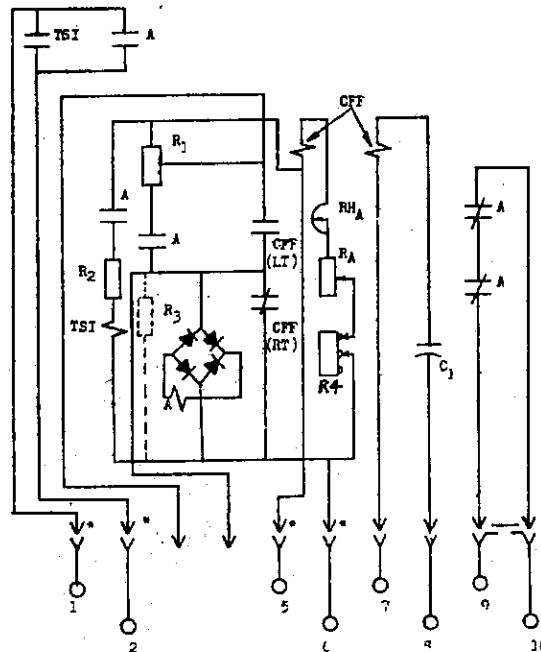


FIG. 14 (0208A5550-0) The Test Diagram For Checking The Frequency Sensing Unit In The CFF12C Relay



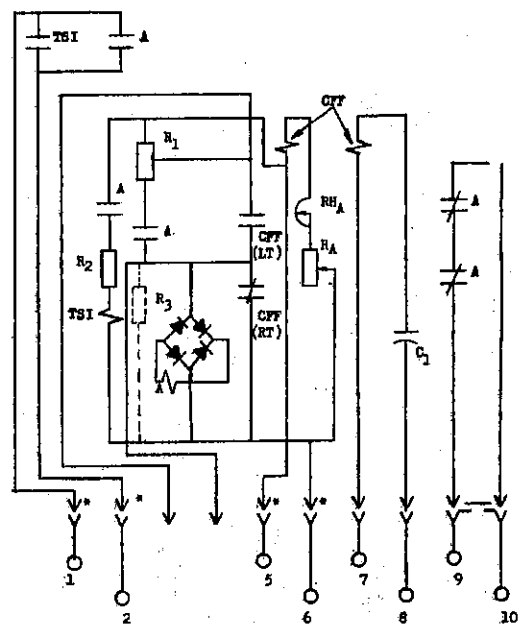
* = SHORT FINGERS

FIG. 15 (0203A8575-1) Internal Connections Diagram For The CFF12A Relay-Form 41 To 60 (Front View)



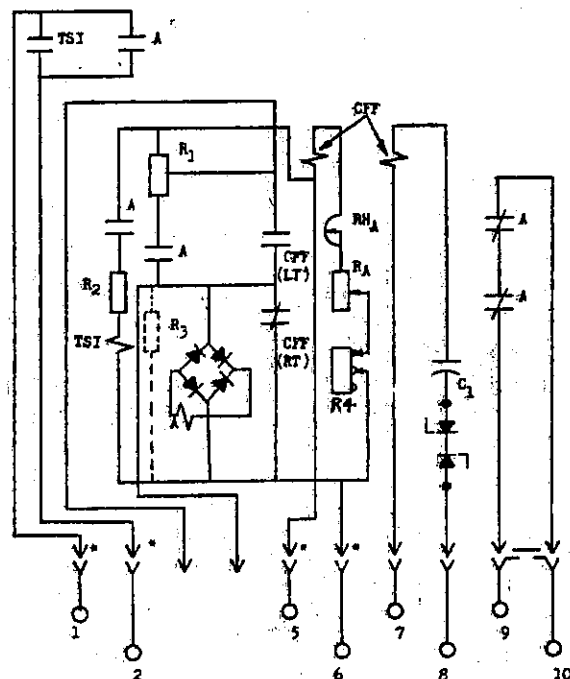
* = SHORT FINGERS
 SOLID LINES - 115V OPERATION
 DOTTED LINES - 230V OPERATION
 TSI - TARGET SEAL-IN
 A - AUXILIARY RELAY
 R_A - RHEOSTAT FOR VERNIER CONTROL OF CALIBRATION

FIG. 16 (0203A8667-1) Internal Connections Diagram For The CFF12C13 Relay (Front View)



**= SHORT FINGERS
 SOLID LINES — 115V OPERATION
 DOTTED LINES — 230V OPERATION
 TSI — TARGET SEAL-IN
 A — AUXILIARY RELAY
 RH_A — RHEOSTAT FOR VERNIER CONTROL OF CALIBRATION

FIG. 17 (0195A4964-4) Internal Connections Diagram For The CFF12C14A And CFF12D11 And Up Relays (Front View)



**= SHORT FINGERS
 SOLID LINES — 115V OPERATION
 DOTTED LINES — 230V OPERATION
 TSI — TARGET SEAL-IN
 A — AUXILIARY RELAY
 RH_A — RHEOSTAT FOR VERNIER CONTROL OF CALIBRATION

FIG. 18 (0208A2356-0) Internal Connections Diagram For The CFF12C15A Relay (Front View)

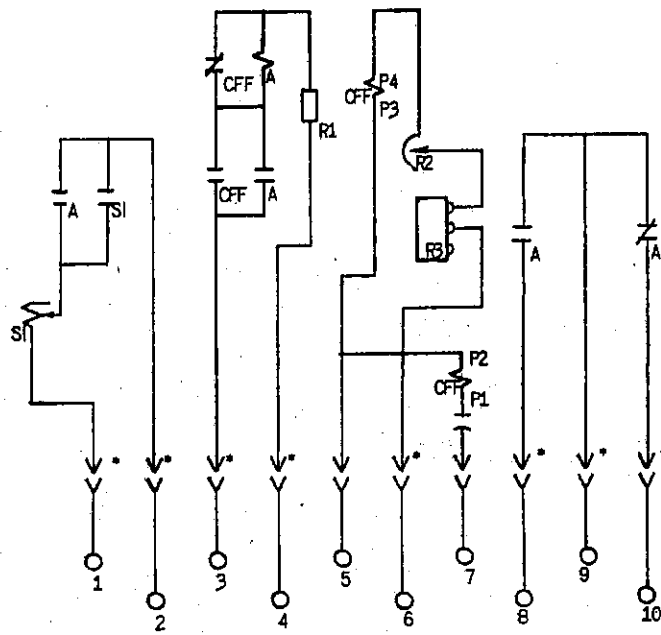


FIG. 19 (0203A8666-0) Internal Connections Diagram For The CFF12E Relay Form 3 & Up (Front View)

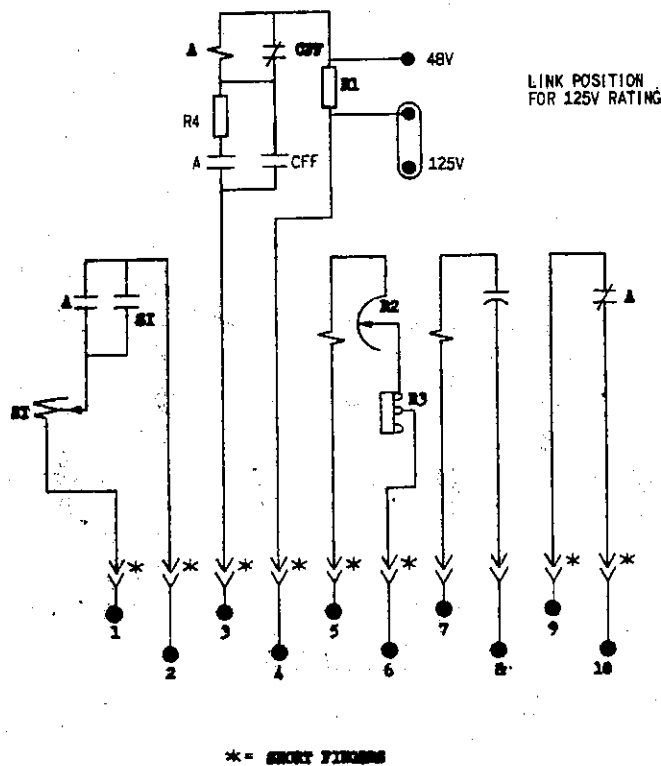


FIG. 20 (0207A7866-0) Internal Connections Diagram For The CFF12F Relay (Front View)

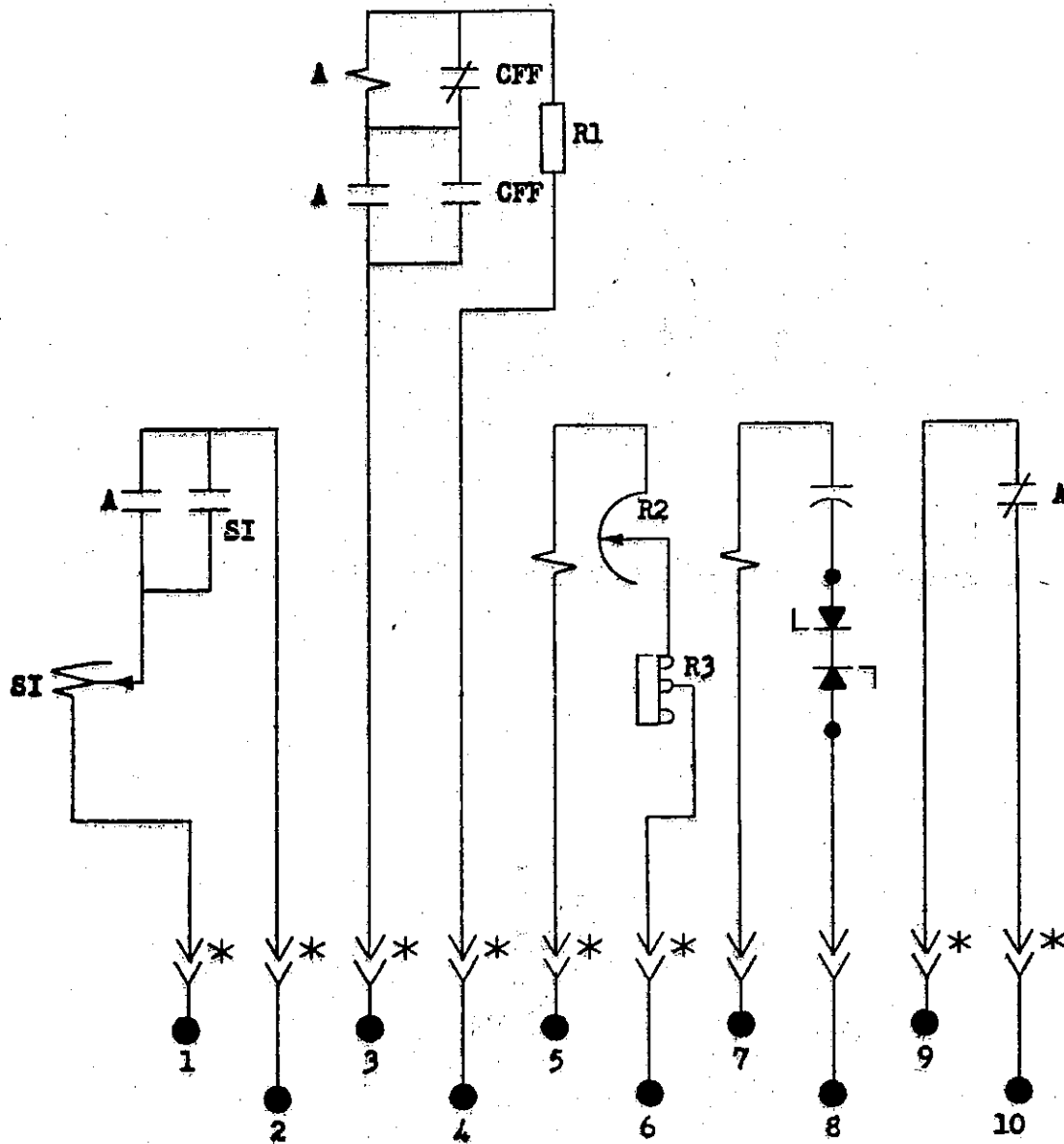


FIG. 21 (0208A2357-0) Internal Connections Diagram For The CFF12A Relay - Form 61 & Up (Front View)

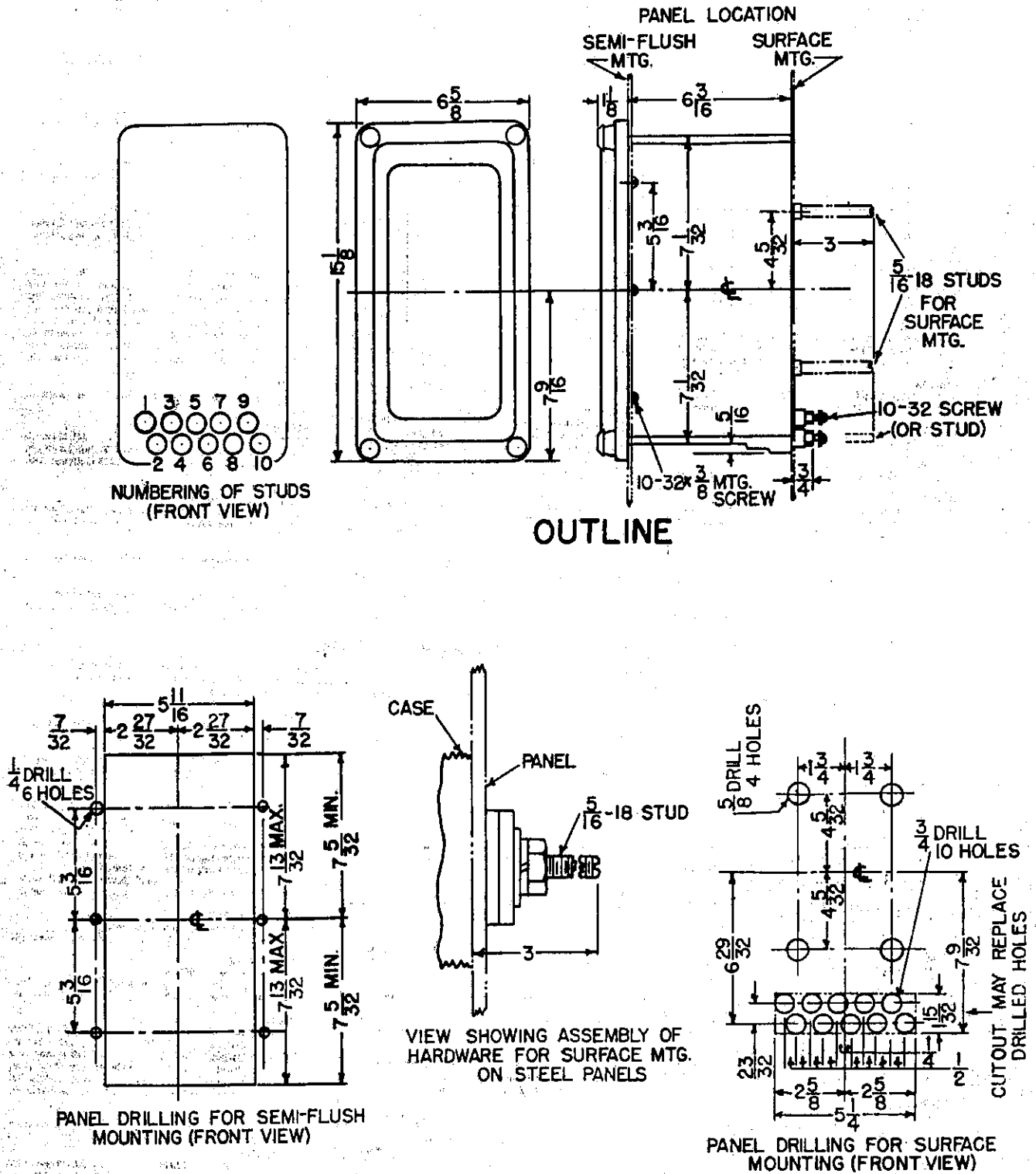


FIG. 22 (K-6209273-2) Outline And Panel Drilling Dimensions For The CFF Type Relays

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