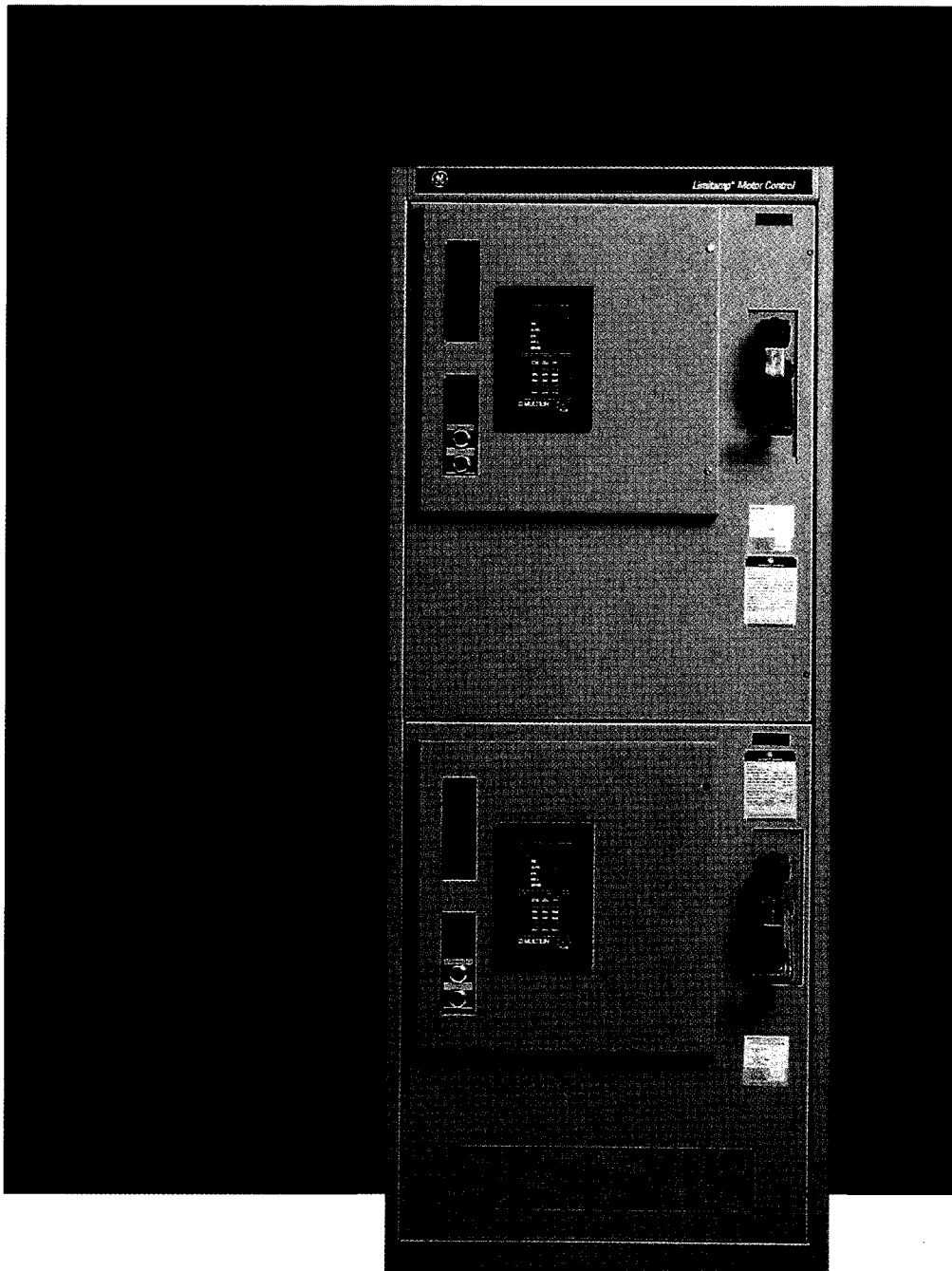




Limitamp® Medium Voltage Motor Control

2400-7200 Volts

Application and Selection Guide





The General Electric Limitamp motor control center provides an economical means of centralizing motor starters and related control equipment. It permits motor control starters, feeders, isolator switches, distribution transformers, interlocking relays, programmable control, metering and other miscellaneous devices to be obtained in a single floor-mounted structural assembly fed from a common enclosed main bus.

Limitamp motor control centers are constructed of standardized heavy gauge vertical sections housing vertical and horizontal buses and compartmented starters. Sections are bolted together to form a single line-up assembly. The entire center may be powered by incoming line connection at a single point. When possible, Limitamp motor control centers bear UL section and unit labels.

General

Controllers

5kV Load-Break Switches

Incoming Line

Enclosures

Protection & Control

Components

Application Data

Elementary Diagrams

Guideform Specifications, Basic Starter Features

A

B

C

D

E

F

G

H

I

J



GE manufactures and provides full support for the following types of medium voltage controllers:

Table A.1 Product Scope

Controllers	Design Layout			Construction	
	1-High	2-High	3-High	Welded	Bolted
CR 194 Stationary Vacuum 400 amp	X			X	
CR 194 Stationary Vacuum 800 amp	X			X	
CR 194 Stationary Vacuum 400 amp		X			X
CR 194 Drawout Vacuum 400 amp		X			X
CR 7160 Drawout Air-Break 400 amp	X	X	X	X	
CR 7160 Drawout Air-Break 700 amp	X			X	

Limitamp Control is designed to meet NEMA ICS 3, Part 2 and UL 347 requirements. Various enclosure types and constructions are available and there is a broad selection of modifications for complete control and protection of motors used on modern power-utilization systems with high available short-circuit currents.

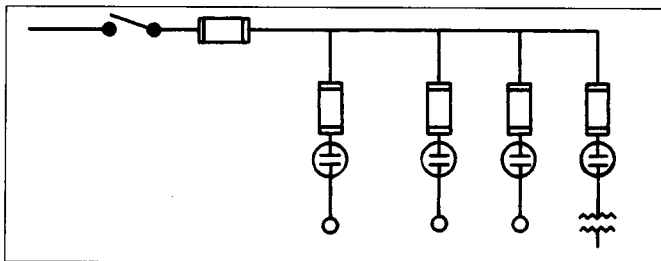
Our preferred design is the CR194 two-high bolted frame for our CR193B 400 ampere vacuum contactor. In addition to vacuum technology, we continue to offer our CR7160 air-break drawout contactor, originally designed in 1966. For detailed information on each of these designs, please see the "Controllers" section.

APPLICATIONS

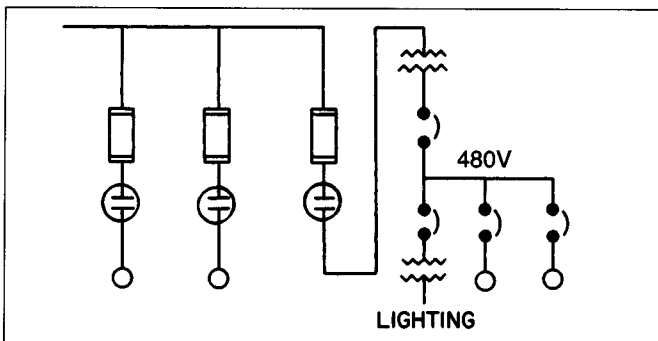
Limitamp controllers are primarily designed for the requirements of motor controllers applied to distribution systems rated 2400, 4160 or 4800 volts. 7200-volt starters are available in limited applications.

Because of its flexibility, other uses for Limitamp equipment have become common. Some of these uses are:

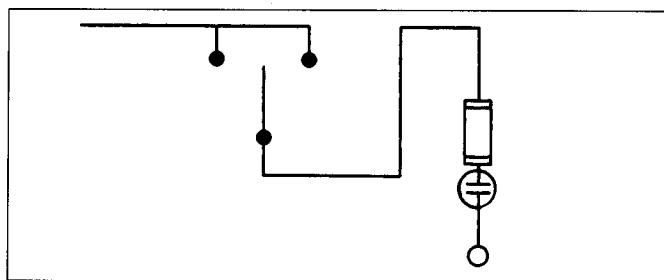
- Limitamp lineup consisting of a fused isolating switch ahead of four NEMA Class E2 Limitamp controllers, the first three being used as motor controllers and the last as a transformer feeder.



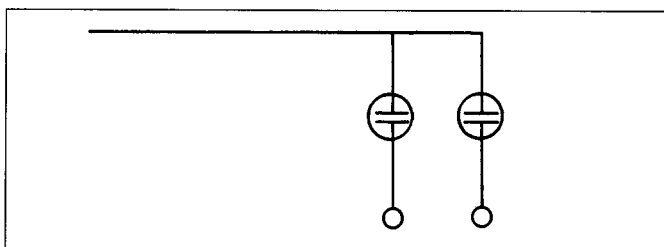
- Limitamp lineup similar to last three units in the preceding description. The transformer, 480-volt motor controllers, and lighting transformer are included in an integrated Limitamp design.



- Limitamp lineup consisting of a reversing isolating switch ahead of a NEMA Class E2 Limitamp motor controller.



- Limitamp lineup consisting of two NEMA Class E1 Limitamp motor controllers, each having interrupting ratings per Table B.1.





A

COMPARISON OF CONTROLLER TYPES

FULL VOLTAGE

The Limitamp Control across-the-line (FVNR) controller is the most popular type of controller. In general, high-voltage systems have fewer power restrictions than low-voltage systems; therefore, full-voltage controllers may be applied to a greater number of applications. Full-voltage controllers provide lowest cost, simplicity, minimum maintenance and highest starting torque.

REDUCED VOLTAGE

Primary reactor (closed-transition) Limitamp controllers are the most popular of the reduced-voltage type starters because they provide a simple, low-cost means of obtaining reduced-voltage starts. The starting time is easily adjustable in the field.

Limitamp closed-transition auto-transformer controllers provide higher starting torque efficiency and a more favorable power factor during starting than a primary reactor starter. The transition time can be easily adjusted in the field. NEMA medium-duty reactors and autotransformers with 50-, 65- and 80-percent taps are provided as standard.

REDUCED INRUSH

Limitamp wye (star)-delta (closed-transition) starters provide a means of reducing the starting inrush where the starting duty is not limited by the controller. This type of controller can be used where extremely long acceleration times are required. Wye-delta starters have a very high torque efficiency. This starter is applicable only to six lead motors and no field correction is possible for starting characteristics. See Table A.2.

TRANSFORMER FEEDERS

Limitamp controllers are generally considered motor starting equipment; however, they are not strictly limited to motors and can provide very good protection for loads such as transformers.

Transformers that can be controlled by Limitamp controllers must have a primary rated in the 2400- to 7200-volt range.

To adequately protect a transformer, it is necessary to define specific protection requirements. The following areas will be considered:

1. Transformer winding fault (primary and secondary)
2. Single-phasing, resulting in a phenomenon known as "ferroresonance"
3. Transformer overload

These functions are basic only and are not intended to be comprehensive. Ground fault, differential, fault pressure, undervoltage, etc., are often required and may also be added to a given control. In addition, a transformer controller must allow for transformer inrush current and not cause a nuisance trip-out from a momentary line-voltage dip.

Transformers must be protected from primary and secondary (winding or downstream) faults. In Limitamp controllers, current-limiting fuses are applied to protect the transformer from a primary winding fault, as well as faults in the conductors from the controller to the transformer. The fuses are selected to clear high-magnitude fault currents at the first fault half-cycle and allow the contactor to energize a transformer without operating on inrush currents. (Inrush currents occur when transformer is energized, typically 8-12 times rated amperes for 0.1 seconds). GE Type EJ-2 current-limiting fuses may be applied when used with an overcurrent relay that is chosen to coordinate with the EJ-2 fuse and protect the transformer from damage as a result of a fault in its secondary circuit.

PROTECTION

To determine a basis for protection, refer to ANSI transformer short-circuit ratings, which define the magnitude and duration of downstream faults that a transformer can withstand without damage. A relay would have to be set to operate before the damage point is reached. Base ratings, impedance and the connection of the primary and secondary windings of the transformer must be supplied in order to arrive at the relay setting. The relay for this purpose can be an electronic overload relay.

A common problem with single-phased transformers is a phenomenon known as ferroresonance, which can occur when an unloaded or lightly loaded transformer sustains an open conductor in its primary circuit.

Ferroresonance causes system overvoltage as a result of the transformer core inductance forming a "tuned" circuit with the system distributed capacitance. To avoid ferroresonance, all three lines must be switched simultaneously as with a medium-voltage contactor. However, if one line fuse blows, then single-phasing will occur. To prevent this, the medium-voltage contactor may be supplied with a contactor tripping mechanism that operates from a striker pin located in the fuse. When the fuse element burns in two, the spring-loaded striker pin is released. It projects upward and operates a contact that trips the contactor. This feature, known as blown fuse trip, would provide positive transformer protection from single-phasing due to blown fuses.



Transformer feeders typically are applied on critical process applications where it is important to maintain continuity of operation through a system voltage disturbance. Mechanically latched contactors allow the contactor to remain closed during a disturbance. Like circuit breakers, latched contactors are opened either manually or by means of a shunt trip solenoid.

CAPACITOR FEEDERS

Limitamp 400 amp contactors are ideally suited for capacitor switching applications. (Note: 800 Amp is not rated for capacitor switching.)

Capacitors may be switched with the motor, but maximum rating for this function must be determined by motor design.

When the capacitors are provided in Limitamp control, they are normally mounted in an auxiliary enclosure beside the Limitamp controller. A capacitor rated up to 200 KVAR can be mounted in the top of a two-high CR194 enclosure with the controller in the bottom. (See Table B.7 for capacitor switching capacities.)

FUTURE STARTERS

Future squirrel-cage, full-voltage non-reversing starters can be installed in two-high and three-high construction only when factory-prepared space has been purchased with the original Limitamp equipment.

The purchase of factory-prepared space provides a space unit equipped with vertical power bus, complete interlocking and isolating mechanisms, operating handle and high-voltage door. It does not include electrical components.

When parts are purchased to fill a future starter, these consist of a contactor, power fuses, control power transformer, CPT fuses and fuse supports, current transformers, and low-voltage panel and devices.

Table A.2 Comparison of Starting Characteristics

Starter	Starting Characteristics Expressed in Percent Rated Value				
	Voltage of Motor	Motor Current	Line Current	Torque	Torque Efficiency
Full Voltage	100	100	100	100	100
Autotransformer					
80 percent tap	80	80	64 ①	64	100
65 percent tap	65	65	42 ①	42	100
50 percent tap	50	50	25 ①	25	100
Primary-Reactor					
80 percent tap	80	80	80	64	80
65 percent tap	65	65	65	42	65
50 percent tap	50	50	50	25	50
Wye-Delta	100	33	33	33	100

① Autotransformer magnetizing current is not included in listed values.

Magnetizing current is usually less than 25 percent motor full-load current.

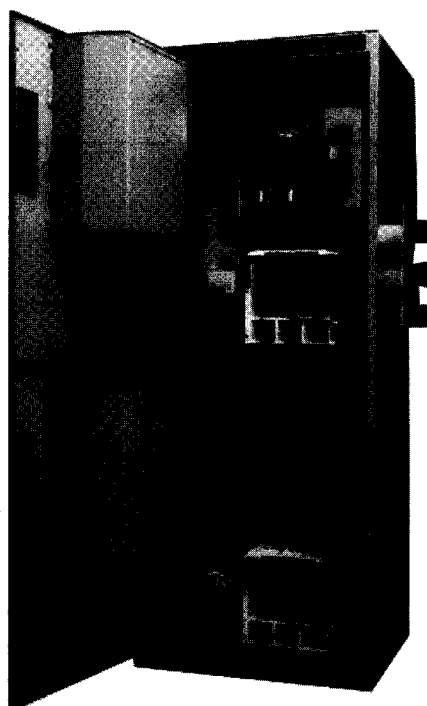


Figure A.1 Medium Voltage Compartments in CR194 two-high design

A



A

Table A.3 Limitamp® UL-Listed Equipment (as of December 1995)

Product/ Application	Max. Fault Rating	Max. Current Rating (Amps)	Main Bus Rating ①	Enclosure Sizes ②	Power Fuse Types	Overload Relays ③	Potential Transformers
One High CR194 400A ⑦ Vacuum Stationary Controller (FVNR) (induction motor or transformer loads)	50 kA RMS symm. 4.80 kV (fused)	360A vented 320A non-vented	1000A ⑧ 2000A	1-high 26W x 90H x 30D (34W optional)	GE Type RB Bolted	CR324C Multilin 269+	N/A
Two High CR194 400A Vacuum Stationary or Drawout (FVNR)	50 kA RMS symm. 4.80 kV (fused)	TOP: 360A vented 320A non-vented BOTTOM: 400A vented 320A non-vented	1000A ⑧ ⑨ 2000A (1950A non-vented)	2-high 36W x 90H x 30D (40W optional) epoxy coated	GE Type RB Bolted	CR324C Multilin 269+	N/A
CR194 800A Vacuum Stationary (FVNR) (induction motor or transformer loads)	50 kA RMS symm. 4.80 kV (fused)	760A vented 640A non-vented	1000A ⑧ & 2000A	1-high 48W x 90H x 30D	Carbone Ferraz Type RB Bolted	CR324C Multilin 269+	N/A
CR7160 400A ⑩ Air-Break Drawout (FVNR) (Induction motor or transformer loads)	50 kA RMS symm. 4.80 kV (fused)	320A 1-high non-vented 360A 1-high vented 310A 2-high vented 250A 3-high vented 310A 3-high, with only 2 contactors	1000A & 2000A	1-high 34W x 90H x 30D (42W optional) 2-high & 3-high 44W x 90H x 30D	GE Type RA or RB	CR324C Multilin 269+	N/A
IC1074 1200A ⑪ Load Break Switch (stationary) (main, feeder, or tie)	50 kA RMS symm. 4.76 kV (fused)	1200A vented w/o fuse 1000A non-vented w/o fuse 960A vented with fuse 840A non-vented with fuse	1000A & 2000A	38W x 90H x 30D	Carbone Ferraz	N/A	ITI stationary only
Auxiliary Sections ⑫ (incoming line, metering auxiliary)	38 kA RMS symm. 4.76 kV	Per devices installed	1000A & 2000A	90H x 30D any width available (22" minimum)	N/A	N/A	ITI stationary only

NOTES:

- ① Copper only, silver or tin plating, insulation available.
 ② NEMA 1 only; gasketing available.
 ③ CR324 is ambient-compensated.
 ④ With primary and secondary fuses.
 Remote control power available.

⑤ High-voltage power cable is MV-90 Dry.

⑥ Includes power supply. Use RB bolted fuses.

⑦ Mechanical latch available. Capacitor trip device also
available with latched contactor.

⑧ A switch may be used for isolation only.

⑨ Surge arresters available: GE #9L11XPB Polymer series.

⑩ Epoxy-coated.

⑪ Refer to factory for 1200A main bus application.

⑫ Obsolete design-for replacement only

Standard UL-listed components are:

- GE CR104P switches, push buttons
- CR151B terminal boards
- American Solenoid Selector Switches
- CR120B control relays

NOTE: ANY UL-LISTED LOW-VOLTAGE
COMPONENT IS ACCEPTABLE.

Other UL-listed components are:

- Switches: GE SBM, SB-1, SB-9, SB-16, HEA, HFA, HMA, HGA States Co. 401-410
- Fused pullout switches: Cooper Industries #15149-2, -3
- Control Circuit Plugs: Amp-LOK, Mate-N-Lok
- Terminal Blocks: GE EB 1, 2, 4, 25, 26, 27; CR151 A, B, C, K
- Time-Delay Relay: F5-143, 152, 162 (Flasher)
- Control Relays: Potter/Brumfield R10T SSAC
- Protective Relays: GE IAC, PJC, NGA, NGV, IJS, IJD, ICW, ICR, IAV, IFC, CFD, IJC

- Voltage Sensing Relays: Wilmar Models D100, D100x, D101, D101X, D1014X, 6X, 10X
- Meters: GE DS-63 through 67, 69; Yokogawa
- Synchroscope, PF, VM, AM, WM, VAR
- Transducers: WodexFunction Monitors: Crompton Inst. Model 256-TWM, TXM, TYM
- Strip Heaters: Wellman Type SS
- Suppressors (Coil): CKE/Electronic RC-1313EFR-N



Table A.4 Publication References for Limitamp Equipment

A

Power Transformers ④	Wiring Type ⑤	Blown Fuse Trip ⑥	Ground Fault
GE 2 or 3 kVA	MTW THW SIS XHHW	Available with indication	ITI #GFM
GE 2 or 3 kVA	MTW THW SIS XHHW	Available with indication	ITI #GFM
GE 2 or 3 kVA	MTW THW SIS XHHW	Available with indication	ITI #GFM
GE 2 or 3 kVA	MTW THW SIS XHHW	Available with indication	ITI #GFM
N/A	SIS only	N/A	N/A
15 kVA max. (stationary)	SIS only	N/A	N/A

Publication	Description	Stocking Location
CR194 Vacuum Design		
GEH-6263	2-high Maintenance Instructions	Bloomington
GEH-5305	1-high Maintenance Instructions	Bloomington
DET-064	Advertising Brochure	Bloomington
GEH-5396	800 Amp 1-high Maintenance	Bloomington
GEF-8016	Contactors Renewal Parts	Mebane
GEH-5306	Contactors Maintenance Instructions	Bloomington
CR7160 Air-Break Design		
GET-3140	Selection & Application	Bloomington
GEH-3091	Instructions	Bloomington
GEH-3102	Contactors Maintenance Instructions	Bloomington
Fuses/Curves		
GES-5000	Power Fuse Curves	Bloomington
General Purpose Controls		
GEP-1260	Control Catalog — Covers Full Line of Products	Bloomington
Pilot Devices		
GEA-10877	CR104P Push Buttons and Pilot Lights	Bloomington
Relays and Timers		
GEA-10639	CR122B, CR122BT, Series A Relays	Bloomington
GEH-4115	CR120B AC Relays	Bloomington
GEH-4120	CR120B Latched Relays	Bloomington
GEH-4147	CR122B Time-Delay Relays	Bloomington
GEH-4139	CR122BP Time-Delay Relays	Bloomington
GEH-969	CR7 Control and Timing Relay	Bloomington
GEH-5475	C-2000 Mini-Contactors Control Relays	Bloomington
GEH-5201	CR192 μ SPM for Synchronous Starters	Bloomington
1601-0057	Multilin 469	GE-Multilin
1601-0025	Multilin 269	GE-Multilin
1601-0013	Multilin 269+	GE-Multilin
1601-0060	Multilin 239	GE-Multilin
GEA-10618	Load Trak IV	DRIVES —Salem, VA
GEH-5600	Load Trak IV	DRIVES —Salem, VA
Metering		
GEH-6302	Power Leader EPM, User's Guide	Bloomington
GEH-5892	Power Leader, User's Guide	Bloomington

CSA-certified Limitamp Controllers: Refer to GE sales office for applications requiring compliance with CSA and CSA labels.



CR194 VACUUM STATIONARY & DRAWOUT*

INTRODUCTION

CR194 Vacuum Limitamp Control is a high-interrupting-capacity, high-voltage control used throughout industry to control and protect squirrel-cage, wound-rotor and synchronous motors. It can also be used to feed transformers and other power-utilization circuits.

Typical applications are in paper, steel, cement, rubber, mining, petroleum, chemical and utility-type industries. Limitamp control is also used in water and sewage plants and public buildings for air conditioning, pumps and compressors.

FEATURES

- **Easily removable contactor** — The stationary or drawout contactors can be easily removed by loosening easily accessible bolts. Front access to the coil and tip wear checks will substantially reduce the need to remove the contactor in normal circumstances.
- **400 or 800 Ampere Contactor** — Vacuum Limitamp control meets the varying needs of industry including today's higher horsepower requirements.
- **NEMA rated** — Vacuum Limitamp control is fully rated and designed to meet the requirements of NEMA ICS 3, Part 2 Class E2 controllers.
- **UL rated** — Vacuum Limitamp control is fully rated and designed to meet the requirements of UL 347.
- **Self-contained power bus** — Vertical power bus is a standard feature of Vacuum Limitamp control. Horizontal power bus is available within the standard 90-inch height and lines up with that of previous Limitamp designs. The power bus ratings have capacity for extended lineups and larger starter requirements.
- **Installation ease** — Provision for cable runs from the top and bottom; easily accessible terminals and small overall size make installation fast and easy.
- **Proven reliability** — Vacuum Limitamp control utilizes the latest vacuum interrupter technology for long, reliable service.
- **Simplified construction** — The operating mechanisms inside Vacuum Limitamp control have been simplified for further improvements in reliability and ease of maintenance.
- **Cooler operation** — The reduced power losses of vacuum interrupters, coupled with other design improvements, provide a controller that is cooler operating to further enhance service life.

- **Quick-make quick-break non load-break disconnect** — Disconnection of the starter from the main bus is accompanied by a quick-make quick-break non load-break disconnect switch. This switch improves the overall control integrity by eliminating the need to rack out the contactor to isolate the load from the power bus.
- **Viewing window** — The switch is equipped with a viewing window for visual assurance that the disconnect contacts are open, and a full barrier for personnel safety. When the plunger on the handle is depressed, the CPT secondary is (isolated) disconnected, which drops out the contactor coil. Then, when the handle is thrown to the "off" position, the CPT primary and the high voltage compartment are isolated from line power.
- **Dependable performance** — Vacuum Limitamp control is coordinated to provide the required motor protection functions and offer reliable overcurrent protection against the damaging effects of overloads and short circuits.

INTERRUPTING RATINGS

The interrupting ratings of the controllers vary with the value of the utilization voltage. The following table depicts typical NEMA E1 (unfused) interrupting ratings for Class E1 controllers.

Table B.1 NEMA Class E1 Interrupting Ratings

Contactor Type and Rating	Interrupting Rating rms symmetrical (mVA)			
	2400 Volts	4200 Volts	5000 Volts	7200 Volts
CR193B 400 Amp	25	43	50	75
CR193D 400 Amp	25	43	50	—
CR193C 800 Amp	37	65	75	—

In addition to normal motor protective relays, NEMA Class E1 Limitamp control must include instantaneous overcurrent relays to signal the contactor to open on fault current. NEMA Class E1 Limitamp control may be employed on systems having available short-circuit currents up to the interrupting rating of the contactor.

Relaying, metering, ground fault protection and lightning arresters are typical of available modifications.

NEMA Class E2 Limitamp control incorporates the high-interrupting capacity of fast-acting fuses. These current-limiting fuses protect both the connected equipment and control against the high short-circuit current available from modern power systems. (See Table B.2.)

*Drawout available in two-high construction only



CR194 control is designed for operation on the following power systems.

Table B.2

System Distribution Voltage	Maximum Motor Hp ③		Interrupting Rating (mVA) Symmetrical 3- phase 50 or 60 Hz
	Induction, Wound-rotor Synchronous (0.8 PF)	Synchronous (1.0 PF)	
CR194 400 Ampere stationary and drawout			
2400	1600 ①	2000 ①	200
4200	2800 ①	3500 ①	350
4800	3200 ①	4000 ①	400
7200	4800 ①	6000 ①	600
CR194 800 Ampere stationary			
2400	3200 ②	4000 ②	200
4200	5600 ②	7000 ②	350
4800	6400 ②	8000 ②	400

① Based on 400 amperes RMS maximum, enclosed, NEMA 1, vented one-high

② Based on 800 amperes RMS maximum, enclosed, NEMA 1, vented one-high

③ For non-vented enclosures, apply a factor of 0.8 to the maximum horsepower

There are three basic constructions available utilizing the vacuum contactor:

- CR194 two-high 400 Amp
- CR194 one-high 400 Amp
- CR194 one-high 800 Amp

CR194 TWO-HIGH 400 AMP

The two-high construction has basic dimensions of 36" wide, 90" high and 30" deep, making it the industry's smallest. An optional 40-inch-wide enclosure is also available when additional cabling space is required. Bolted rigid frame construction provides an accurate and simple building platform, giving greater structural strength and flexibility. Full top and bottom compartment isolation is provided for greater safety, and the two-high construction is UL/CSA approved.

A door-in-door construction provides roomy low-voltage compartments, which offer flexibility, safety and high density. Large low-voltage door mounting surface permits multiple relays and metering packages, including drawout relays. The interior of the low-voltage compartment features a white mounting panel, which is easily accessible and provides ample space for numerous control options.

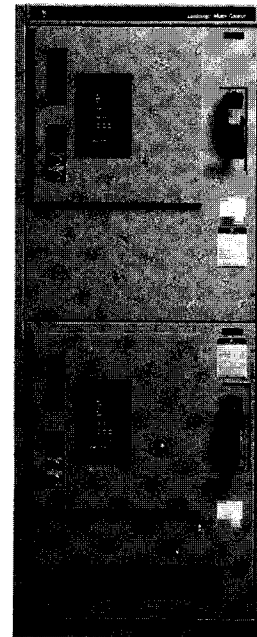


Figure B.1 CR194 two-high construction

The enclosure will accommodate outgoing cable sizes as shown in Table B.4 when both top and bottom compartments house contactors. There is also an option to use the top compartment as an incoming line section with limited cable sizes. Refer to the factory for details. Otherwise, an auxiliary section will be required.

It is not necessary to de-energize one controller to service or install the second controller. The enclosure is designed to safely permit termination of one set of motor leads while the other controller is energized.

Main horizontal power bus is available in 1000/1200 amperes and 2000 amperes. Both the main and vertical bus is epoxy-insulated and accessible from front and rear. The horizontal power bus will match with existing Limitamp lineups, including air-break units.

The current ratings are shown in Table B.3.

Table B.3 Ratings and Horsepower Limitations in CR194 Two-high

Contactor Location	Maximum Current		Horsepower			
			2400 Volts		4000-4800 Volts	
	Vented	Non- Vented	Vented	Non- Vented	Vented	Non- Vented
TOP	360	320	1600	1200	2800	2500
BOTTOM	400	320	1800	1200	3100	2500

B



Table B.4 Cable Size Limits (approximate) in CR194 Vacuum Control

Construction	With Non-shielded Cable		With Shielded Cable and Prefabricated Stress Cones		With Shielded Cable and Hand- wrapped Stress Relief	
	Per phase		Per phase		Per phase	
400-Ampere	Incoming	Load	Incoming	Load	Incoming	Load
One-high 26"-wide Case	1-500 kcmil	1-500 kcmil	1-500 kcmil	1-500 kcmil	1-500 kcmil	1-250 kcmil preferred 1-500 kcmil possible
One-high 34"-wide Case	2-500 kcmil	2-500 kcmil	2-500 kcmil	2-500 kcmil	2-500 kcmil	2-500 kcmil
Two-high 36"-wide Case	Contact Factory	1-500 kcmil	Contact Factory	1-250 kcmil preferred 1-500 kcmil possible	Contact Factory	1-#3/0 preferred 1-#4/0 possible
Two-high 40"-wide Case	Contact Factory	1-500 kcmil	Contact Factory	1-500 kcmil	Contact Factory	1-250 kcmil
800-Ampere						
One-high 48"-wide Case	2-750 kcmil	2-750 kcmil	2-750 kcmil	2-750 kcmil	2-750 kcmil	2-750 kcmil

CR194 ONE-HIGH 400-AMP

The one-high packaging (one contactor per enclosure) for the 400-ampere vacuum contactor has basic dimensions of 26 inches wide, 90 inches high, and 30 inches deep, including power bus. It is constructed from a welded enclosure to house a single vacuum contactor in the high-voltage compartment located at floor level. The entire upper compartment is available for low-voltage equipment and includes a swing-out panel for ease of component mounting and accessibility.

This enclosure will accommodate cable sizes as shown in Table B.4. Cable runs may enter from top or bottom without modification. Top or bottom cable entrance into the enclosure does not need to be specified.

The one-high design will accommodate the following combination of components:

1. One three-phase potential transformer used for metering.

2. Up to 10 kVA extra capacity CPT (34" wide only). 3 KVA max on two-high design.

3. Up to approximately 10 control relays for induction motor starters.

4. Two size S1 drawout relay cases.

A 34-inch-wide, one-high enclosure is available as an option, where more cable room or multiple cable connections are required. Power factor correction capacitors can also be supplied and will be mounted in an auxiliary enclosure.

CR194 ONE-HIGH 800-AMP

The one-high enclosure for the 800-ampere vacuum contactor has basic dimensions of 48" wide, 90" high and 30" deep in a welded frame. Maximum cable sizes are shown in Table B.4. Protected raceways isolate the motor and power leads from one another. Cable runs may enter from the top or bottom and are straight runs.



VACUUM CONTACTORS

The vacuum contactors supplied with Vacuum Limitamp are of the magnetically held type. They are fully rated at 400 or 800 amperes in accordance with NEMA and UL standards. The contactors differ in size, weight and method of termination. The vacuum interrupters are also different among the various models and are not interchangeable due to their different current ratings, and variations in interlock and wire harness mounting.

The contactor may be easily removed for service in each of the designs available, providing easy access for normal maintenance, such as vacuum interrupter wear checks and replacement of the operating coil, without removing the contactor. The only time the contactor needs to be removed is to replace a vacuum interrupter at the end of its service life or to adjust the vacuum interrupter for wear on the interrupter tips.

The standard contactors for industrial motor starters are closed by a single magnet and are held closed by the same magnet. This contributes to simplicity of mechanical design and increases the mechanical life of the contactor. Standard contactors may not need adjustment or mechanical repair for many years, primarily due to mechanical simplicity and sturdiness. However, preventive maintenance checks at least once per year are recommended.

Low voltage on the contactor operating coil of an electrically held contactor will cause the contactor to open. For most motor applications, it is desirable to disconnect the motor from the line when the system voltage is lost or lowered appreciably; therefore, the electrically held contactor is appropriate. The DC operating coil of the contactor is designed to be used with a holding circuit to limit coil current. The contactor coil is designed for use on 115 volts rectified AC or 125 volts DC.

For all NEMA Class E1 controllers, the contactor must be capable of interrupting the available short-circuit current. For these applications, instantaneous overcurrent relays must be used to interrupt the contactor coil current. See Table B.5 for additional technical specifications on the vacuum contactor.

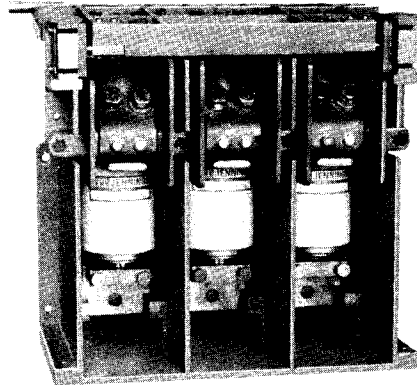


Figure B.2 400-Ampere Vacuum Contactor

LATCHED CONTACTORS

There are some applications where it is not desirable to disconnect the motor from the line during voltage depression. These applications are generally those associated with a critical drive where the continued rotation of the drive may be more important than possible damage to the motor from low voltage.

The mechanical latch maintains contactor closure under the most severe undervoltage conditions, including complete loss of voltage. Latched contactors may be specified if required by the application. The standard close and trip coils are designed for use on 120 volts rectified AC or 125 volts DC. Trip coils are also available in 24V, 48V and 220V. A manual release feature is provided as standard. Capacitor trip devices can also be used for release on the trip coils.

The Limitamp latched contactors are identical to the unlatched versions, with the exception of a small latch attachment mounted on the contactor, which slightly increases the depth of the contactor.

Latched contactors are interchangeable mechanically with the standard non-latched versions, both from latched to non-latched, and vice versa. However, in each case, it is necessary to change the wiring in the control circuit to the contactor coil or coils and to change the enclosure door to accommodate the manual latch release knob.



APPLICATION NOTES — VACUUM CONTACTORS

Switching Transients and Vacuum Contactors

B Voltage transients when transmitted downstream can be harmful to motor insulation systems. The transients occur in most electrical systems and are usually due to switching surges or lightning strikes. Vacuum contactor switching is only one source of voltage transients. For these reasons GE recommends that customers install surge capacitors and arresters at the motor terminals for vacuum as well as airbreak contactor applications. The surge capacitors reduce the steepness of the voltage transient wavefront, thus reducing the stress on the motor insulation.

Vacuum contactors have proven their suitability as a reliable and safe means of controlling motors, transformers, and capacitor loads. This has been demonstrated by a very good track record over a period of more than 10 years in Vacuum Limitamp equipment and much longer in GE Power-Vac switchgear equipment.

Also, an independent EPRI study, investigating the reliability of vacuum switching devices a number of years ago, concluded "... motors switched by vacuum devices had failure rates which are no higher than those for motors switched by air or air-magnetic devices."

Chopping Transients in Vacuum Limitamp

The vacuum switching device is among the best switching device available because it most frequently interrupts load currents in an "ideal" fashion — that is, when the load current is at a current zero. However, there is a probability that some switching operations may produce voltage transients due to chopping. Chopping is a phenomenon that occasionally occurs as the current through a contactor pole is interrupted during a contactor opening operation.

To understand the nature of chopping, a little understanding of what occurs as a vacuum contactor interrupts current is necessary. When the operating coil of a vacuum contactor is de-energized, kick-out springs in the contactor cause the armature to open and force the vacuum interrupter tips to part. Any current that is flowing through the tips at the instant of parting continues to arc across the open tips. This arcing continues until the sinusoidally varying current approaches zero. As the polarity reverses across the open tips, current ceases to flow because all charge carriers in the arc disappear dur-

ing the zero-crossing, leaving in its place a very high dielectric vacuum space. Chopping occurs just before the current zero crossing because the arc becomes unstable under the light current conditions and prematurely interrupts the current. The instantaneous level of current when this interruption occurs is called the "chop" current. The magnitude of the resulting voltage transients is the product of the "chop current" and the load surge impedance.

GE employs special metallurgy in its tip design to minimize chopping. The tip material consists of a sintered tungsten-carbide material that is impregnated with silver. The tungsten provides long life in hot arcing conditions, and the silver provides for low chop currents. In chop current tests performed on GE's 400 ampere vacuum contactors, it was found that the load surge impedance had significant effect on the average chop current. For example, tests with a surge impedance of 1000 ohms yielded average chop currents of 1.2 amperes but only 0.28 amperes with 4500 ohms surge impedance. These levels of chop currents cause little concern for motor insulation systems.

If motors are expected to be "jogged" or frequently switched-off while accelerating up to speed, surge suppressing devices discussed earlier should be seriously considered to minimize the effects of long term motor winding insulation degradation due to multiple re-ignition transients that can occur while interrupting motor inrush currents. Multiple re-ignitions are surges of arcing current across an opening vacuum interrupter tip that occur in the first few micro-seconds after the tips part. Multiple re-ignitions are virtually non-existent while interrupting normal motor running currents.

Vacuum Interrupter Integrity

The loss of interrupter integrity due to loss of vacuum is a potential concern because the vacuum interrupter ceases to act as an interrupter if vacuum is lost. Vacuum Limitamp interrupters are tested three times during the manufacturing process for vacuum integrity. Historically, this process has reliably eliminated loss of vacuum during normal product operation. To maintain integrity, annual hipot checks are recommended as part of a user's normal preventative maintenance practice. The recommended hipot test voltage is 20 kV AC RMS for the 400 ampere and 800 ampere contactors. The hipot procedures are described in equipment instructions GEH-5305.



AC vs. DC Hipot

The AC hipot is recommended for vacuum interrupters because DC hipot may indicate problems with a good interrupter. The reason for this is complex, but in essence there may be microscopic gap broaching “anomalies” across the open interrupter tips that the DC hipot cannot distinguish from real problems such as a loss of vacuum. AC hipot systems, on the other hand are able to “burn-off” these anomalies, allowing the good interrupter to recover (Normal contactor load currents will also burn-off these anomalies).

If it is desired to use a DC hipot on a vacuum contactor, it is important to recognize that the results may falsely indicate a bad bottle. Also, DC voltage levels should not be greater than 1.4 times the recommended AC RMS value in order to maintain a safe margin of voltage to X-ray emission. At 35kV small amounts of X-ray radiation may be emitted. The level of emission is well below the allowable levels established in ANSI 37.85-1972. Using DC hipot at 28 kV (1.4 x 20 kV AC RMS) does maintain a safe margin to X-ray emission.

Table B.5 Vacuum Contactor Technical Specifications

Ratings		CR193B CR193D	CR193C
Rated voltage (Volts)		5000 7200 ①	5000
Rated current (Amperes)		400	800
Short circuit interrupting current (kA) symmetrical		6.0 6.0	9.0
Class E1 mVA		50 75	75
E2 mVA	2400 volts	200	200
	3600 volts	300	300
	4160 volts	350	350
	4800 volts	400	400
	7200 volts	600 ①	—
Short-time current (amperes)			
30 seconds		2400	4800
1 second		6000	12,000
Impulse withstand (kV)		60	60
Dielectric strength 1 minute (kV)		13.25 18.2	13.25
Vacuum integrity test (AC RMS)		20 kV	20 kV
Switching frequency (Operations/hour)		1200	600
Mechanical life (Operations)		2 x 10 ⁶	1 x 10 ⁶
Electrical life (Operations)		1 x 10 ⁶	0.25 x 10 ⁶
Closing time (Maximum MS)		350	270
Opening time (Maximum MS) (Switched on DC side of rectifier)		50	55
Pick-up voltage (% of rated)		85% max	85% max
Drop-out voltage (% of rated)		10 - 65%	10 - 65%
Control voltage (Volts)		115 rect. AC	115 rect. AC
Control circuit burden (VA)			
Closing		175	550
Hold-in		30	110
Auxiliary contacts		20 ② maximum (N.O. or N.C.)	20 maximum (N.O. or N.C.)
Ratings	Current (amperes)	10	10
	Voltage (volts)	600	600
Switching	AC	6 amperes at 600 volts	6 amperes at 600 volts
	DC	1 ampere at 240 volts	1 ampere at 240 volts
Contactor weight lb (kg)		77 (35)	114 (52)
Standards applicable		UL 347 NEMA ICS 3, Part 2	UL 347 NEMA ICS 3, Part 2

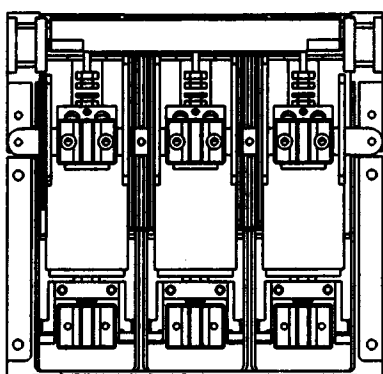
① CR193B only.

② Limited to 10 in two-high starter.



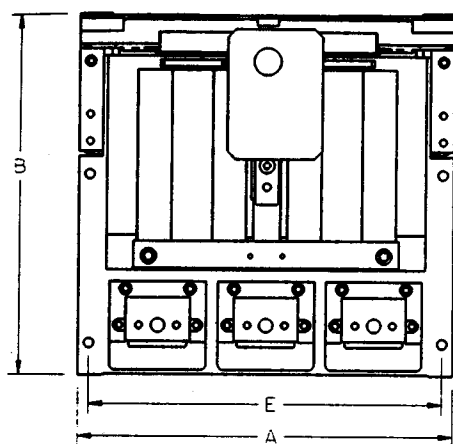
Table B.6 Contactor Dimensions in (mm)

Key	CR193B	CR193D	CR193C
A	14.88 (378)	14.88 (378)	18.90 (480)
B	13.50 (343)	13.50 (343)	16.93 (450)
C	14.65 (372)	14.65 (372)	17.52 (445)
D	10.24 (260)	10.24 (260)	12.99 (330)
E	12.99 (330)	12.99 (330)	17.00 (432)
F	8.48 (215)	8.46 (215)	11.02 (280)
G	1.18 (30)	1.18 (30)	1.38 (35)
H		1.93 (49)	

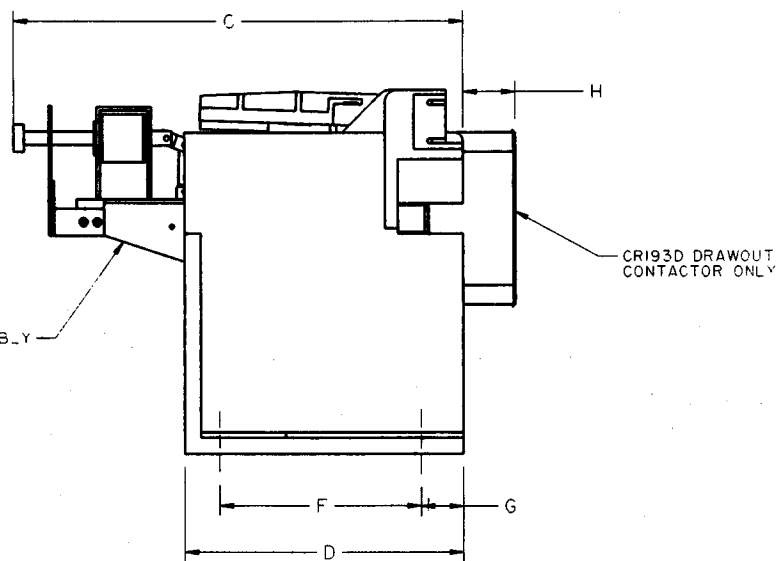


VIEW FROM INTERRUPTER SIDE

Figure B.3



VIEW FROM COIL SIDE



SIDE VIEW

Figure B.4

TRANSFORMER & CAPACITOR FEEDERS

Table B.7 is a listing of switching capacities for both transformer and capacitor loads. A more detailed discussion of these two applications is in the Section A.

Table B.7 CR194 Vacuum Switching Capacities (One-high)

8-hour Open Rating (Amperes)	System Voltage	3-Phase Transformers (kVA)	3-Phase Capacitors (kVAr)
400	2400	1600	1200
	4160	2800	2100
	4800	3200	2400
	7200	4800	3600
800	2400	3200	N/A
	4160	5600	
	4800	6400	

WEIGHTS AND DIMENSIONS

Vacuum Limitamp control varies in weight by controller type and construction. The approximate weight for estimating purposes is included in Table B.8.

All Limitamp controllers have a common depth of 30 inches and height of 90 inches. Overall width of controllers vary according to type of controller as shown in Table B.8.

Main horizontal power bus for electrically connecting sections of Limitamp control does not add to the standard 90-inch height.



Table B.8 Estimated Weights and Dimensions — CR194 Vacuum Controllers, NEMA 1 Vented Enclosure ①

Controller Type ② One High (One Starter) ⑤	Contactor Ampere Rating ③	2400 Volts			4000-4800 Volts ④			7200 Volts		
		Max Hp 3-Phase 50/60	Approx. weight in Lbs	Width in inches ⑥ (90 high x 30 deep)	Max Hp 3-phase 50/60	Approx. weight in Lbs	Width in inches ⑥ (90 high x 30 deep)	Max Hp 3-phase 50/60	Approx. weight in Lbs	Width in inches ⑥ (90 high x 30 deep)
Squirrel-Cage Induction Full-Voltage Nonreversing	400 800	1600 3200	1200 1400	26 48	2800 5600	1200 1450	26 48	4800 —	1200 —	34 —
Squirrel-Cage Induction Full-Voltage Reversing	400	1600	1500	58	2800	1500	58			
Reduced-Voltage Nonreversing Primary Reactor Type	400 400	1000 1600	2800 4800	58 98	1000 2800	2800 4800	58 98			
Reduced-Voltage Nonreversing Autotransformer Type (Closed Transition)	400 400 800	1000 1600 3200	3000 5000 5200	58 90 112	1000 2800 5600	3000 5000 5200	58 90 112			
Two-Step Part-Winding Nonreversing	400	1600	1400	58	2800	1400	58			
Two-Speed One-Winding FVNR	400	1600	1600	68	2800	1600	68			
Two-Speed Two-Winding FVNR	400	1600	1400	58	2800	1600	58			
Induction/Synchronous FVNR		0.8 PF	1.0 PF		0.8 PF	1.0 PF		0.8 PF	1.0 PF	
Synchronous Induction FVNR	400	1600	2000	1400	2500	3500	1400	4800	5500	1400
Brush Type & Brushless	800	3200	4000	2600	5600	7000	2600	—	—	—
Synchronous Motor, RVNR Primary Reactor	400 400	1000 1600	3000 5000	68 90	1000 2800	3000 5000	68 90			
Synchronous Motor, RVNR Autotransformer	400 400	1000 1600	1250 2000	3200 5200	76 108	1000 2800	1250 3500	3200 5200	76 108	
Induction/Synchronous Motor, RVNR								0.8 PF	1.0 PF	
Neutral Reactor	400							4800	5500	68

① See Enclosure & Bus Ratings Section E for NEMA 3R enclosures.

② For wound-rotor motor starter consult factory.

③ Derate by 0.8 for non-vented enclosures.

④ Maximum horsepower at 4160 volts AC in one-high NEMA 1 enclosure.

⑤ Two-high Starters are available in bolted-frame construction, available only for 400 ampere, squirrel-cage FVNR applications. Dimensions are 36" wide x 90" high x 30" deep. Weight is 2000 lbs.

⑥ Dimensions shown are approximate, based on standard motor designs.

B



CR7160 AIR-BREAK DRAWOUT

INTRODUCTION

Air-break Limitamp control is high-interrupting capacity high-voltage control used throughout industry to control and protect squirrel-cage, wound-rotor and synchronous motors. It can also be used to feed transformers and other power-utilization circuits.

Typical applications are in paper, steel, cement, rubber, mining, petroleum, chemical, and utility-type industries. Limitamp control is also typically used in water and sewage plants and public buildings for air conditioning, pumps and compressors.

FEATURES

- **Drawout construction** — Contactor and power fuses form a single drawout assembly. No cables to disconnect.
- **Unique swing-open contactor design** — The contactor is compact and has unique swing-open feature, providing quick inspection and maintenance.
- **400- or 700-ampere contactor** — Limitamp control meets the varying needs of industry including today's higher horsepower requirements.
- **One-, two- or three-high selectivity** — Limitamp control is available in either one-, two- or three-high enclosures to meet the needs of the application.
- **NEMA rated** — Limitamp control is fully rated and designed to meet the requirements of NEMA ICS 3, Part 2, for E2 controllers.
- **UL rated** — Limitamp control is fully rated and designed to meet the requirements of UL 347.
- **Built-in power bus** — Vertical power bus is a standard feature of Limitamp control. Horizontal power bus is available within standard 90-inch height and lines up with that of previous designs.
- **Installation ease** — Drawout construction; straight cable runs from top or bottom. Ample room to enter enclosure makes installation fast and easy.
- **Safe, simple operation** — A unique mechanical interlocking system is tied in with the ON-OFF position operating handle to provide sure and simple operation.
- **Dependable performance** — Limitamp control is coordinated to provide the required motor functions and offer reliable overcurrent protection against the damaging effects of overloads and short circuits.
- **Fast, easy maintenance** — Every component is accessible and removable from the front for simple inspection

and maintenance. The drawout contactor swings open for rapid contact tip and shunt inspection and maximum access when maintenance is required.

INTERRUPTING RATINGS

Limitamp control is designed to meet NEMA ICS 3, Part 2 and UL 347 requirements with a 60-kV BIL rating. It employs fast-acting current-limiting power fuses, a drawout air-break contactor rated either 400 amperes open (360 amperes, enclosed, NEMA 1, vented, one-high enclosure) or 700 amperes open (630 amperes, enclosed, NEMA 1, vented, one-high enclosure), and ambient-compensated overload relays for complete control and protection of motors used on modern power utilization systems with high available short-circuit currents.

The 400-ampere unfused contactors have an interrupting rating of 50 mVA; the 700-ampere unfused contactor, 75 mVA.

In addition to normal motor protective relays, NEMA Class E1 Limitamp control includes instantaneous overcurrent relays to signal the contactor to open on fault current, NEMA Class E1 Limitamp control may be employed on systems having available short-circuit currents up to the interrupting rating of the contactor.

Relaying, metering, ground fault protection, and lightning arresters are typical of available modifications.

NEMA class E2 Limitamp control incorporates the high-interrupting capacity of fast-acting fuses. These current-limiting fuses protect both the connected equipment and control against the high short-circuit current available from modern power systems.

CR7160 control is designed for operation on the following power systems.

Table B.9

System Distribution Voltage	Maximum Motor HP ①		Interrupting Rating (mVA) Symmetrical 3- phase 50 or 60 Hz
	Induction Wound-rotor Synchronous (0.8 PF)	Synchronous (1.0 PF)	
CR7160 400 amp			
2400 4800	1500① 2500①	1750① 3000①	200 400
CR7160 700 amp			
2400 4800	2500② 4500②	2750② 5000②	260 520

① Based on 360 amperes maximum, enclosed, NEMA 1, vented, one-high enclosure.

② Based on 630 amperes maximum, enclosed, NEMA 1, vented, one-high enclosure.



Table B.10 Horsepower Limitations in Multi-high Construction

Induction	2400 Volts		4000-4800 Volts	
	Amperes (per starter)	Hp (per starter)	Amperes (per starter)	Hp (per starter)
Three-high				
Vented	250	1000	250	1750
Non-vented	150	625	150	1000
Two-high				
Vented	310	1250	310	2500
Non-vented	210	875	210	2000

With one common design drawout contactor, CR7160 400 amp control is available in either one-, two- or three-high construction.

CR7160 700 amp control is available in one-high construction only.

BASIC CONSTRUCTION

Limitamp starters may be stacked multi-high (two- or three-high), where horsepower rating and need for metering and relaying is limited to allow stacking. See Table B.10 for horsepower and ampere limitations in multi-high construction. Non-stack design (one-high) is normally used for synchronous-motor starters, wound-rotor starters, and squirrel-cage induction starters, which have a considerable number of extra control functions, protective relays, and/or metering. All enclosures have the same bus location and may be connected together by bus splicing plates.

CR7160 ONE-HIGH 400 AMP

The one-high packaging (one 400 amp contactor per enclosure) has basic dimensions of 34 inches wide, 90 inches high and 30 inches deep, including power bus. It is constructed to house a single drawout contactor in the high-voltage compartment located at floor level. The entire upper compartment is available for low-voltage equipment and includes a swing-out panel for ease of mounting and accessibility.

This enclosure will accommodate cable sizes as shown in Table B.11. Cable may enter from top or bottom without modification. Top or bottom cable entrance in the enclosure need not be specified.

The CR7160 400 ampere one-high design will accommodate the following combination of components:

1. Synchronous static exciter up to 9 kW.
2. Two single-phase or one three-phase potential transformers.
3. Up to 10 kVA extra capacity CPT.
4. Up to approximately 20 control relays for induction starters.
5. Up to six size S1 drawout relay cases.

Power-factor-correction capacitors can be supplied and will be normally mounted in an auxiliary enclosure.

CR7160 TWO-HIGH 400 AMP

Two-high packaging accommodates two contactors in the enclosure, with basic dimensions of 44 inches wide, 90 inches high, and 30 inches deep. It is constructed in vertical sections of two space units each. Two FVNR induction starters may be housed in a vertical section.

Cable sizes which may be accommodated in a two-high design are reduced slightly from that which may be connected in the one-high design. (Refer to Table B.11 for cable size limitations.)

The enclosure is designed to safely permit termination of one set of motor leads while the other controller is energized. The two sets of motor cables are isolated from one another. Incoming power cable raceway is also isolated. All sets of cables may be brought into the starter from the top or the bottom.

Control relay space is available in a separate compartment with its own door and barriers. Approximately three extra control relays in addition to a ground fault relay and time-delay undervoltage protection can be mounted in the low-voltage compartment. One ammeter and switch, four push buttons, and four lights can be mounted on the low-voltage door. If no extra control relays are used, a watt hour meter can be mounted on the door.

CR7160 THREE-HIGH 400 AMP

Three-high packaging (up to three FVNR starters per enclosure) sharply reduces floor space requirements. It is constructed in vertical sections of three space units each. Each space unit is capable of housing one full-voltage, nonreversing squirrel-cage motor starter. You can purchase one or two starters per vertical section and add others later in factory-prepared space units. Although the enclosure is only 44 inches wide x 90 inches high x 30 inches deep (including power bus), an isolated motor-cabling compartment and an isolated incoming power-cabling compartment is included.



All starters must be de-energized to connect motor cable to any one starter.

Cable sizes are limited for motor connection.

Each starter unit has a low-voltage control compartment with separate access door located to the left of the high-voltage compartment.

One extra control relay, time-delay undervoltage protection and the ground fault relay can be mounted in the low-voltage compartment. Two push buttons, two lights, and one ammeter and switch can be mounted on the low-voltage door.

Note: Two-high and three-high constructions require power bus.

CR7160 ONE-HIGH 700 AMP

The one-high enclosure for CR7160 700-ampere control has basic dimensions of 42 inches wide, 90 inches high and 30 inches deep. This 42-inch enclosure has sufficient space to permit termination of two (2) 750 kcmil cables per phase with stress cones for power and motor leads. (See Fig. B.4.) Protected raceways isolate the motor and power leads from one another. Cable runs may enter from the top or bottom and are straight runs.

The 42-inch wide one-high enclosure is available as an option on the CR7160 400-ampere where more cable room or multiple cable connections are required.

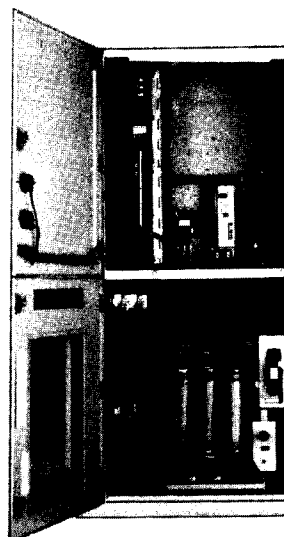


Figure B.5 CR7160 700 amp control with (2) 750 kcmil motor cables per phase, entering from bottom

Table B.11 Cable Size Limits (Approx.) in CR7160 Air-break Control

Construction	With Non-shielded Cable		With Shielded Cable and Prefabricated Stress Cones		With Shielded Cable and Hand-wrapped Stress Relief	
	Per Phase		Per Phase		Per Phase	
400-Ampere	Incoming	Load	Incoming	Load	Incoming	Load
One-high 34" wide Case	2-500 kcmil	1-500 kcmil	1-500 kcmil	1-500 kcmil	1-500 kcmil	1-250 kcmil Preferred 1-500 kcmil Possible
Two-high 44" wide Case	2-500 kcmil	1-500 kcmil	1-500 kcmil	1-250 kcmil Preferred 1-500 kcmil Possible	1-500 kcmil	1-#3/0 Preferred 1-#4/0 Possible
Three-high 44" wide Case	2-500 kcmil	1-500 kcmil	1-500 kcmil	1-#3/0 Preferred 1-250 kcmil Possible	1-500 kcmil	1-#2/0 Preferred 1-#4/0 Possible
700-Ampere						
One-high 42" wide Case ①	2-750 kcmil	2-750 kcmil	2-750 kcmil	2-750 kcmil	2-750 kcmil	2-750 kcmil

① Can be supplied as option on 400-ampere Limitamp control when more cable space is required

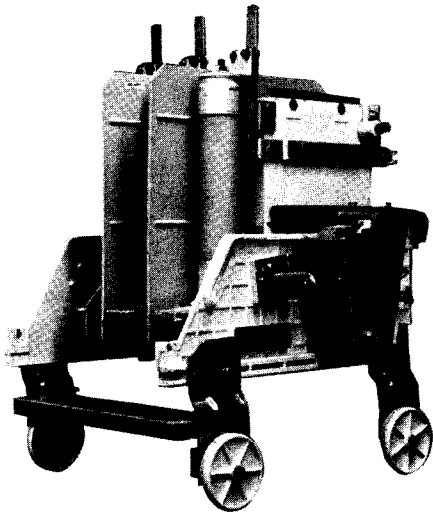


Figure B.6 CR7160 400-ampere air-break contactor is fully rated and completely roll out or drawout

DRAW OUT AIR-BREAK CONTACTORS

The air-break contactor normally furnished on Limitamp control is of the magnetically held-in type. It is drawout and fully rated at 400 or 700 amperes (eight-hour open rating) in accordance with NEMA and UL standards. Both the 400- and 700-ampere contactors have the same basic design but with current-carrying parts of different capacity. This uniquely constructed contactor can actually be swung open, exposing all integral parts for rapid inspection and maintenance. Power fuses are combined with the contactor to form a single assembly which is completely drawout without disconnecting cables.

In one-high Limitamp control, the drawout contactor, which may be rated 400 or 700 amperes, is mounted on wheels and can be easily rolled out of or into the floor-level high-voltage compartment. The contactor can be swung open after simple removal from the enclosure.

The DC operating coil of the contactor is designed to be used with a holding impedance that is inserted after the contactor is fully closed to limit coil current. The contactor coil is designed for use on 120 volts AC (rectified) or 125 volts DC control source.

Two- and three-high Limitamp control uses the 400-ampere contactor only. It is mounted on slide rails for easy removal and can be swung open within the enclosure from its drawout inspection position. Normal inspection and maintenance is done with the contactor in the enclosure. A contactor lifting table is available for contactor removal during installation.

The standard contactors for industrial motor starters are closed by a single magnet and are held closed by the same magnet. This contributes to simplicity of mechanical design and increases the mechanical life of the contactor. Mechanical latch contactors are available as an option and are explained on page B4.

See Table B.14 for additional technical specifications on the air magnetic contactors.

WEIGHTS AND DIMENSIONS

Limitamp control varies in weight by starter type and construction. The approximate weight for estimating purposes is included in the Table B.12.

All Limitamp control has a common height of 90 inches and a common depth of 30 inches. However, the overall width varies with type of Limitamp and is included in Table B.12.

For convenience in handling and installation, Limitamp control is equipped with removable lifting angles or lugs.

Power bus for electrically connecting sections of Limitamp control does not add to the standard 90-inch height.

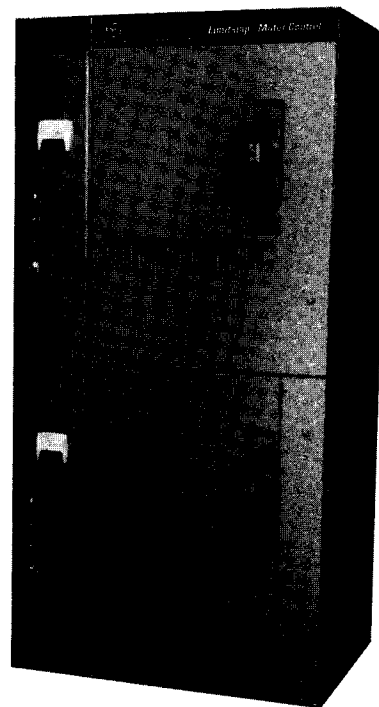


Figure B.7 CR7160 two-high construction



Table B.12 Estimated weights and Dimensions — CR7160 Air-break Controllers, NEMA 1 Vented Enclosures

Controller Type	Contactor Ampere Rating	Max HP 3-phase 50/60		2400 Volts		4800 Volts	
				Approx. weight (lb.)	Width in inches (90 high x 30 deep)	Approx. weight (lb.)	Width in inches (90 high x 30 deep)
Squirrel-cage Full-voltage non-reversing	Three-high sections						
	400	1000 1750		2600	44	2600 2600	44 44
	Two-high sections						
	400	1250 2500		2400	34	2400	44 44
	One-high sections						
	400	1500 2500		1600	34	1600 1600	34 34
	700	4500		2400	42	2400	42
Squirrel-cage Full-voltage Reversing	400	1500 2500		2200	66	2200 2000	34 34
	700	4500		3200	74	3200	74
Squirrel-cage Reduced-voltage Non-reversing Primary Reactor	400	100 400 1000 1500 2500		2700 2900 3400 4800	66 66 66 66	2700 2900 3400 4800 5400	66 66 66 98 98
	700	4500		8400	118	8400	118
Squirrel-cage Reduced-voltage Non-reversing Autotransformer	400	100 400 1000 1500 2500		2900 3100 3600 5000	98 98 98 130	2900 3100 3600 5000 5600	98 98 98 130 130
	700	4500		9200	140	9200	140
Wound-rotor Non-reversing	400	150 400 700 1000 1500 1750 2250 2500		2200 2600 2800 3600 4000	66 98 98 162 194	2200 2600 2800 3600 4000 4400 4700 5200	66 98 98 162 194 226 258 290
	700	1750 4500		6100 7000	230 262	7900 7900	294 294
Synchronous Full-voltage Non-reversing		0.8pf	1.0pf				
	400	1500 2500	1750 3000	2000	34	2000 2000	34 34
	700	4500	5000	2800	42	2800	42



TRANSFORMER & CAPACITOR FEEDERS

Table B.13 is a listing of switching capacities for both transformer and capacitor loads. A more detailed discussion of these two applications is in Section A.

Table B.13 CR7160 Air-break Switching Capacities (One-high)

System Voltage	3-Phase Transformers (kVA)	3-Phase Capacitors (kVA)
400 amp contactor		
2400	1500 ①	1100
4800	2500 ①	1800
5500	3000	2250
6000	3000	2250
6600	3750	2800
6900	4000	3000
7200	4000	3000
700 amp contactor		
2400	2500 ②	1800
4800	4500 ②	3375

① Based on 360 amperes maximum, NEMA 1, vented, one-high enclosure.

② Based on 630 amperes maximum, enclosed, NEMA 1, vented, one-high enclosure.

MULTI-HIGH CONSTRUCTION

Use the HP and current rating of Table B.10 for transformer kVA.

Use 0.75 times the transformer rating for capacitor feeder rating.

Table B.14 Air-break Contactor Technical Specifications

Ratings	IC 302 Air Magnetic	IC 302 Air Magnetic
Rated Current (Amperes) (open rating)	400	700
Rated voltage (Volts)	5000	5000
Short circuit interrupting current (kA)	6.0	9.0
Class E1 mVA	50	75
Class E2 mVA	2400 V 4200 V 4800 V	200 350 400
Short-time current (amperes)	30 seconds 1 second	2160 5400
Impulse withstand (kV)	60	60
Dielectric strength 1 minute (kV)	13.25	13.25
Switching frequency (Operations/hour)	600	600
Mechanical life (Operations)	1 x 10 ⁶	1 x 10 ⁶
Electrical life (Operations)	2.5 x 10 ⁵	2.5 x 10 ⁵
Closing time (Maximum MS)	120	120
Opening time (Maximum MS) (Switched on DC side of rectifier)	100	100
Pick-up voltage (% of rated)	85% max	85% max
Drop-out voltage (% of rated)	10-65%	10-65%
Control voltage (Volts)	115 rect. AC	115 rect. AC
Control circuit burden (VA)	Closing Hold-in	2000 150
Auxiliary contacts Quantity	12 maximum (N.O. or N.C.)	12 maximum (N.O. or N.C.)
Ratings Current (amperes)	10	10
Voltage (volts)	600	600
Switching AC	6 amperes at 600 volts	6 amperes at 600 volts
DC	1 ampere at 240 volts	1 ampere at 240 volts
Contactor weight Lb(kg)	275(125)	300(136)
Outline dimensions drawing	Figure B.8	Figure B.9
Standards applicable	UL 347 NEMA ICS 3, Part 2	UL 347 NEMA ICS 3, Part 2

B



B

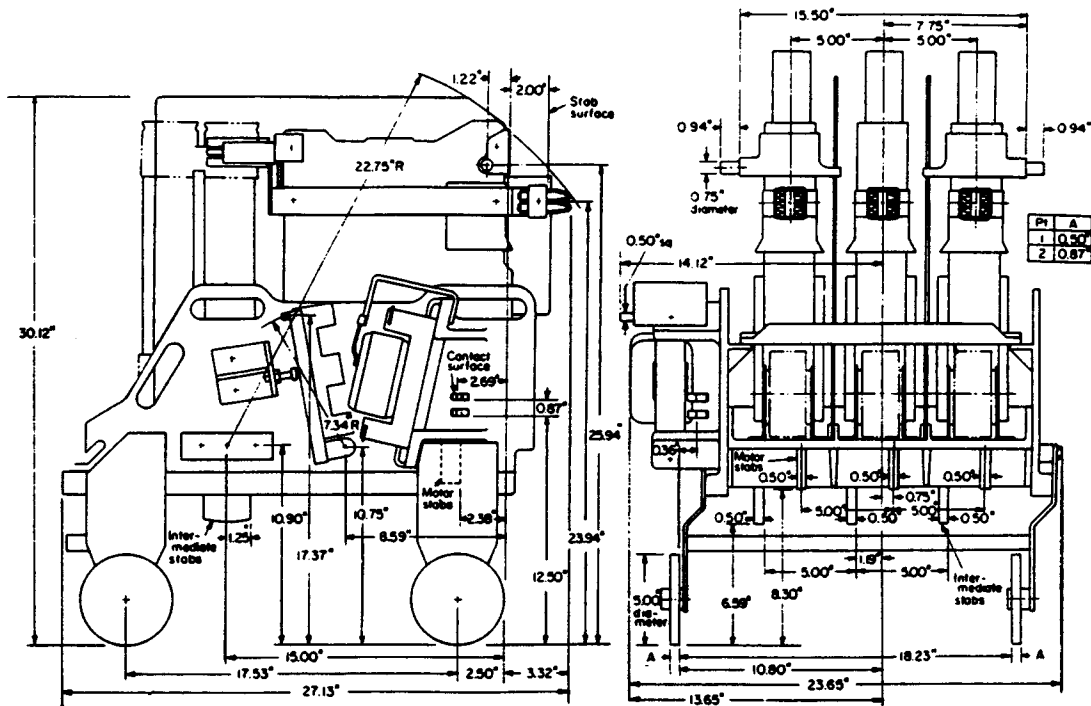


Figure B.8 Standard contactor 400 amperes, with wheels, fuse clips, and stab connections. (No fuses included). Weight 275 pounds applicable to one-high controllers

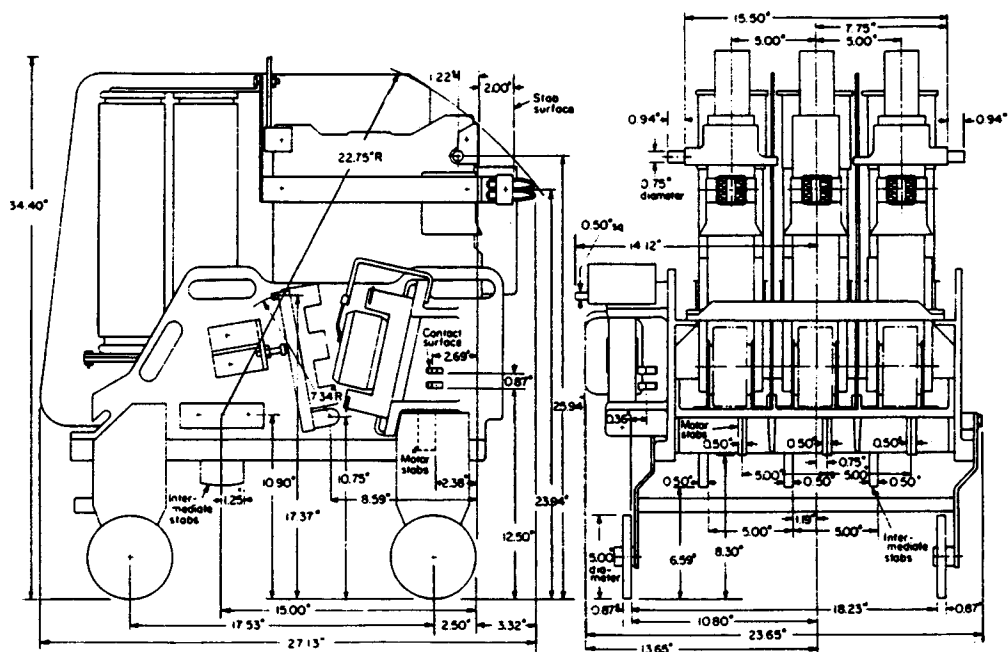


Figure B.9 700-amperes contactor with bolted fuses, stab connections and wheels. Weight 300 pounds



INTRODUCTION

IC1074 load-break switches are manually operated triple-pole, single-throw disconnecting switches with an integral interrupter and stored-energy spring that has the capability of interrupting magnetizing and load current within the ratings shown in Table C.1. They are designed and tested to comply with the performance requirements of ANSI Specification C37.57 and C37.58.

The IC1074 600-ampere drawout switch is designed for stab connection at line and load terminals. This switch must be fused. Current-limiting fuses are available up to a continuous rating of 630 amperes for installation in the switch.

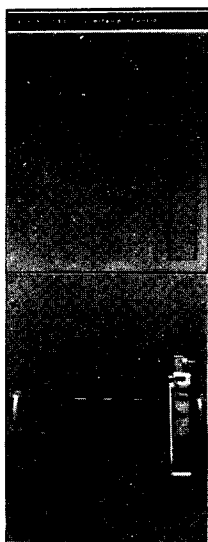


Figure C.1 600-ampere drawout load-break switch

The switch is designed to accommodate the bolt-on version of the current-limiting fuse, but clip mounting is available. Construction may be either one- or two-high, with one-high in a rollout design instead of drawout. Either two switches or a combination switch and 5kV air-break starter can be mounted in a two-high enclosure.

The IC1074 stationary switch (600- or 1200-ampere) is designed for mounting in one-high construction only. It contains line- and load-terminal pads for bolting incoming and outgoing conductors directly to the switch. It may be supplied fused or unfused. If supplied as an unfused switch, an upstream circuit breaker with instantaneous trips must be available to coordinate with switch capabilities — or the switch must be supplied with key lock capabilities — for all of the Limitamp starters in the

lineup. For the 1200-ampere switch, fuses are available up to 960 amperes continuous. These large fuses must be applied as line protectors for short circuit only, relying upon branch circuits or backup overload protection by other means.

Drawout switches must be applied as feeders only. The fixed mounted switches may be used as incoming switches or feeder switches.

These switches are designed specifically for use with Limitamp control. They are available with 1000- or 2000-ampere AC main power bus within the enclosure for easy lineup with Limitamp starters.

Other features of these switches are:

- Viewing window to see condition and position of switch blades.
- Blown-fuse indicator that can be seen through view window.
- Bolted fuses available for maximum reliability.
- High reliability interruption.
- Available with key-type interlocks. Maximum of three keys per position (lock open or lock closed).
- Outside door interlocked directly to shaft to prevent opening with switch energized.
- Externally operated handle that activates spring-charged quick-make/quick-break mechanism.
- Easy inspection.
- High mechanical life.



Table C.1 IC1074 Load-break Switch Technical Specifications

Type	600-Ampere Drawout Switch (Fuse)	600-Ampere Stationary Switch (Fused or Unfused)	1200-Ampere Stationary Switch (Fused or Unfused)
Ratings			
Maximum nominal rating	4760 volts	4760 volts	4760 volts
Unfused rating			
Vented enclosure	N/A	600 amperes	1200 amperes
Non-vented enclosure	N/A	540 amperes	1020 amperes
Fused rating			
Vented enclosure	600 amperes	600 amperes	960 amperes
Non-vented enclosure	540 amperes	540 amperes	840 amperes
Make/Break rating	600 amperes	600 amperes	1200 amperes
Fault-closing rating (asym)			
Fused	61,000 amperes	61,000 amperes	61,000 amperes
Unfused	N/A	61,000 amperes	61,000 amperes
Momentary rating (asym)			
Unfused	N/A	61,000 amperes	61,000 amperes
Basic impulse level (BIL)	60 kV	60 kV	60 kV
Short-circuit interrupting capacity (fused)			
2400 volts	200 mVA (sym)	200 mVA (sym)	200 mVA (sym)
4800 volts	400 mVA (sym)	400 mVA (sym)	400 mVA (sym)
Dimensions			
	Dimensions in inches (W x H x D)	Dimensions in inches (W x H x D)	Dimensions in inches (W x H x D)
One-high construction	34 x 90 x 30	38 x 90 x 30	38 x 90 x 30
One-high construction (option)	42 x 90 x 30	N/A	N/A
Two-high construction	44 x 90 x 30	N/A	N/A
Cable space			
Incoming 38"-wide case	N/A	2-500 kcmil per phase with or without stress cones	2-500 kcmil per phase with or without stress cones
Outgoing 38"-wide case	N/A	2-500 kcmil per phase with or without stress cones	2-500 kcmil per phase with or without stress cones
Incoming (for bus only) 34"-wide case	2-500 kcmil per phase without stress cones 1-500 kcmil per phase with stress cones	N/A	N/A
42"-wide case	2-750 kcmil per phase with or without stress cones	N/A	N/A
44"-wide case	1-500 kcmil per phase with or without stress cones	N/A	N/A
Outgoing 34"-wide case	1-500 kcmil per phase with or without stress cones	N/A	N/A
42"-wide case	2-750 kcmil per phase with or without stress cones	N/A	N/A
44"-wide case	1-300 kcmil per phase with or without stress cones	N/A	N/A



CABLE-ENTRANCE COMPARTMENT

When incoming cable exceeds limits shown in the cable size limits tables, an optional cable-entrance compartment is required.

TRANSITION COMPARTMENT

Limitamp control can be close-coupled to transformers and switchgear by a transition compartment to make a continuous lineup. The transition compartment is normally 22 inches wide; however, this can vary. See Table D.1.

BUS ENTRANCE COMPARTMENT

Bus entrance compartments are required in all cases where power is fed to the controller lineup by means of bus. See Table D.1.

CABLE TERMINALS

Terminal lugs for both line and load cables are not supplied unless specified.

Clamp-type lugs or NEMA 2-hole compression-type lugs can be supplied as options.

The customer must specify the number and size cable when lugs are to be supplied by GE.

Where aluminum cable is to be used, special attention must be given to terminal selection.

HIGH-RESISTANCE GROUNDING EQUIPMENT

IC9181 high-resistance grounding equipment can be mounted in an enclosure which will match and line up with Limitamp dimensions and bus location.

For description of high-resistance grounding equipment, refer to GE publication GEP-345.

Note: Order GEP-345 from:

**General Electric Company
Drive Systems Department
1501 Roanoke Blvd.
Salem, VA 24153**



Table D.1 General Guidelines for Incoming Line

Incoming Line	Maximum Cable Size per Phase	Enclosure Width	Typical Device Devices That Can Be Included
Cable Compartment	Top Entry 4-500 kcmil	22"	VM, VMS, 2 stationary PTs, lightning arresters and surge capacitors
Cable Compartment	4-750 kcmil	32"	All of the above plus 3 CTs, AM, and AMS
Cable Compartment	4-750 kcmil	38"	All of the above plus D/O PTs can replace the stationary PTs. 1 D/O CPT can be mounted.
Cable Compartment	Bottom Entry Same as top entry except a D/O CPT cannot be mounted in the enclosure		
Bus Entrance Compartment	N/A	32"	Same as 32"-wide cable compartment
Transition to GE Switchgear	N/A	22"	VM, VMS, 2 stationary PTs, lightning arresters and a surge capacitor
Transition to GE Transformer	N/A	22"	Accessories cannot be mounted in transformer transition. Additional auxiliary enclosure is required.
Load-break Switch Fused or Unfused	2-500 kcmil top or bottom	38"	AM, AMS, 3-CTs, 2-stationary PTs, VM, VMS
Load-break Switch Fused or Unfused	2-500 kcmil top or bottom	38" and 22" auxiliary enclosure	Same as 38" switch plus lightning arresters, surge capacitors and switchgear relay can be mounted in the 22" wide enclosure
Load-break Switch Fused or Unfused	2-500 kcmil top or bottom	38" and 38" auxiliary enclosure	Same as 38" switch except D/O PTs can be mounted in the auxiliary enclosure plus switchgear relays



ENCLOSURES

NEMA TYPE 1 — GENERAL PURPOSE

The NEMA Type 1 is the standard Limitamp enclosure designed primarily to prevent accidental contact with control apparatus. This enclosure is suitable for general purpose indoor applications with normal atmospheres.

For CR194 two-high design with vented enclosures, add 2½" to the height.

NEMA TYPE 1A — GASKETED

The NEMA Type 1A rubber-gasketed enclosure is a dust-resistant enclosure (not dust-tight), designed to give protection against dust, and when control devices are properly selected, to give proper operation in a dusty atmosphere. It is recommended for all moderately dusty atmospheres, especially in those industries whose dust are abrasive, conductive, or form high-resistance contacts. NEMA Type 1A rubber-gasketed enclosures are not provided with steel bottoms. It is expected that the case will sit on concrete, effectively sealing the bottom against dust.

NEMA TYPE 2 — DRIPTIGHT

This enclosure is made to protect control apparatus against falling moisture or dirt. All openings are rubber-gasketed and provided with doors or covers. It is intended for use in atmospheres where condensation is heavy or where quantities of water are used in a process or for cleaning. (For applications where a hose is to be directed on the equipment from any direction except above, use NEMA Type 4.) Normal instruments, meters and devices are mounted on the door as in NEMA Type 1. Strip heaters are used only as the application requires them.

NEMA TYPE 3R — WEATHER-RESISTANT

These enclosures must be suitable for outdoor installation and offer protection against driving rain and snow storms, as well as against dust. Limitamp NEMA 3R enclosures are provided with solid-steel bottoms and tops, an overhanging sloping roof and strip heaters, with provisions for future extension.

The following types of NEMA 3R enclosures are available:

- NEMA Type 3R, weather-resistant, full-height cover door, non-walk-in (42 inches deep by 101 inches high). (Use when a number of devices are on the door.)
- NEMA Type 3R, weather-resistant walk-in (92 inches deep by 111½ inches high).

Walk-in enclosures allow ample space for inspection and maintenance of starters within the enclosure.

Standard construction is suitable for wind velocities of 130 mph and roof loading up to 30 pounds per square

foot. Exterior finish is applied by an electro-static powder coat process (polyester based).

NEMA TYPE 4 — WATERTIGHT

This enclosure must withstand the hose test as described in NEMA standards and must preclude the entry of water under such test. It is intended for use in installations such as dairies or paper mills where cleaning is done with hoses.

Strip heaters are furnished.

NEMA TYPE 12 — DUSTTIGHT

These cases are designed to meet the requirements of industrial locations where protection is required against entrance of fibers and flying lint, dust, dirt, light splashing, seepage dripping and external condensation of non-corrosive liquids.

Typical requirements for NEMA 12 are:

- A gasketed cover that is hinged to swing horizontally, and held in place with screws, bolts or other suitable fasteners.
- No open holes through the enclosure. All openings are sealed with gasketed cover plates.
- No conduit knockouts or knockout openings.
- Steel bottom.

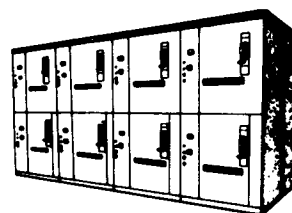
INDOOR ENCLOSURE CONSTRUCTION

Limitamp indoor enclosures are manufactured from 12-gauge steel throughout, except for 13-gauge on the rear covers. For surface preparation, see the Application Data section.

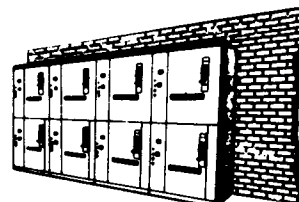
CHOICE OF MOUNTING — INDOOR

You may select either back-to-back (60 inches deep) or back-to-wall (30-inches deep) mounting, letting you arrange control lineups to your own floor space and application requirements.

Back-to-back mounting



Back-to-wall mounting



E



Table E.1 Enclosure dimensions

Type	Description	Page
NEMA 1 motor starters	CR194 Vacuum Stationary and Drawout, Bolted Construction	
	400A, 2-high, 36" wide	E4
	400A, 2-high, 40" wide	E5
	CR194 Vacuum Stationary, Welded Construction	
	400A, 1-high, 26" wide	E6
	400A, 1-high, 34" wide	E7
	800A, 1-high, 48" wide	E8
	CR7160 Air-break Drawout, Welded Construction	
	400A, 1-high, 34" wide	E9
	400A, 2-high, 44" wide	E10
NEMA 3R motor starters	400A, 3-high, 44" wide	E11
	700A, 1-high, 42" wide	E12
	CR194 400A and 800A, 1-high, non-walk-in	E13
	CR194 400A, 1-high, walk-in	E14
	CR194 800A, 1-high, walk-in	E15
	CR7160 400 1-and 2-high, non-walk-in	E16
	CR7160 400A 1- and 2-high, walk-in	E17
IC1074 load break switches	CR7160 700A, 1 high, walk-in	E18
	Estimated widths	E19
	NEMA 1, 38" wide	E20
	NEMA 3R, 42" deep, non-walk-in	E21
	NEMA 3R, 92" deep, walk-in	E22

NAMEPLATES

Enclosure nameplates are provided for identification on front panels and internally for identifying units and devices.

Standard unit nameplates are 1" x 3" 2-ply thermoplastic, black letters on white background or white letters on black background.

Front panel device nameplates are 1/2" x 1 1/2" thermoplastic.

Internal device nameplates are fabric type with adhesive backing.

Thermoplastic nameplates are fastened with corrosion-resistant steel screws.

Table E.2 Enclosure features

Description	NEMA 3R Non-walk-in 42" deep	NEMA 3R Walk-in 92" deep
Strip heater	Standard ①	Standard ②
Thermostat	Option	Standard
Receptacle	Option	Standard
Incandescent light	Standard	Standard
Undercoat	Standard	Standard
Door stops	Standard	Option
Floor sills	Standard	Standard

① In starter only

② One in starter, one in aisle

LIMITAMP BUS SYSTEMS

AC power bus is used for conducting power throughout a group of starters joined together in a lineup. Incoming power cable can be terminated at one or more points in the lineup and the power bus employed to distribute power throughout the length of the group.

This bus is available in ratings of 1000 and 2000 amperes and may be tin-plated copper, silver-plated copper or bare copper. For higher ratings refer to factory. Derating is necessary in certain applications. The horizontal bus compartment is located within the standard 90-inch-high enclosure in the same position as in current and previous air-break designs, dating back to 1960, making all compatible. Limitamp horizontal bus is rated 60kV basic impulse level (1.2 x 50 µ sec wave). Mechanical strength under short-circuit currents is 50 kA RMS symmetrical.

GROUND BUS

Ground bus in a Limitamp lineup provides a low-resistance path between ground connection points in any group of controllers. This low-resistance path is a bus bar and is for the purpose of decreasing to a low value a possibly hazardous voltage difference between grounding points in the starter group. These voltage differences would occur under ground fault conditions if a low-resistance ground path were not provided.

The ground bus is normally located near the AC power bus on the inside rear of the enclosure. The bus provides a common termination point for all ground connections within each controller, including the enclosing case, and offers a convenient terminal for incoming ground cables. It should be noted that the customer must make a suit-



suitable ground connection to the bus in order to make it effective. When ground bus is not provided, the ground connection may be made to the ground stud provided.

Extensions to the ground bus are located in the incoming line cable compartment and near the load termination points in the high-voltage compartment to make grounding cable shield terminations easy to accomplish.

CONTROL BUS

Control bus is a convenient means of conducting control power throughout a group of controllers joined together in a lineup. Conductors from a single control power source may be terminated in one unit in the lineup and the control bus employed to distribute the power to each unit of the grouped lineup. Control bus may also be used to distribute the power from a single control transformer located in the lineup.

Control bus normally consists of properly sized insulated wire conductors run between terminal boards.

Standard voltage for control bus is 120 or 240 volts AC and maximum current rating is determined by application, such as total present and anticipated future load.

POTENTIAL BUS

Potential bus is a means of distributing a common source of low voltage throughout the lineup for metering and instrumentation. Potential bus consists of properly sized wire connected between terminal boards typically mounted on the top inside of enclosure. Maximum voltage is 600 volts.

INSULATED POWER BUS

Insulating the AC power bus reduces the possibility of bus faults from causes such as surge voltages, ionized vapors, falling objects (tools, etc.), ground tapes, etc. It also prevents corrosion and oxidation of the bus and its hardware.

The standard power bus consists of bar conductors on insulator supports. Insulation for the conductors can be provided, and it may consist of various types of insulating material, such as 130°C HV rubber splicing tape or other material dictated by availability and individual job requirements.

The CR194 two-high Vacuum Equipment design uses epoxy-insulated main and vertical bus as standard.

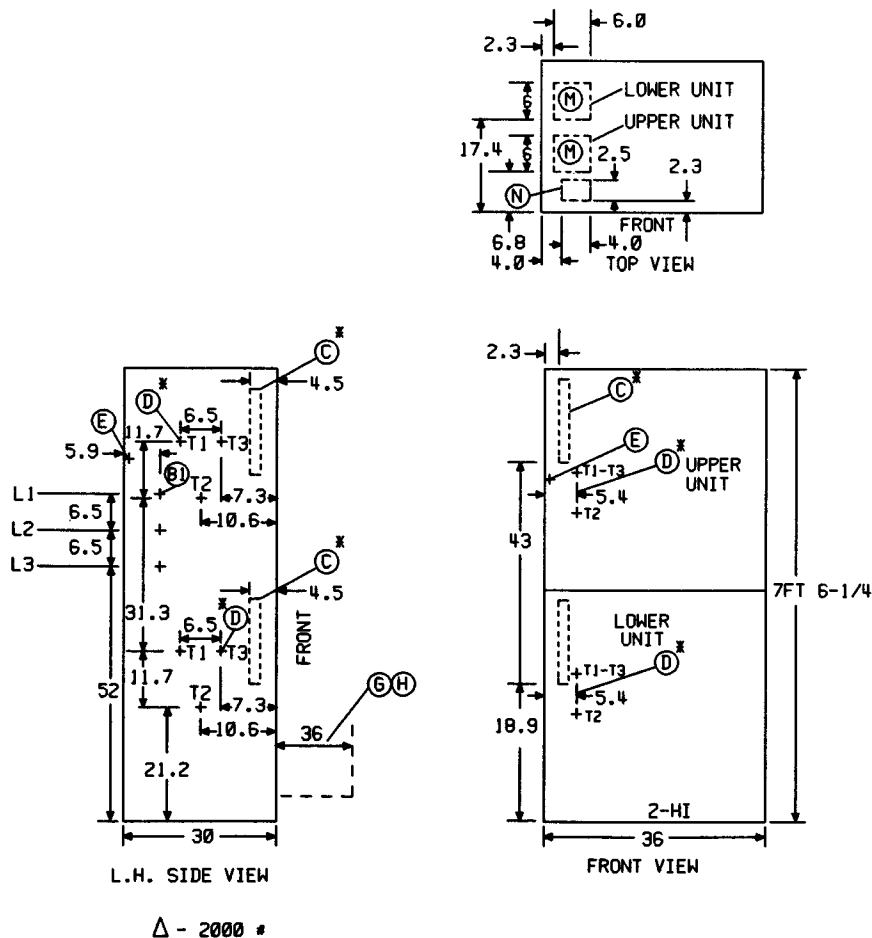
Table E.3 Bus cross section

Bus type	Rating	Cross section
Main bus	1000A ^①	¼" x 3" copper
	2000A	(2) ¼" x 3" copper
Vertical bus	400A	¼" x 1" copper
	700A	½" x 1" copper
	800A	¼" x 3" copper
Ground bus	400A	¼" x 2" copper
	600A	¼" x 2" copper

① Refer to factory for 1200A applications.



ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS
CR194 400-ampere Vacuum Stationary or Drawout (Two-high)
Standard 36" Wide



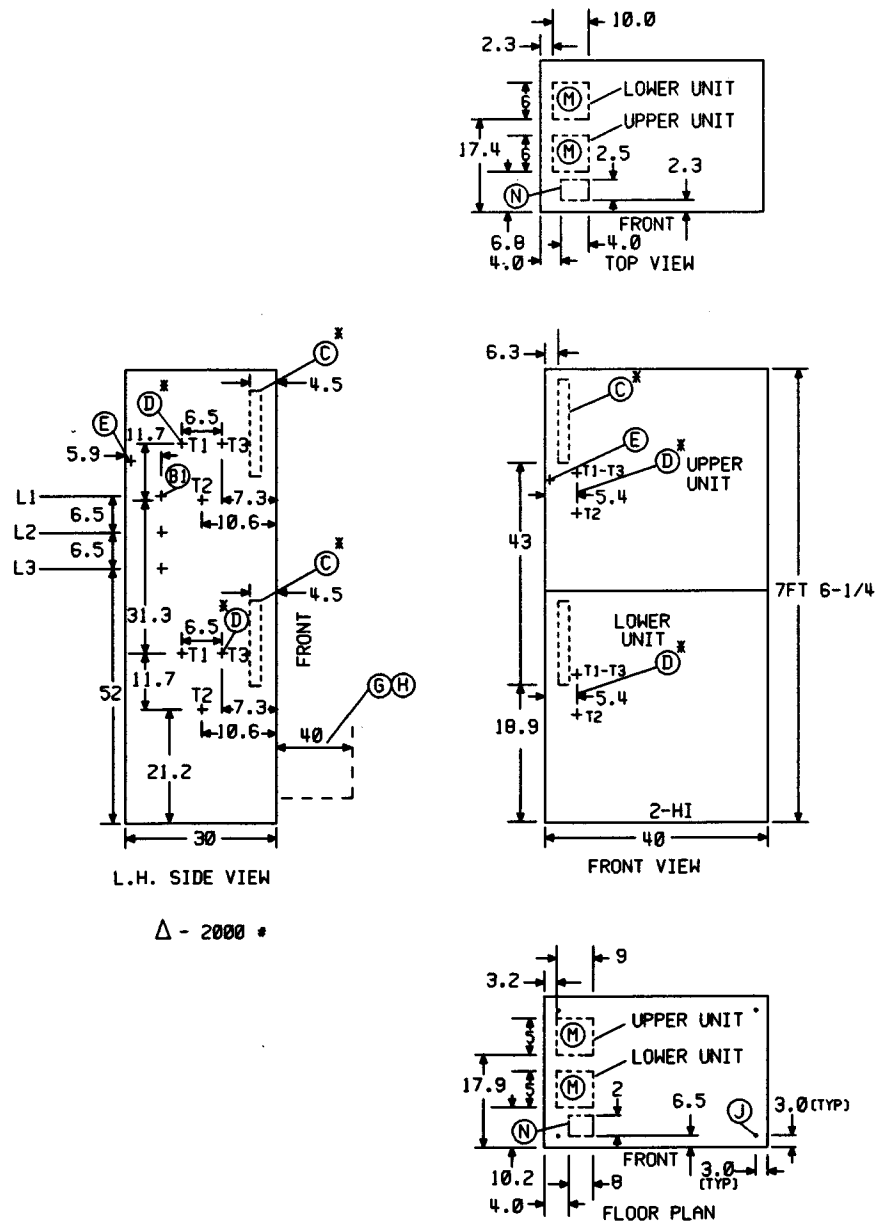
Notes:

- B1 — AC Power Bus
- C — Control Lead Terminal Board
- D — Motor Lead Terminal Connection
- E — Ground Bus Terminal Connection
- G — Space Required to Open Doors 90°
- H — Four-foot Aisle for Contactor Removal
- J — Mounting Holes for 1/2" Diameter Anchor Bolts
- M — Recommended Position for Incoming Motor Conduit
- N — Recommended Position for Incoming Control Conduit
- * — Indicates Terminal Location — Approximate for Cable Length
- Δ — Approximate Weight



ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

**CR194 400-ampere Vacuum Stationary or Drawout (Two-high)
Optional 40" Wide**



△ - 2000 #

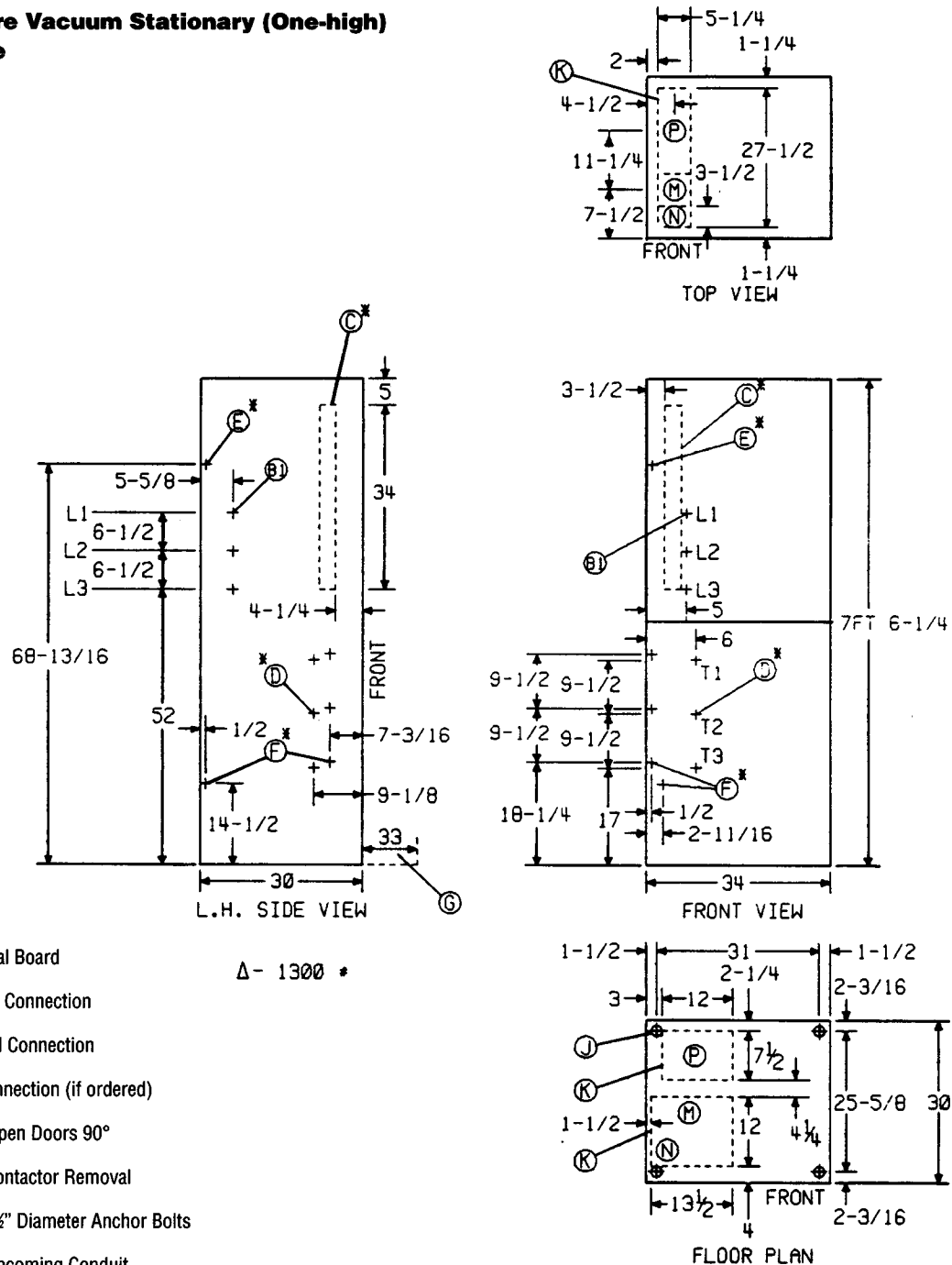
Notes:

- B1 — AC Power Bus
- C — Control Lead Terminal Board
- D — Motor Lead Terminal Connection
- E — Ground Bus Terminal Connection
- G — Space Required to Open Doors 90°
- H — Four-foot Aisle for Contactor Removal
- J — Mounting Holes for 1/2" Diameter Anchor Bolts
- M — Recommended Position for Incoming Motor Conduit
- N — Recommended Position for Incoming Control Conduit
- * — Indicates Terminal Location — Approximate for Cable Length
- △ — Approximate Weight



ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

**CR194 400-ampere Vacuum Stationary (One-high)
Optional 34" Wide**



Notes:

B1 — AC Power Bus

C — Control Lead Terminal Board

D — Motor Lead Terminal Connection

E — Ground Bus Terminal Connection

F — Ground Terminal Connection (if ordered)

G — Space Required to Open Doors 90°

H — Four-foot Aisle for Contactor Removal

J — Mounting Holes for 1/2" Diameter Anchor Bolts

K — Space Available for Incoming Conduit

M — Recommended Position for Incoming Motor Conduit

N — Recommended Position for Incoming Control Conduit

P — Recommended Position for Incoming Power Conduit

* — Indicates Terminal Location — Approximate for Cable Length

△ — Approximate Weight

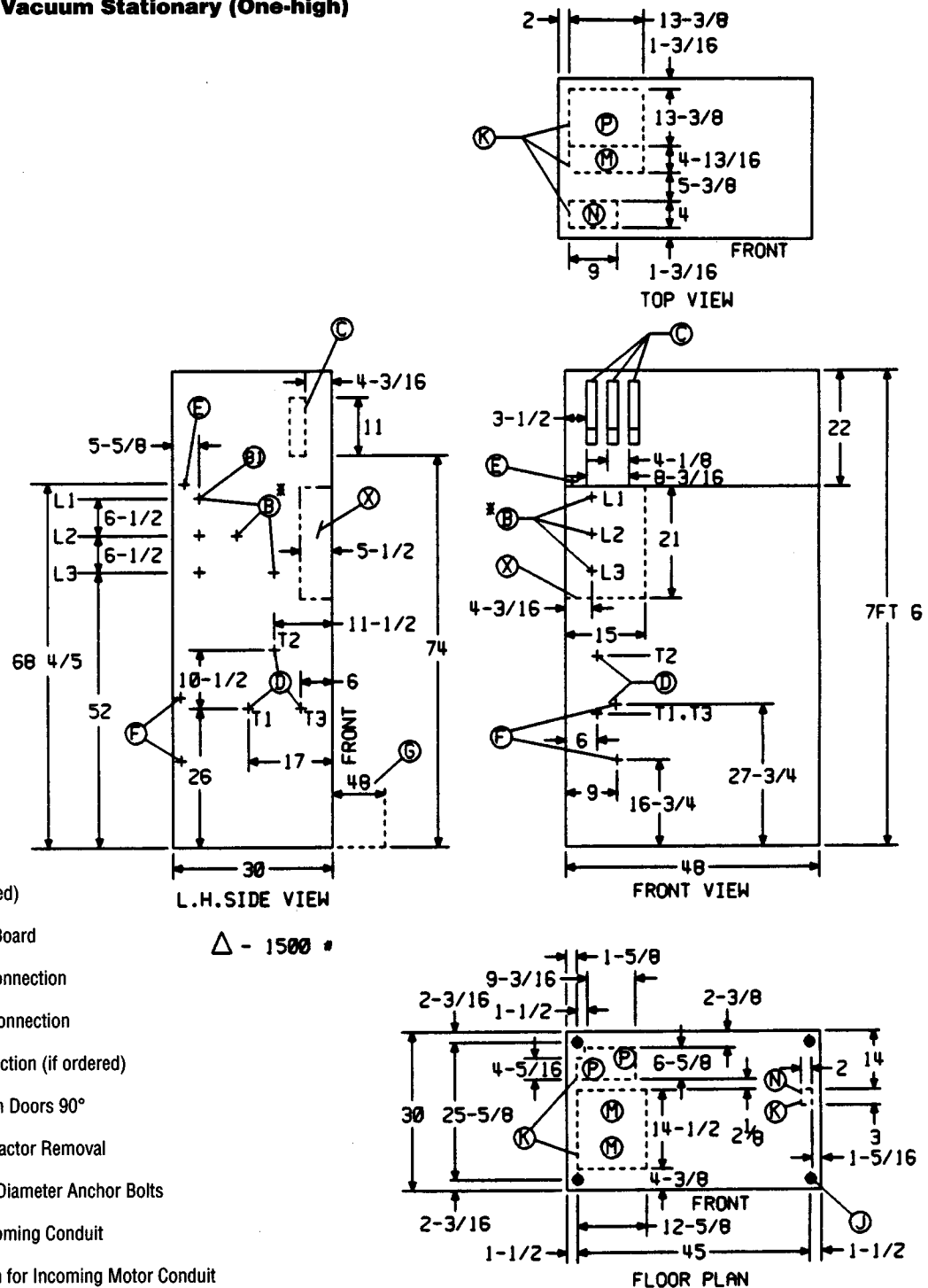
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E



ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

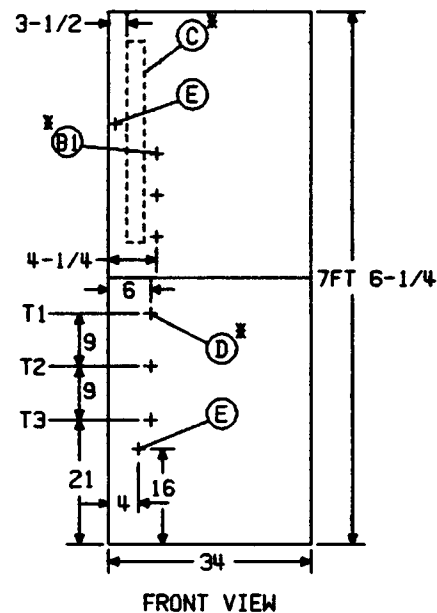
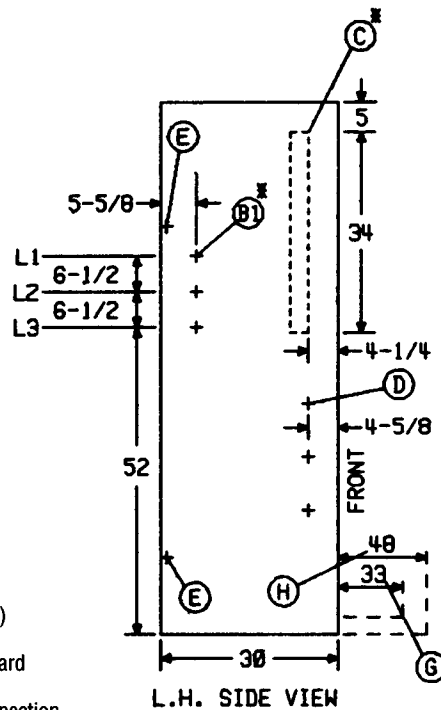
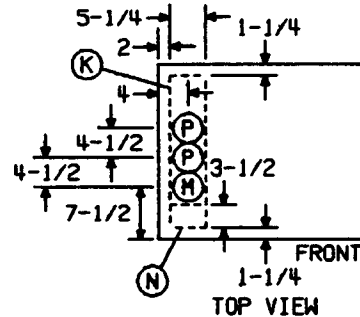
**CR194 800-ampere Vacuum Stationary (One-high)
Standard 48" Wide**





ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

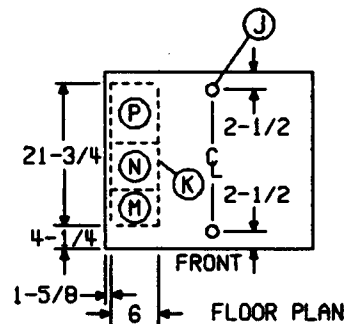
**CR7160 400-ampere Air-break Drawout (One-high)
Standard 34" Wide**



Notes:

- B1 — AC Power Bus (if ordered)
- C — Control Lead Terminal Board
- D — Motor Lead Terminal Connection
- E — Ground Bus Terminal Connection
- F — Ground Terminal Connection (if ordered)
- G — Space Required to Open Doors 90°
- H — Four-foot Aisle for Contactor Removal
- J — Mounting Holes for 1/2" Diameter Anchor Bolts
- K — Space Available for Incoming Conduit
- M — Recommended Position for Incoming Motor Conduit
- N — Recommended Position for Incoming Control Conduit
- P — Recommended Position for Incoming Power Conduit
- * — Indicates Terminal Location — Approximate for Cable Length
- △ — Approximate Weight

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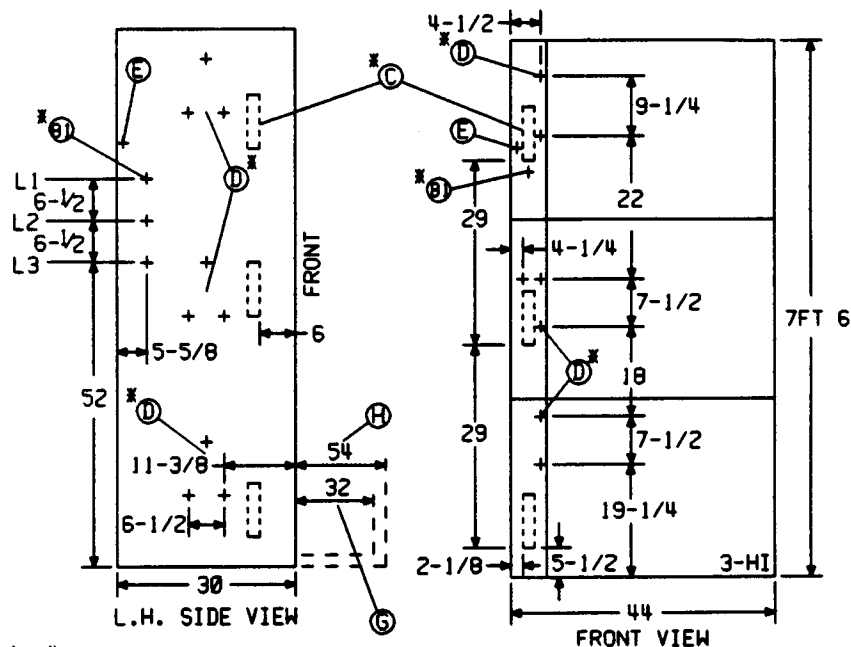
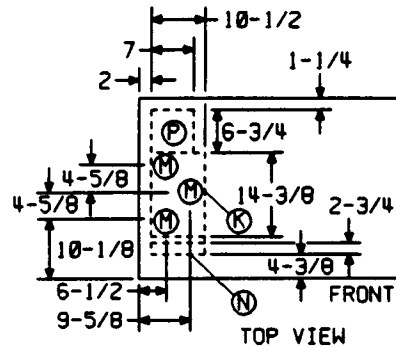


E



ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

**CR7160 400-ampere Air-break Drawout (Three-high)
Standard 44" Wide**



Notes:

B1 — AC Power Bus

C — Control Lead Terminal Board

D — Motor Lead Terminal Connection

E — Ground Bus Terminal Connection

F — Ground Terminal Connection (if ordered)

G — Space Required to Open Doors 90°

H — Aisle for Contactor Removal

J — Mounting Holes for 1/2" Diameter Anchor Bolts

K — Space Available for Incoming Conduit

M — Recommended Position for Incoming Motor Conduit

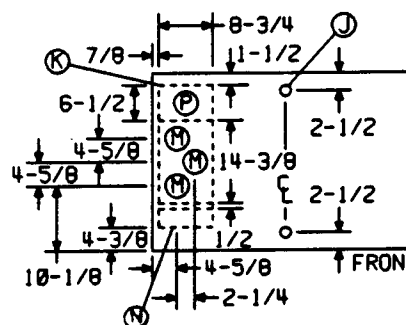
N — Recommended Position for Incoming Control Conduit

P — Recommended Position for Incoming Power Conduit

* — Indicates Terminal Location— Approximate for Cable Length

△ — Approximate Weight

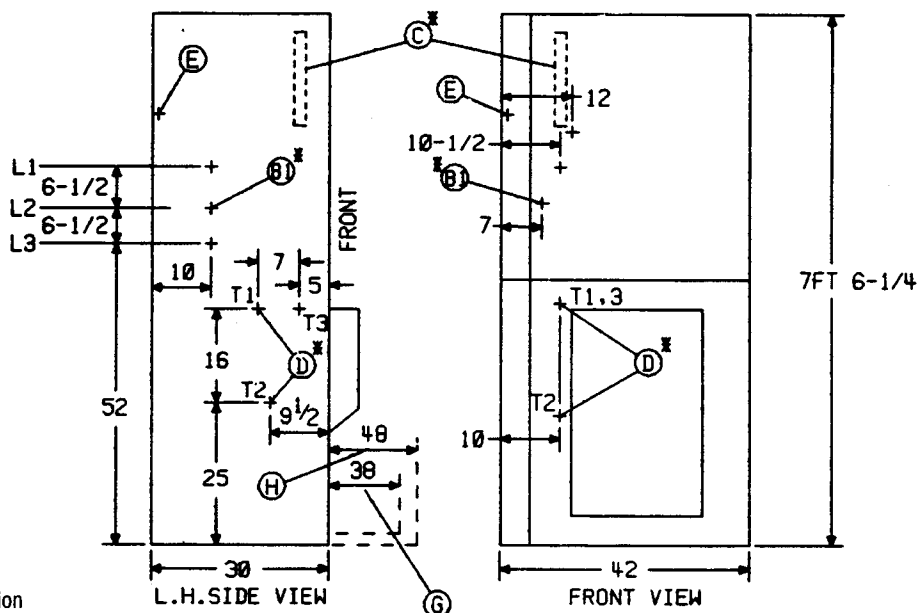
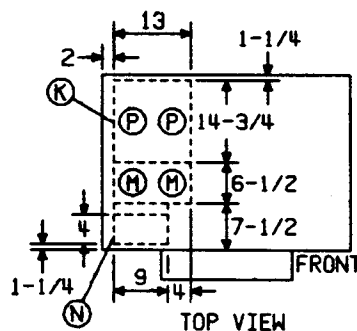
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ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

**CR7160 700-ampere Air-break Drawout (One-high)
Standard 42" Wide**

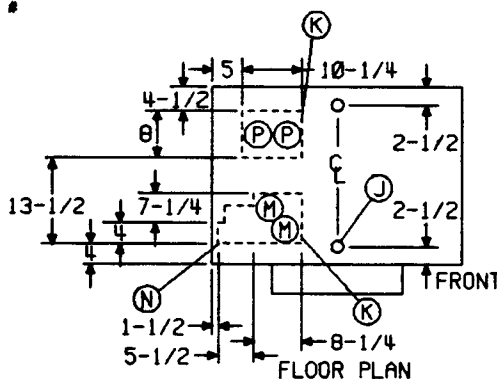


Notes:

- B1 — AC Power Bus (if ordered)
- C — Control Lead Terminal Board
- D — Motor Lead Terminal Connection
- E — Ground Bus Terminal Connection
- F — Ground Terminal Connection (if ordered)
- G — Space Required to Open Doors 90°
- H — Four-foot Aisle for Contactor Removal
- J — Mounting Holes for 1/2" Diameter Anchor Bolts
- K — Space Available for Incoming Conduit
- M — Recommended Position for Incoming Motor Conduit
- N — Recommended Position for Incoming Control Conduit
- P — Recommended Position for Incoming Power Conduit

* — Indicates Terminal Location— Approximate for Cable Length

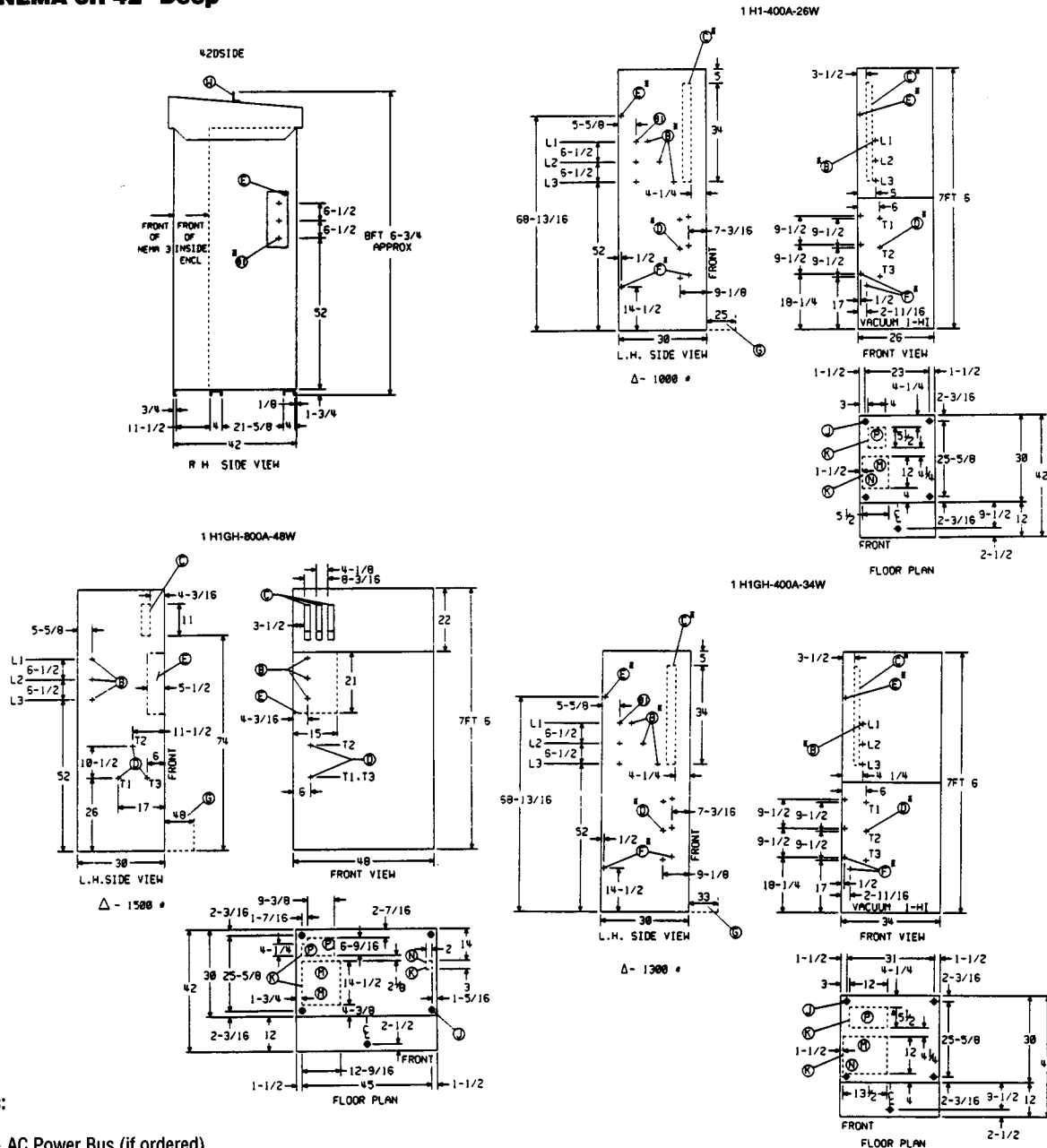
△ — Approximate Weight





ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

**CR194 Vacuum 400-ampere and 800-ampere Vacuum Stationary (One-high)
NEMA 3R 42" Deep**



Notes:

B1 — AC Power Bus (if ordered)

C — Control Lead Terminal Board

D — Motor Lead Terminal Connection

E — Ground Bus Terminal Connection

F — Ground Terminal Connection (if ordered)

G — Space Required to Open Doors 90°

H — Four-foot Aisle for Contactor Removal

J — Mounting Holes for 1/2" Diameter Anchor Bolts

K — Space Available for Incoming Conduit

M — Recommended Position for Incoming Motor Conduit

N — Recommended Position for Incoming Control Conduit

P — Recommended Position for Incoming Power Conduit

W — Lifting Angle

* — Indicates Terminal Location — Approximate for Cable Length

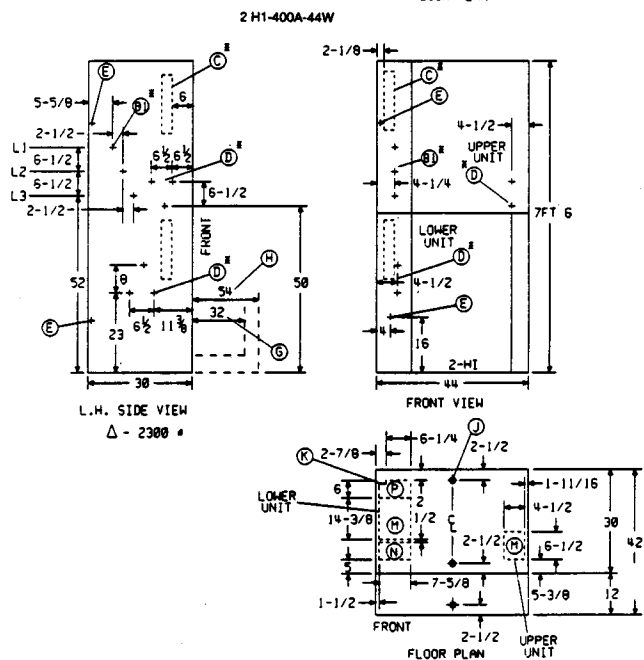
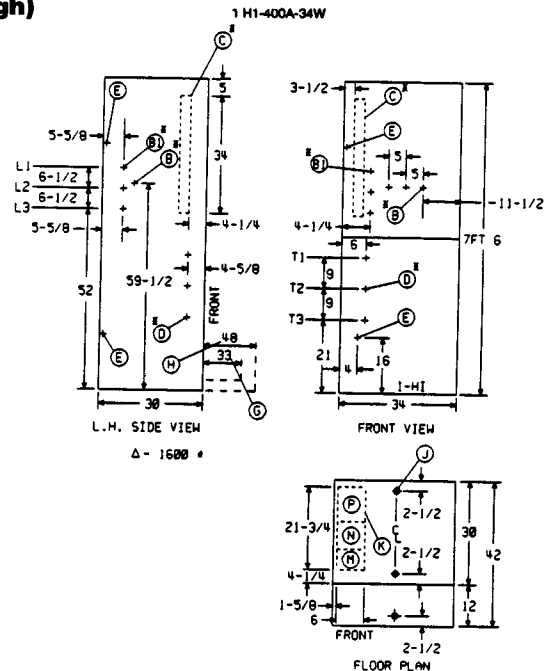
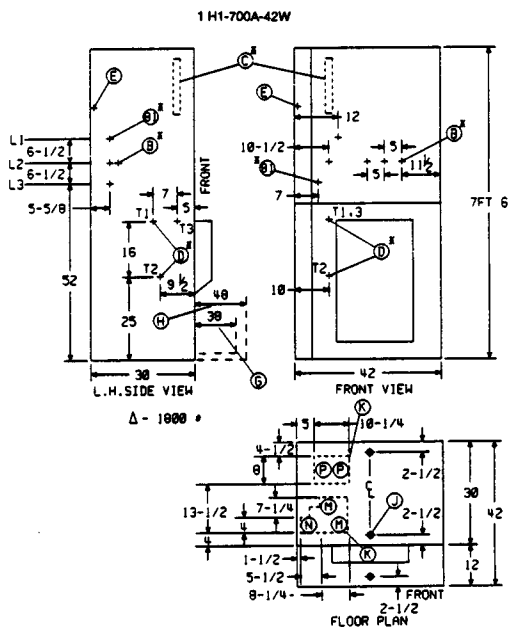
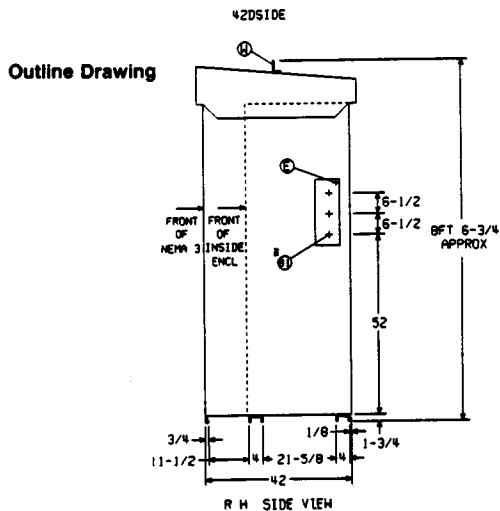
△ — Approximate Weight

E



ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

**CR7160 400-ampere Air-break Drawout (One- & Two-high)
NEMA 3R 42" Deep**



Notes:

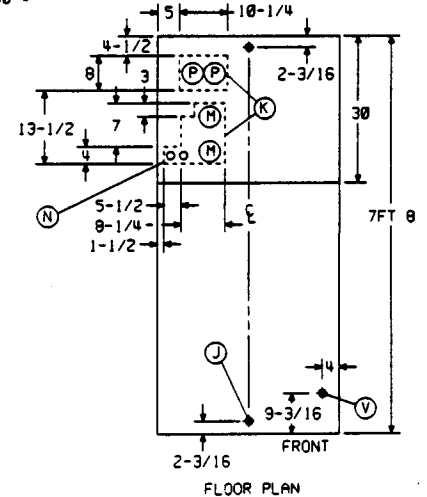
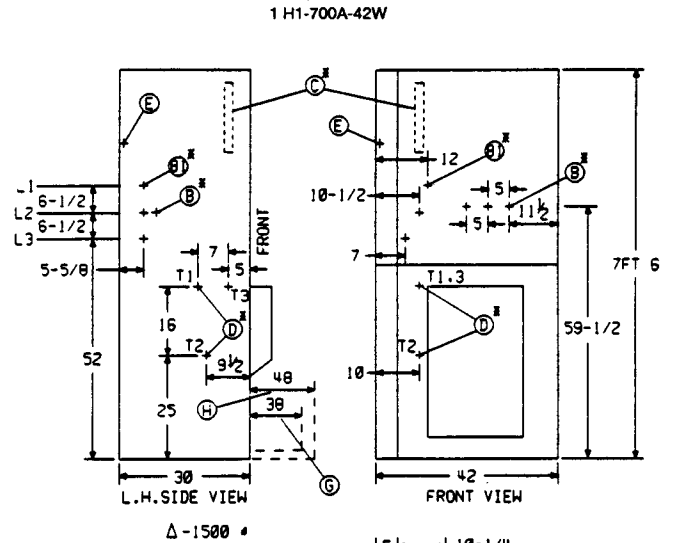
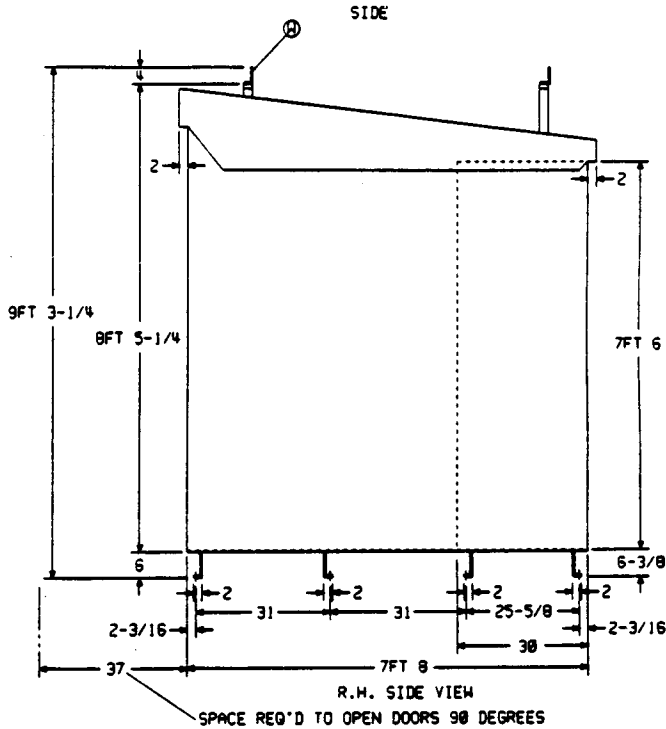
- B1 — AC Power Bus (if ordered)
- C — Control Lead Terminal Board
- D — Motor Lead Terminal Connection
- E — Ground Bus Terminal Connection
- F — Ground Terminal Connection (if ordered)
- G — Space Required to Open Doors 90°
- H — Four-foot Aisle for Contactor Removal
- J — Mounting Holes for 1/2" Diameter Anchor Bolts

- K — Space Available for Incoming Conduit
- M — Recommended Position for Incoming Motor Conduit
- N — Recommended Position for Incoming Control Conduit
- P — Recommended Position for Incoming Power Conduit
- W — Lifting Angle
- * — Indicates Terminal Location — Approximate for Cable Length
- △ — Approximate Weight



ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

**CR7160 700-ampere Air-break Drawout (One-high)
NEMA 3R 92" Deep Walk-in**



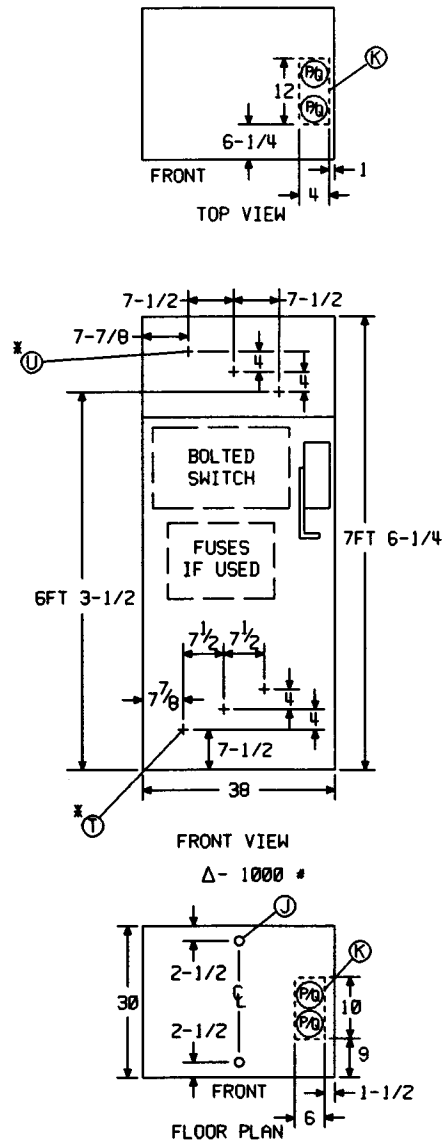
Notes:

- B1 — AC Power Bus (if ordered)
- C — Control Lead Terminal Board
- D — Motor Lead Terminal Connection
- E — Ground Bus Terminal Connection
- F — Ground Terminal Connection (if ordered)
- G — Space Required to Open Doors 90°
- H — Four-foot Aisle for Contactor Removal
- J — Mounting Holes for 1/2" Diameter Anchor Bolts
- K — Space Available for Incoming Conduit
- M — Recommended Position for Incoming Motor Conduit
- N — Recommended Position for Incoming Control Conduit
- P — Recommended Position for Incoming Power Conduit
- W — Lifting Angle
- * — Indicates Terminal Location— Approximate for Cable Length
- △ — Approximate Weight



ENCLOSURE OUTLINE DIMENSIONS 2400-4160 VOLTS

**IC1074 Bolted Load Break Switch
NEMA 1 Standard 38" Wide**



Notes:

- J — Mounting Holes for 1/2" Diameter Anchor Bolts
- K — Space Available for Incoming Conduit
- P — Recommended Position for Incoming Power Conduit
- Q — Recommended Position for Incoming Feeder Conduit
- T — Switch Feeder Terminal Connection
- U — Switch Incoming Power Terminal Connection
- * — Indicates Terminal Location — Approximate for Cable Length
- △ — Approximate Weight



FUSES

INTRODUCTION

To protect the motor branch circuit against the damaging effects of short circuits, current-limiting power fuses are used in Limitamp control. They interrupt all overcurrents of magnitude greater than intended for contactor interruption. On full fault, these fuses start limiting current within the first $\frac{1}{4}$ cycle and interrupt within the first $\frac{1}{2}$ cycle. Because they are fast acting, these fuses are easily coordinated with system protective relaying to give selectivity in short-circuit protection.

Standard fuses supplied with Limitamp CR194 Control are bolt-in type. Clip-in fuses may be supplied in applications where motor full-load current plus service factor does not exceed 320 amperes, but they must be specified by the customer. The blown fuse indicator and the anti-single-phase trip are available with bolt-in fuses only.

Motor-starting fuses are current-limiting as indicated in Figure F.1. They melt before the current in the first major loop can reach its peak value when subjected to melting currents within the current-limiting range. Consequently, the total "let-through" energy involved is low because the fuses operate with such great speed. The contactor, current transformers, and overload relays of a Limitamp controller are coordinated with the fuses to give full protection to the system.

A design feature of motor-starting fuses inherently limits recovery voltage to safe values, thus protecting control insulation.

Controller fuses must have sufficient capacity to carry starting and full-load currents, and yet must interrupt fault currents at a desirable low value. They are therefore made in a number of ratings or sizes so that maximum protection can be obtained over a range of motor horsepower.

For a given set of motor characteristics, it is usually possible to use one of several fuses. The smallest fuses will normally be furnished. If the load is a fluctuating one, involving swings of current above full-load, the fact should be noted in specifying a controller so that a fuse one size larger than minimum will be furnished.

Transient conditions do not generally affect motor-starting fuses since the sand in the fuse conducts heat away rapidly. If transient currents do not come within 25 percent of the minimum melting curve on a time basis, melting will not occur. For example, if the melting curve for a given size fuse shows melting in 10 seconds at 1000 amperes, transient peaks of 1000 amperes would be withstood repeatedly up to 7.5 seconds duration.

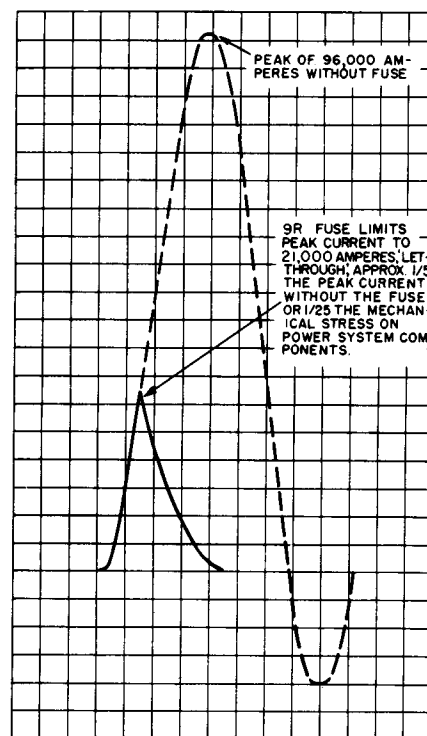


Figure F.1 Current-limiting action of typical fuse.

Motor-starting fuses can be applied on 25-Hertz systems but with lower interrupting capacity than for 50- and 60-Hertz systems. Fuse selection is based on full-load and locked-rotor current.

For a lineup of controllers it may be desirable to use fuses larger than minimum size to reduce the variety of spares required. Such standardization must be specified, however.

BLOWN FUSE TRIP AND BLOWN FUSE INDICATION

The possibility of having one fuse melt, thereby causing a large motor to single phase, has inhibited consideration of fuse-contactor-type starters. Although such a condition is in reality quite unlikely, GE Limitamp Control can be equipped with an optional special mechanism which will detect a blown fuse and cause the contactor to open. Bolt-on fuses contain button indicators to show a blown fuse. This button indicator can be coupled with an anti-single-phase trip mechanism containing a control contact, which, when used in contactor control circuit, can open the contactor to prevent single phasing and/or provide a blown fuse indication on the front door. Blown fuse indication on the front door is available for CR194 equipment only.

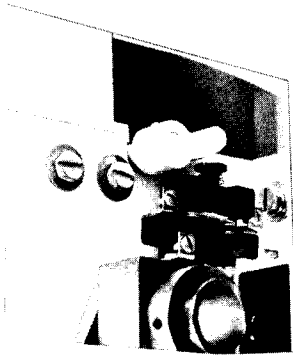


Figure F.2 Anti-single-phase trip mechanism

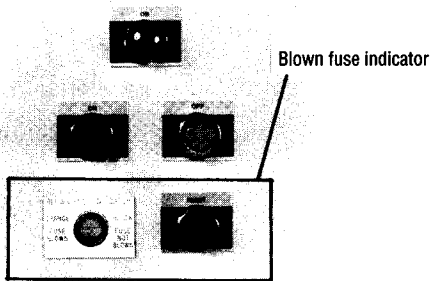


Figure F.3 Blown fuse indicator on door

With this feature, fuses are always bolted in place for correct orientation and alignment. In addition to providing maximum reliability, this feature makes it impossible to mount the fuse in an upside down position which would nullify the trip bar operation.

COORDINATION WITH OTHER PROTECTIVE DEVICES

When Limitamp starters are installed on a given power system, it is necessary to coordinate the time-current characteristics of system protective devices with those of the starters. Use the time-current curves included in GE Time Current Curve No. GES-5000 for this purpose. It includes overload-relay tripping curves, fuse-melting curves and fuse-clearing time curves.

SURGE PROTECTION

The economics of rotating-machine insulation dictates that the machines be protected from voltage stresses above the operating level insofar as is reasonably possible. Overvoltage damages reduce the insulation life. There are many causes of accidental over-voltage whose effects may be reduced by protective means. The most prominent causes are:

1. Lightning.
2. Physical contact with higher voltage system.
3. Repetitive restrike (intermittent grounds).
4. Switching surges.
5. Resonance effects in series inductive capacitance circuits.

Switching transients occur in every electrical system. A well-known phenomenon associated with vacuum interrupters is current chop. GE utilizes vacuum interrupters constructed with widely accepted contact tip materials to provide low chopping currents.

Additional protection against surges for rotating machines may be economically attractive for system voltage installations of 2300 volts and above. This consists of a surge capacitor and lightning arresters.

Lightning arresters reduce the amplitude of the voltage impulse wave. The surge capacitor further reduces the amplitude — but in addition, reduces the steepness of the wave front. It is important to reduce the steepness of the surge wave front to keep the turn-to-turn voltage stress in the machine winding to a minimum.

To prevent overvoltage in current transformer secondary circuits during switching, CTs should be provided with Thyrite protectors when surge capacitors are installed at motor terminals.

Surge capacitors and arresters should be installed as close to the machine terminals as possible. Capacitors and arresters require a 22-inch wide auxiliary enclosure if installed in the controller.

F



OVERLOAD RELAYS

Several types of overload relays are used in Limitamp Control. Limitamp controllers use thermal-overload relays, unless other types are specified.

THERMAL-OVERLOAD RELAYS

Overload relays provided in Limitamp control have inverse-time characteristics and are ambient compensated. Limitamp control utilizes either a thermal-type relay or the solid-state protective relay. These relays, operating from current transformers in the control equipment, carry current proportional to the motor-circuit current. When motor overloads occur, the relay operates to open the main power contactor. The time required for operation varies inversely with the magnitude of the overload. The standard thermal relay should only be used on motors with starting times up to 10 seconds.

EXTERNAL-RESET OVERLOADS

Some industrial plants do not permit a machine operator to open the doors of control equipment enclosures, this being reserved for electricians. To make possible overload-relay reset by operators, it is therefore necessary to provide some means to do so outside the enclosing case. This is accomplished by providing a mechanical-linkage reset mechanism between the relay and door-mounted reset button.

Where external reset is not absolutely necessary, greater simplification of relay mounting results, and this is of benefit to the user because it simplifies maintenance.

Inasmuch as the tripping of an overload device is indicative of too much strain on the motor, it is preferable that only experienced and reliable personnel be allowed to reset overloads. Such personnel should be capable of realizing whether it was an unintentional overload on the part of the machine operator or whether there is an electrical and/or mechanical defect. The customer should consider this factor, however, before electing to provide externally reset overloads.

SOLID-STATE OVERLOAD RELAYS

Solid-state overcurrent protection is available as an optional feature in place of standard thermal overload relays. The inverse-time characteristics can be adjusted to protect motors of various characteristics, such as long acceleration time or short allowable-stall times. Characteristics are accurate and have a smaller error band compared to bimetal relays. The solid-state overload relay is recommended for hermetically sealed air-conditioning motors, and is well suited as a stall-protection relay.

MULTIFUNCTION SOLID-STATE RELAYS

Large motors on vital drives need accurate protection against overloads, phase unbalance or ground faults. Multifunction solid-state relays are available from GE that offer total motor protection in one compact package. Basic protective functions such as overtemperature, overload, instantaneous overcurrent, open-phase, phase reversal, phase unbalance, ground-fault, load jam, load loss and bearing overtemperature protection can be provided.

OVERTEMPERATURE RELAYS

Some motors have RTDs placed in the stator slots. The purpose is to obtain an indication of winding temperature by measuring the RTD resistance and its change with temperature. Difficulty arises in obtaining a continuously accurate indication of temperatures, however, because of the time lag of heat transfer from the stator conductors to the RTD caused by the insulating material surrounding the conductors. Temperature changes in the conductor will not be reflected in RTD resistance change until heat is transferred through the thermal resistance and capacitance of the insulating material.

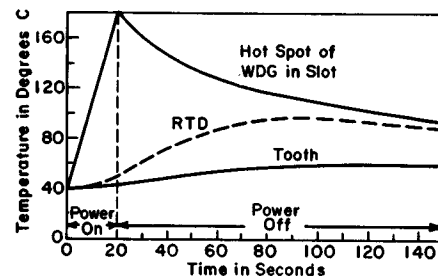


Figure F.4 Approximate temperature of RTD in large motor during locked rotor.

If the copper temperature is changing very rapidly, such as during locked rotor, the RTD will lag far behind the copper temperature as shown in Figure F.4. Consequently, monitoring the RTD temperature is inadequate for thermal protection during rapid-transient conditions. However, for steady-state indication of temperature, the RTD is very accurate.

A relay which responds to changes in resistance of RTDs, providing steady-state indication of motor-winding temperature, used in conjunction with a bimetallic overload relay will provide reasonably precise over-temperature protection for the motor.

Available solid-state relays contain a device which will more accurately compute hot-spot temperature by utilizing RTD amperes and line amperes. This relay accurately



tracks motor heating and is recommended in preference to the separate bimetal relay and RTD relay.

OPEN-PHASE AND PHASE-UNBALANCE PROTECTION

A three-phase motor may be damaged when subjected to unbalanced line currents. Usually, the damage occurs in the rotor from overheating, caused by reverse sequence components of currents not detected by normal overload devices. The rate of motor heating will be a function of the degree of phase unbalance, the most extreme of which is the open-phase condition. For that reason, open-phase relays should operate instantaneously to avoid serious motor damage. Likewise, a motor may be damaged over a period of time with as little as 10% unbalance, where unbalance is a transient condition which would not justify instantaneous shutdown. Consequently, the time to trip should be delayed in proportion to the percentage of unbalance.

More comprehensive open-phase or single-phase protection can be obtained by applying a solid-state motor-protective relay, which will trip the contactor in the event of an open phase, regardless of the cause, even if external to the vacuum Limitamp control.

A possible concern that may arise when applying a medium-volt contactor to a transformer feeder is what happens to the contactor when a voltage dip occurs. In the past, the contactor would drop out — removing power from the primary of the transformer when the contactor coil power is reduced to 60 to 80 percent of full voltage. To prevent dropout during loss of control voltage, latching contactors should be applied. In these cases, the contactor is latched by a closing coil and unlatched by a trip coil. A capacitor trip device can be applied to trip the contactor in the event of total loss of control power. (See Latched Contactors, page B4.)

CURRENT DIFFERENTIAL PROTECTION

The term differential, as applied to a type of protective relaying, designates the principle on which the scheme operates — that is, a difference in current. The relays used are connected in such a way as to detect a percentage differential in current between ends of a motor winding. Ordinarily, in a machine operating without a winding fault, the current into one end of a phase winding is equal to the current out the other end of the same winding. When a fault occurs, however, the current into one end of the winding is short circuited inside the machine (to another phase or to ground) at the place of fault, so that a differential occurs between current “in” and current “out.” This causes the relay to operate. The percentage differential may at times be quite small when the

fault is located at a point of high impedance inside the motor winding, and this is the reason why straight over-current relays alone do not always give adequate protection.

The cost of this type of relaying is justified by the size of the investment to be protected. Large motors (usually above 1500 hp) that are expensive to repair or replace often employ differential relays.

Specifically, differential relays accomplish the following:

1. Provide for power interruption to a motor in the event of a phase-to-phase insulation failure in the motor windings.
2. Provide for power interruption to a motor in the event of a phase-to-ground fault in the motor winding.

The primary use of differential relays in Limitamp Controllers is to give fast, sensitive protection for faults in the end turn outside the stator punchings. Such faults are relatively rare compared with ground faults. However, when they do occur, the presence of differential relays would probably mean the difference between minor and extensive damage.

Two methods of differential protection are available. One uses six identical current transformers: three located in the motor leads and three located in the wye points of the motor windings, usually at the motor. In conjunction with these six current transformers, a Type IJD or CFD relay is used to detect the difference in current in the current transformer (CTs). The other method, known as self-balancing, uses three donut-type CTs. Both the motor leads and the wye connections are brought back through the holes in the donut CTs. For this system, an instantaneous relay of the hand-reset type is used.

GROUND-FAULT RELAYS

Ground fault relays are justified economically for all motors rated 2300 to 7200 volts, 150 horsepower and above. The purpose is to provide interruption of power to the motor as rapidly as is practical after positive indication that a ground fault has occurred.

The time of interruption of ground-fault current is dependent on several factors:

1. Sensitivity of the ground-fault relay.
 - (a) Instantaneous type
 - (b) Time-delay type
2. Magnitude of ground current.
3. Clearing time of the power interrupter.

The importance of clearing ground-fault current rapidly cannot be overstressed. Ground current inside rotating



machines causes damage to the lamination which, if not interrupted rapidly, necessitates complete disassembly and repair of the motor.

Although most ground-fault relays are now of the instantaneous type, few applications do require inverse-time current relays for coordination and selectivity reasons. The use of instantaneous-type relays is made possible through the employment of a zero-sequence “donut” or window-type current transformer installed in the starter in such a way as to permit all three conductors of the three-phase line to be used as the current-transformer primary.

Phase currents add to algebraic zero, regardless of magnitude, and no secondary current flows except that induced by the primary current going to ground. This system gives positive indication of ground current, eliminates false tripping and permits instantaneous relaying.

If time coordination with other ground-fault relays is necessary, time overcurrent relays may be used in the current-transformer arrangement.

For certain sized motors where the power system permits, ground-fault relays may be used as a less expensive alternative to differential relays. Most phase-to-phase winding faults detected by differential relays result in a simultaneous phase-to-ground fault, thereby operating the ground fault relay. For that reason, ground fault relays may be used as a less expensive alternative to differential relays.

Another method of detecting ground currents in a three-phase system employs three separate line-current transformers, one in each phase, with the secondaries fed through a single current relay. In this system, the secondary currents should sum to zero just as they do in the primary of the “donut” current transformer. And, with no ground current flowing, the three secondary currents do add and cancel each other out. Ground current only will cause the relay to operate. For currents of large magnitude, however, such as motor locked-rotor current, current-transformer saturation becomes a problem, causing residual current to flow in the relay coil...resulting in false tripping. To prevent false tripping with the residual connection, time-delay relays are necessary to permit riding over the starting period of the motor. This fact makes instantaneous relays impractical in the residual system.

Instantaneous ground-fault relays may be applied to Limitamp (NEMA Class E2) controllers without limitation on available ground current. The fuse and relay-con-

tactor clearing times are such that ground-fault currents up to and including the fuse rating will be cleared without damage to the controller.

Standard ground-fault relay used in Vacuum Limitamp Control is a solid-state relay which operates on approximately 4 to 12 amperes ground-fault current. If greater sensitivity is required, other solid-state ground-fault relays may be furnished which can be adjusted to trip as low as 1 ampere. However, extreme care must be exercised in applying ground-fault relays of such low pick up. They could trip falsely on system-charging current. A magnetic ground-fault relay can be provided on request.

UNDERVOLTAGE PROTECTION

NEMA defines undervoltage protection as a device whose principal objective is to prevent automatic restarting of equipment.

Instantaneous undervoltage protection is inherent to the standard 3-wire control circuits, since the contactor will drop out and stay out on loss of voltage.

TIME-DELAY

Time delay undervoltage protection (TDUV) for a Limitamp controller can be provided to prevent shutdown of a motor on adjustable duration voltage dips below the adjustable dropout voltage. With either time-delay or the standard instantaneous undervoltage protection, the motor remains disconnected until the operator restarts the motor.

TDUV — AUTOMATIC RESTART

In the event of voltage dips of short duration, conventional TDUV circuits provide an automatic restart of Limitamp contactor without operator intervention. (A time delay of approximately 1.5 seconds is usually provided.) However, in motor applications, automatic restarting can cause serious damage to windings and mechanical loads connected to the motor due to out-of-phase reclosing. In worst cases this out-of-phase reclosing could apply up to two times the normal voltage to motor windings. TDUV auto-restart scheme is not recommended for synchronous, wound-rotor or large horsepower high-speed squirrel-cage motor controllers without additional circuitry to delay reclosing after a UV condition.

The TDUV automatic restart scheme in Limitamp Control permits instantaneous shutdown by connection of the STOP button into the UV relay circuit. Care should be taken not to connect a maintained-contact device into this circuit.



SYNCHRONOUS-MOTOR CONTROL AND EXCITATION

SYNCHRONOUS MOTOR CONTROL

GE Limitamp synchronous-motor controllers are offered for both brush-type and brushless synchronous motors. As a standard, both brush-type and brushless synchronous motor controllers are equipped with the CR192 μ SPM solid-state field application and protection module. This microprocessor-based module provides basic synchronous motor control and protection functions including squirrel-cage starting protection, power factor and pull-out running protection, and field application control to maximize pull-in torque (for brush-type machines only). Digital displays of motor running line current and power factor are featured along with a keypad for entering set-point parameters. Available options are field loss protection, exciter voltage check protection, field amps display, exciter volts display, incomplete sequence protection, and power factor regulation (when used with compatible SCR type variable field exciters).

EXCITERS FOR BRUSH TYPE MOTORS

For synchronous motors equipped with slip-rings and brushes, Limitamp is offered with a variety of excitation options. Single-phase solid-state exciters can be integrated in the controller NEMA 1 ventilated enclosure up to 9 kW (exciters must be derated for non-ventilated enclosures). Larger exciters require auxiliary enclosures that can be placed in the common bussed line-up with the Limitamp controllers. Two basic types of exciters are available:

- SFC (fixed excitation with adjustable tapped transformer)
- VFC (on-line adjustable excitation by manual or automatic means)

FIXED EXCITATION

The basic exciter offering is a single-phase, tapped-transformer, static field contactor (SFC). The SFC is a solid-state switching device consisting of silicon controlled rectifiers (SCRs) in a bridge circuit for rectification of AC power to DC. Additional SCRs are provided to switch the field discharge resistor. During starting, the SFC switches the field discharge resistor on so that the induced field current from the motor field is passed through the discharge resistor. The field discharge resistor is also switched on to discharge the field current when DC is removed at motor shutdown and if, during normal motor operation, the motor field generates a high voltage surge above approximately 600 volts, such as would occur if the motor “slips” a pole. When the motor has accelerated to near synchronous speed, the

CR192 μ SPM module signals the SFC to apply DC to the motor field, the SFC switches the field discharge resistor off and causes the SCRs in the rectifier bridge to turn on, resulting in DC being applied to the motor field. The bridge SCRs are gated “full on” so that they emulate a diode rectifier bridge. The voltage of this DC field supply is determined by the tap connection of the customized transformer that feeds AC power to the rectifier bridge. This transformer has secondary taps arranged so that the DC voltage can be adjusted in 5% increments from 70% to 130% of the transformer nominal secondary voltage by changing connections at the transformer tap.

VARIABLE EXCITATION

Another exciter offering is the electronic variable field contactor (VFC). The VFC is available in single- or three-phase versions. Three phase VFC exciters are recommended for sizes 20 kW and above (125 VDC fields), and 25 kW and above (250 VDC fields). Like the SFC (above), the VFC controls the switching of the field discharge resistor and DC to the field depending on inputs from the CR192 μ SPM. The difference is that the gating of the rectifier bridge SCRs can be controlled by varying an analog voltage at its control input. This allows on-line control of the DC exciter voltage by any of several means:

- 1) Manual control via a door-mounted potentiometer.
- 2) Automatic control via the field current regulation module.
- 3) Automatic control via the CR192 μ SPM equipped with power factor regulation.

ON-LINE FIELD ADJUSTMENT

The manual potentiometer is normally mounted on the door and allows an operator to adjust the motor field current while the motor is running. This provides the convenience over the SFC type exciter of not having to shut down the motor and physically move cables between several taps on the exciter transformer.

FIELD CURRENT REGULATION

The field current regulator module also employs a manual potentiometer for adjustment of the field current. However, the regulator provides a closed loop control so that the VFC DC output is automatically adjusted to maintain the set-point field current as set by the manual potentiometer. This feature allows the operator to set the field one time at a desired field current. The field current will then be regulated to compensate for field resistance changes due to field winding heating or system voltage fluctuations. The leading reactive power contribution of a synchronous motor is related to the level of



field current. If it is desired to maximize the contribution of leading reactive power from the synchronous motor at all shaft loading conditions, set the field current as high as possible without exceeding its nameplate rating. Field current regulation is the ideal choice for maximizing the leading reactive power because it allows the operator to set the field current very close to rated and not worry about the current “creeping” higher or lower from the potentiometer setting.

POWER FACTOR REGULATION

F Power factor regulation is an excellent choice for applications requiring field forcing, which is applying DC excitation above its rating for a short time. Many drives, such as chippers, are subject to transient impact overloads many times the motor rating for short time intervals. By forcing the field, the synchronous motor can be enabled to deliver shaft torques above the rating without “pulling-out” of synchronism and shutting down. GE tests on chipper drives have demonstrated that the power factor regulation option can provide the rapid field forcing feature to prevent disruptive motor “pull-out.” Power factor regulation operates on the principle that the motor running power factor is a good predictor of motor pull out. Before a motor pulls out of step (as a result of high shaft loading from a hard or oversized log entering a chipper), the power factor dips in the lagging direction drastically. By setting the regulator such that it boosts excitation as the power factor dips more lagging than the regulator set point, the motor running power factor is held to a “healthy” level and motor “pull-out” is avoided. Power factor regulation also allows the field excitation power to be conserved when the motor is running lightly loaded or unloaded. This not only allows energy conservation but also deeper no-load cooling of the motor windings, so the motor runs cooler for a given level of RMS loading. Power factor regulation can help regulate the power system voltage by minimizing reactive power swings over a wide range of motor loads.

BRUSHLESS SYNCHRONOUS CONTROL

The CR192 μ SPM is also designed for use with brushless synchronous motors. It provides timed field exciter application, power factor and pull-out protection and starting/stall protection. Included with the standard brushless synchronous motor Limitamp controller is a variable exciter field supply consisting of a door mounted variable autotransformer and rectifier for on-line exciter voltage control.

FIXED-TAP FIELD RESISTOR

A fixed-tap field resistor may be used for separate DC source. This resistor, when supplied with the Limitamp

panel, is mounted on top and is connected directly in series with the synchronous-motor field as a means of adjusting field current. The resistor is continuously rated with taps to adjust field current 10-percent above and below rated full-load field current for rated power factors in approximately 2½-percent steps.



CONTROL CIRCUITS

CONTROL POWER TRANSFORMER

Control power transformers used in Limitamp starters are single-phase, air-cooled, core-and-coil construction with high-voltage windings covered to prevent contamination by dust and dirt. Those furnished in standard panels have a 25-kV Basic Impulse Level (BIL) rating. When specified, 60-kV BIL rated control transformers can be furnished, but will require special space consideration. Two kVA is standard in a basic controller. Transformers above 2 kVA are optional, and above 3 kVA may require an auxiliary enclosure for mounting.

OMISSION OF CONTROL POWER TRANSFORMER

A lineup of starters can use a common control power transformer or other source of control power. In either case, the power source and control circuit must be provided with interlocking relays so the loss of either will shut down all operating motors. Control bus is required in all controllers if a common source of control power is used.

A single source of control power results in some disadvantages: (1) Unless each panel is provided with a fused control switch, troubleshooting must be done with live wires in the panel; (2) a single controller, if relocated independent of the lineup, will require modification to add a control transformer and fuses; and (3) the loss of control power will cause shutdown of all machines.

TIMING RELAYS

Pneumatic-type timing relays close or open a circuit after a definite elapsed time on either energization or de-energization.

Motor-driven timing relays close or open a circuit with time delay on either energization or de-energization. They provide a wide range of time, however, and are not affected by ambient temperatures. Solid-state timing relays with high accuracy and repeatability can be furnished.

INCOMPLETE-SEQUENCE RELAY

An incomplete-sequence relay is used to shut down the motor (squirrel-cage induction or synchronous) on reduced-voltage starting if the control fails to transfer to full voltage. It protects the starting reactor or autotransformer from energization longer than rated time. The relay can be furnished for other sequencing functions also.

JOGGING

Drives requiring “jogging” (or inching) must have the control circuit arranged for repeatedly closing the line contactor at short intervals to effect small movements of the driven machine. The line contactor is held closed only as long as the JOG button is held depressed.

An anti-kiss circuit is provided with the JOG push button, including a jog relay. The jog relay closes when the JOG button is depressed, energizes the line contactor coil, seals itself in around the JOG button and is dropped out only after the line contactor has closed and wiped in. This makes possible repeated opening and closing of the line contactor, but also assures that the tips wipe closed each time.

CURRENT INTERLOCKING

Current-operated relays indicate when the arc is completely extinguished after the line contactor opens. These relays then permit closure of a reversing contactor. A short circuit may occur if a reversing contactor closes after the forward contactor opens but before the arc has been extinguished. This circuit is necessary in controllers with “plug stop” or where pressing one instantaneous contact picks up reversing contactor while running forward. Current interlocking is not normally used on overhauling loads such as mine hoists, since during the lowering cycle enough current may not be drawn to operate the interlocking relays.

This circuit is not supplied on standard Limitamp reversing controllers, as the operator is expected to turn the selector switch to reverse only after pressing the STOP button.

POTENTIAL INTERLOCKING

Potential interlocking is used for the same reason as in current interlocking. Potential transformers and interlocking relays are added to prevent closure of one primary contactor before complete interruption of the arcs at the tips of the other (reverse) contactor. Operation is based on the principle that by the time the disconnected motor's generated EMF has decayed to the point where the interlocking relays have dropped out, the arc in the disconnected contactor has extinguished, and closing the reversing contactor is permissible.

Potential interlocking is used on hoists and other applications having possible overhauling loads.



INSTRUMENTATION

AMMETER

An ammeter (panel-type or switchboard-type) is used to indicate either motor amperes or total incoming amperes. It can either be hardwired to the current transformer of one phase or all three phases can be monitored by the use of a selector switch. One current transformer is required for single-phase reading; two are required for open delta three-phase reading; three are required in a wye circuit. Three window-type current transformers are provided as standard on Limitamp Controllers.

VOLTMETER

The voltmeter (panel-type or switchboard-type) is used to indicate phase-to-phase potential. One potential transformer is required if only one phase-to-phase potential is monitored. Two potential transformers, connected in an open-delta configuration, are required along with a selector switch to monitor any one of the three phases. Three potential transformers mounted in an auxiliary enclosure and a selector switch are required to read both phase-to-phase and phase-to-neutral potentials.

POWER FACTOR METER

A power factor meter is used to indicate power factor lead or lag. It is useful in adjusting power factor in synchronous motor drives and in determining the power factor of a given drive. The addition of a power factor meter requires the addition of potential transformers, or of some other potential source with correct phase and accuracy. When a synchronous starter is supplied, the CR192 μ SPM has a digital power factor meter built into the device.

WATTMETER

A wattmeter is used to indicate loading or useful power being delivered to a drive at any instant. The instrument is typically calibrated in kilowatts. Two potential transformers connected in open delta are required for operation.

OPERATION COUNTER

The operation counter is electrically operated from a control interlock on the line contactor. It totals the number of times the contactor has closed and opened, and thus provides data for the establishment of maintenance schedules, a record of the number of batch processes initiated over a given period of time, or any other purpose where the number of line contactor closures may be significant.

VARMETER

The varmeter indicates lagging or leading reactive power. It requires the addition of two potential transformers. In totaling reactive power on a bus feeding several loads, individual vars for each load can be measured by means of individual varmeters on each motor and added directly.

ELAPSED TIME METER

An elapsed time meter is used to indicate hours of operation or shutdown time of a particular motor or drive for the purpose of production records, maintenance scheduling, or engineering records.

TRANSDUCERS

Transducers are used to transmit electrical properties to remote devices, while maintaining a high accuracy when the cabling distance or resistance may be high. The standard output is 4 - 20 mA DC. Current transducers require (1) CT; voltage transducers require (1) PT; watts transducers require (2) CTs and (2) PTs.

TEST BLOCKS

Current and potential test blocks provide a plug-in feature for portable meters, to obtain readings or records without shutting down the machine.

WATT-HOUR METER

A watt-hour meter is used basically to measure work done. Specifically, it registers total watt-hours used by the motor or other load on the controller. It is useful in assigning power charges in plant accounting or for record keeping of power consumed per unit of manufacturing. It requires the addition of two potential transformers connected in open delta.

A demand register indicates maximum demand. It is useful in determining peak loads for particular machines where demand must be controlled to keep power costs at a minimum.



Below are typical push buttons, selector switches and control wiring used in standard Limitamp. The following pages depict cut-sheets showing details of typical components. For more detail, refer to Table A.4, which shows publication reference.

Table G.1 Typical push buttons

Function	Device used	Application
Start-Stop	CR104P momentary type	FVNR starters with 3-wire control
Stop	CR104P momentary type CR104P maintained type Options: Mushroom head Provisions for locking open	Starters with 3-wire control Starters with 2-, 3-wire control
Forward-Reverse-Stop	CR104P momentary type	FVR starters
Fast-Slow-Stop	CR104P momentary type	2-speed starters

Table G.2 Typical selector switches

Function	Device used	Application
On-Off	CR104P maintained type	Permissive start with 2-, 3-wire control
Hand-Off-Auto	CR104P maintained type	Auto or manual start with 2-wire control
Fast-Slow-Off-Auto	CR104P momentary type	2-speed starters

Table G.3 Control wiring details

Item	Standard	Option
Control wiring type	MTW, thermoplastic 600V, 90° C	SIS (vulkene)
Control wire size	AWG #14	AWG #12
Control wire terminals	Uninsulated spade type	Insulated ring type
Wiremarkers	Plastic sleeve type	Heat-shrinkable labels
Wire color code	Power-Black Control-Red Neutral-White Ground-Green	
Terminal blocks	CR151B, 30A, 600V	EB-25, 50A, 600V Connectron Type KUX



CR120B MACHINE TOOL AND INDUSTRIAL RELAYS

The CR120B and CR120BL Series A, multi-circuit industrial relays are designed to meet most panel application requirements. They are available as standard, latched or time-delay relays.

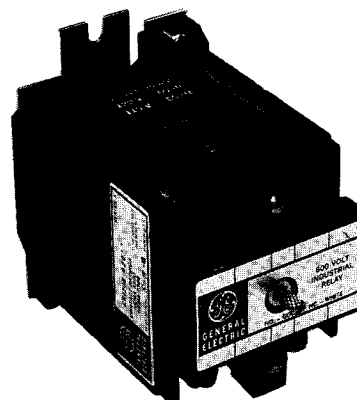
All forms of the relay mount on the same base and in the same small panel-mounting area. Relays may be arranged in any configuration or modified on a panel without altering the mounting area.

FEATURES

- **Bifurcated contacts assure positive make** — unique bifurcated contacts assure positive make at all voltages and give excellent fidelity, even in harsh environments.
- **Transparent Lexan® contact cartridges** — allow inspection of contacts.
- **Convertible contacts** — allow conversion from normally open to normally closed, or vice versa. Just change the terminal screws and invert the contact module.
- **Quick-change coil** — can be changed without removing any screws.

LATCH ATTACHMENT

The latch attachment mounts on any standard CR120B relay in the same manner as a deck adder.



CR120B standard AC relay

Table G.4 Coil data

	Inrush VA	Sealed VA	Sealed watts
AC relay coil	120	15	7
AC unlatch coil	31	15	9.2
DC relay coil	235	2.8	2.8

Table G.5 Coil data

	Volts
60 Hz	115-120, 230, 460
DC	24, 48, 125

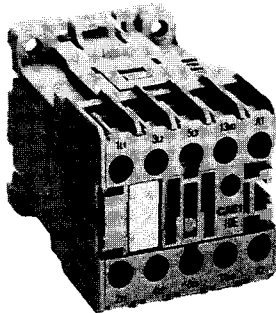
Table G.6 Contact ratings

Type of contacts	Max. AC voltage	Max. Continuous rating amperes	Maximum AC volt-ampere rating		Maximum AC rating amperes		Maximum DC rating amperes		Maximum DC volt-ampere rating
			Make	Break	Make	Break	125V	250V	
Inst.①	600	10	7200	720	60	6	1.1	0.55	138
Delay	600	5	3600	360	30	3	0.5	—	—

① Use for CR120B contact rating.



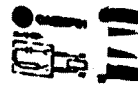
C-2000 MINI-CONTACTORS (MCR4)



FEATURES AND BENEFITS

- **Modular design** — Various configurations can be created with the wide selection of available accessories.
- **Compact size** — The contactor/relay mounting profile is approximately 1 1/8" x 1 1/8".
- **Long life** — This family of relays offers superior performance. Mechanical life is rated at 10 million operations.
- **Reliable operation** — These products are manufactured with the latest advancements in materials technology and designed to ensure long, dependable operation. (Coils are designed for protection against burnout during demanding brownout conditions.)
- **Flexible mounting** — Mounting is not restricted for contactor and relay applications; contactors may be horizontal-, tabletop- or ceiling-mounted.
- **International acceptance** — Devices are listed and certified to IEC 947.4, VDE0660 and North American standards, and they provide dual markings.

ACCESSORIES



Surge Suppressor

Used to protect control circuits from voltage transients. Plugs into front of contactor, no external wiring required.

While the standard line of DC-operated relays requires only three-watt coil holding current, some PLC applications require lower wattage coils to efficiently interface with the PLC. Special relays are available with 24-volts DC coils, which only require 1.2 or 2 watts for pull-in and holding. These relays are available in three different terminal configurations — 4NO, 3NO-1NC and 2NO-2NC.

Table G.7 Main contacts data

	Control relays
Rated insulation voltage (IEC 947.1)	660 volts
Rated thermal current (UL 508)	10 amperes
Contact rating	A600, Q600
Frequency limits	25-400 Hz
Impedance per pole	2.4 mΩ
No overlap between NO and NC contacts	
Space	1.1 mm
Time	>2 msec

Table G.8 Main contacts data

Time	Rating amperes	Carry continuous amperes	Make momentary amperes	Break amperes
A600	AC	10	60	6
Q600	DC	2.5	0.55	0.55

Table G.9 Pickup/Dropout percentage coil voltage

Type coil	Pickup	Dropout
AC controlled	80%-110%	35%-55%
DC controlled	80%-110%	20%-40%
PLC interface (1.2W)	80%-125%	20%-30%
PLC interface (2W)	70%-125%	20%-35%



CR104P PILOT DEVICES



DESCRIPTION

Newly designed nameplates with chrome-plated octagonal rings project an attractive, quality appearance. Positive-feel selector switches give a quality touch in all illuminated, solid-color, spring-return and maintained units.

Standard and illuminated push buttons and selector switches are available with key or conventional operation. The CR104P push button line also includes press-to-test and standard indicating lights, mushroom-head, joystick, push-pull and push-push operators.

APPLICATION

These pilot devices are specially adapted to machine-tool service or any application where oil or coolant is present. The convenient one-hole mounting makes this line suitable for general purpose use in equipment of all kinds where panel mounting is possible. This line is ideal for applications where oil tightness, watertightness and long life are essential.

All units are suitable for use in Type 1, 3, 3R, 4, 12 and 13 environments when mounted in enclosures rated for those same applications. (See ① under Table G.10.)

FEATURES

- **Ease of assembly** — One-screw contact block mounting. Octagonal ring provides ease in front panel mounting and enclosure applications.
- **Greater torque** — Due to the eight-sided ring design, greater torque can be developed during assembly and installation to provide oil tightness.
- **Stocking inventories reduced** — Forms may be furnished as complete units or as components, allowing building-block construction from a minimum of stock.
- **Color convertible** — Colored knobs and caps are available in kit form for easy field conversion.

Type	Standard	Push-to-test	Bulb	Color
Full voltage (120 Volts AC)	X	X	#120PSB	Red Green Amber
Transformer (6 Volts AC Secondary)	X	X	#755	Blue White Clear
Neon	X	N/A	Neon	Red White Amber Clear
LED (Transformer type only)	X	X	LED (6 volt)	Red Green Blue Amber

CONTACT RATINGS

Table G.10 AC ratings, NEMA A600 heavy pilot duty

Maximum AC	Continuous current amperes	AC voltamperes 50/60 Hz②	
		Make	Break
600	10	7200	720

① CR104PTP units are suitable for Type 1, 12 and 13 applications only.

② Maximum make and break currents are 60 and 6 amperes, respectively, for voltages of 120 and below.

Table G.11 DC ratings, NEMA P600

Maximum make or break amperes		
125 volts	250 volts	600 volts
1.1	0.55	0.2

CR104P PILOT LIGHTS

Pilot lights match appearance of switches above. Standard applications use full-voltage or transformer-type lights. Optional nameplates match those used with switches; neon lights are available (with limited lens colors).

Table G.12 Typical pilot lights

Function	Device used	
Full voltage	CR104P with 120-volt, 10,000-hour lamp	
Transformer	CR104P with 6-volt, 20,000-hour lamp	
Push-to-test	CR104P, full-voltage or transformer-type	
Colors available	Red Amber Green	On, Fast, Forward, Up Down, Reverse, Slow Stopped, Ready



CR7R INDUSTRIAL TIMING CONTROL RELAY



The CR7R industrial control timing relay is a compact relay designed for heavy-duty industrial control applications where reliability and versatility are required.

- Compact mounting dimensions
- Mounted on vertical plane
- Straight-through wiring
- Easy coil replacement
- Long contact life
- High operating speed
- Silver alloy contacts
- Captive terminals
- Rated 600 volts
- UL listed

Auxiliary components convert basic four-pole relay to a four-pole relay with two pneumatic time delay contacts.

Table G.13 Instantaneous relay contacts

Contact arrangement AC controlled	Contact arrangement DC controlled
4 NO	4 NO
3 NO, 1 NC	3 NO, 1 NC
2 NO, 2 NC	2 NO, 2 NC

- Pull-in volts Min. 85% rated voltage
- Drop-out volts 50T or less rated voltage
- Mechanical life In excess of 10 million operations
- Contact life In excess of 1 million operations

Table G.14 AC coil ratings

AC coil rating			
24V/60 Hz	24V/50 Hz	277V/60 Hz	240V/50 Hz
48V/60 Hz	48V/50 Hz	—	380V/50 Hz
120V/60 Hz	110V/50 Hz	—	415V/50 Hz
208V/60 Hz	190V/50 Hz	480V/60 Hz	440V/50 Hz
240V/60 Hz	220V/50 Hz	600V/60 Hz	550V/50 Hz
AC inrush	Holding	DC inrush	Holding
VA	VA	W	W
55	9	8.5	8.5

Table G.15 DC coil ratings

DC coil rating	
24 volts DC	125 volts DC
48 volts DC	250 volts DC

Table G.16 Pneumatic time-delay attachments — 1 NO, 1 NC time delay contacts ①

Time-delay (convertible)	Time range (seconds)
TDAE	0.3-30
TDAE	10.0-180
TDAD	0.3-30
TDAD	10.0-180

① Contacts are in addition to base relay contacts.

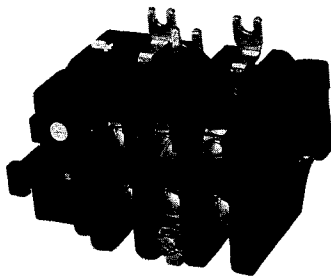
Table G.17 Contact ratings — for relay contacts and timer contacts

Max. AC voltage	Max. continuous amperes	Maximum AC Volt-amperes		Maximum AC amperes		Maximum DC amperes — break or make					
		Make	Break	Make	Break	Relay			Timer		
						24V	125V	250V	24V	125V	250V
600	10	7200	720	60	6	5.0	1.1	0.55	2.5	.55	.27



CR324 BLOCK OVERLOAD RELAYS FOR PANEL MOUNTING

3-POLE 600 VOLTS AC/250 VOLTS DC, 135 MAXIMUM AMPERES CONTINUOUS, UL FILE 2403



APPLICATION

The panel-mount block overload relay with ambient compensation provides overload protection for motors having full-load currents up to 135 amperes. The relays are furnished complete for use on control panels. When an overload condition occurs in any of the three legs in which heaters are inserted, it will cause the relay to trip, opening a normally closed contact, and closing a normally open contact.

A normally open circuit may be connected to a signal light, an alarm bell or input circuit of a programmable controller, e.g., to provide indication of an overload relay trip.

FEATURES

- +10/-10% adjustment of trip current to allow fine tuning and eliminate nuisance tripping
- Bright yellow visual trip indicator tells you at a glance if the relay has tripped
- Manual weld check — Check for welded contacts by depressing the arm to trip the relay and doing a simple continuity check across the terminals
- Dual bimetal current monitoring — Additional bimetal strip “anticipates” the rate of temperature rise in the motor winding, effectively reducing trip time in locked rotor conditions. It prevents dangerous temperature overshoot in the motor windings.
- Flexibility of operation — The trip rating can be easily changed by replacing the front-accessible heaters
- Isolated NO contact — Can be used for input to a programmable controller, an alarm bell, or a signal light
- Safe reset — Operates on upstroke only

Table G.18 Manual reset only

Maximum full-load current in amperes	Size	Control circuit arrangement	Catalog Number
27	1	1 NO, 1 NC	CR324C660A

Table G.19 Contact ratings

Continuous rating amperes	Make amperes	Recommended maximum interrupting capacity, amperes					
		DC circuits		AC circuits			
AC or DC		125V	250V	115V	230V	460V	575V
10	30	0.35	0.17	3	1.5	0.75	0.6



Multilin 269 Plus Motor Management Relay®

PRODUCT DESCRIPTION

The Multilin 269 Plus Motor Management Relay is designed to allow the user to safely maintain maximum-rated motor output without risk of downtime. To achieve this, the 269 Plus system has the following portfolio of Motor Management tools:

- A complete protection package including the unique Multilin features **FlexCurve™** and **MotorMatch™**.
 - **StatTrac™** operation monitoring for effective maintenance.
 - **RelayCom™** option for motor monitoring by computer.
 - Flexibility of control with prior alarms to alert the need for action to maintain operation.
 - Diagnostic data gathering and retrieval to determine the exact cause of shutdown.
 - Exponential running cooldown.
 - Optional metering module with 4 isolated analog outputs.
- The 269 Plus relay is housed in a compact, rugged enclosure compatible with all types of motor starters.

FEATURES

- Rugged, corrosion and flame retardant case.
- Durable polycarbonate front panel.
- 48 character backlit alphanumeric display.
- Red LED on steady when output relay activated.
- Indicator and remote alarm output when self-check detects internal hardware failure.
- Press to display actual motor values of current, temperature, thermal capacity and learned parameters.
- Provides user with application information and programming assistance.
- Allows user to set, alter and examine all alarm, trip and other setpoints.
- Allows user to increment or decrement currently entered setpoint.
- Allows user to scan the next or previous line on the currently selected page.
- Allows user to scan the next or previous page of actual values or setpoints.
- Press to store displayed setpoint in memory when in access mode.
- Use to return from altered setpoint or help message to previous display.
- Permits user to reset latched output relays.

OPTIONS

- Remote Mounted MTM Meter and Transducer Module communicates volts, KW, KVAR, PF and Hz to 269 Plus screen.

EASE OF USE

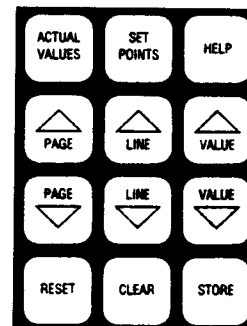
Simple operation

The 269 Plus relay will normally be shipped programmed for most application, and only minor field program changes will be necessary to suit the particular motor.

Use HELP key at any time
for operational assistance.

To facilitate this, the model 269 Plus has the following features:

- Keypad programming
- Tamperproof setpoints
- Backlit, 48-character alphanumeric display
- Question and answer messages
- Request for HELP messages
- Recall of setpoints
- Actual values upon demand
- Output relay status indication

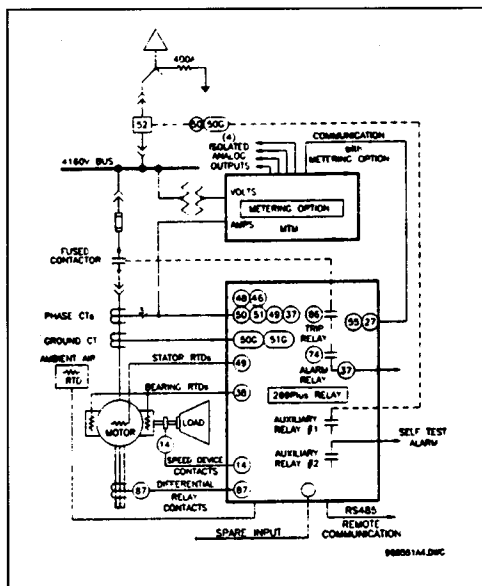


The microcomputer design communicates information to the user through the 48 character alphanumeric display. Just like reading a book, the keypad page and line selection system guides the user through the required setpoint values for optimum motor protection and performance. To aid the user, the HELP key can be pressed at any time to provide additional information and programming assistance. Access for programming is gained by placing a jumper across the access terminals. When programming is complete, the jumper is removed, thus



making the program secure and tamperproof. Alternatively, these terminals can be wired to a separate key-operated shorting switch available as an accessory.

A software access code can also be programmed for added security.



Functional specifications

Motor Management and protection shall be provided by the 269 Plus Protection Relay.

Protective functions must include: Phase overload standard curves (51), overload by custom programmable curve (51), I^2t modeling (49), Stator Overtemperature/Bearing Overtemperature with 10 independent RTD inputs (49), negative sequence unbalance/single phase (46), phase reversal (47), starts per hour and time between starts (48), short circuit (50), ground fault (50G, 50N, 51G, 51N), undercurrent (37) and mechanical jam/stall.

Management functions include:

- Statistical data
- Pre-trip data
- Ability to learn, display and integrate critical parameters to maximize motor protection
- Communication with external devices

The relay shall be capable of displaying important metering functions. As a minimum phase voltages, kilowatt, kilovar, power factor, frequency and MWhr shall be available. In addition, undervoltage (27) and low power factor alarm and trip levels shall be field programmable. It is required that the metering option be a separate box that communicates with the 269 Plus relay and may be field installed without modification to the 269 Plus relay. The metering option can be used with any 269 Plus relay where diagnosis or load measurements are required and shall also provide isolated analog outputs for average RMS amps, kilowatts, kilovars and power factor.

Legend

Device No.	Function
14	Speed Device
37	Undercurrent/Minimum Load
38	Motor/Load Bearing Overtemperature
46	Unbalance — Negative Sequence
47	Phase Reversal
48	Multiple Start/Locked Rotor
49	Stator Winding Overtemperature
49/51	Overload Curves/FlexCurve
50	Short Circuit
	Mechanical Jam/Rapid Trip
50G/51G	Zero Sequence Ground Fault
52	Breaker
74	Alarm Relay
86	Main Trip Latched Relay
	Auxiliary Relay No. 1
	Auxiliary Relay No. 2
	Differential Relay Contact Output
66	Starts Per Hour
27	Undervoltage (Meter Option)
	Frequency (Meter Option)
55	Power Factor (Meter Option)



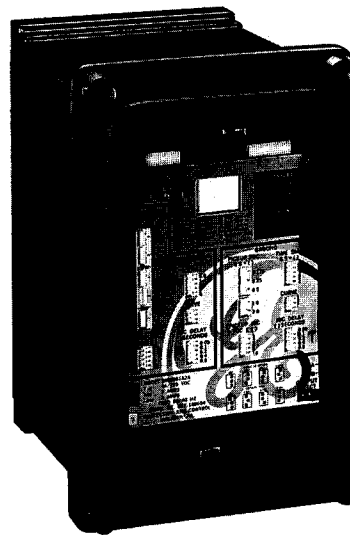
MDP 3-PHASE OVERCURRENT RELAY

DESCRIPTION

The MDP relay is a digital, microprocessor-based non-directional time overcurrent relay that protects against phase-to-phase and phase-to-ground faults. The MDP series relay includes four measuring units, including one for each of the three phases in addition to ground. Each measuring unit contains a time overcurrent unit and an instantaneous unit.

FEATURES

- Information
 - Last trip current
 - Last trip time
 - Trip indication
 - Pickup indication
 - Breaker status
- Eight selectable curves
 - Inverse (51)
 - Very inverse (53)
 - Extremely inverse (77)
 - Long-time inverse (66)
 - Four definite times
- Enhanced selectivity
 - Block instantaneous
 - Block ground
 - Instantaneous delay
 - Breaker status
- Configurable outputs
 - 5 output relay contacts
- Communications
 - Field upgradeable communications
 - Interfaces with POWER LEADER distribution software
- Other
 - Meets ANSI C37.90, BS142 and IEC 255
 - Drawout construction (S2 case)
 - External reset lever

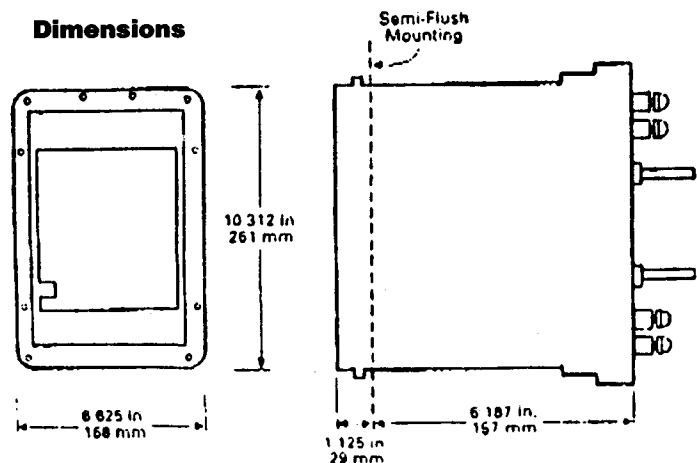


MDP Relay

MDP	*	*	*	0000A
I				
0				No communications or digital inputs
1				Digital inputs* and communication socket
2				Commnet communications card installed
A				RS232 communications option**
			1	5A, 1.5 to 13.125A phase, 0.5 to 4.375 ground
			2	5A, 1.5 to 13.125A phase, 1.5 to 13.125 ground
			3	5A, 1.5 to 13.125A phase, 0.1 to 0.875 ground
			4	1A, 0.3 to 2.625A phase, 0.1 to 0.875 ground
			5	1A, 0.3 to 2.625A phase, 0.3 to 2.625 ground
			6	1A, 0.3 to 2.625A phase, 0.05 to 0.4375 ground
			1	24-48 volts DC
			2	48-125 volts DC
			3	125-250 volts DC

* Digital inputs include block ground, block IOC and breaker status
 ** RS232 communications is not field upgradeable; breaker status not available
 *** MDPCMN upgrade communications card

Dimensions





HFC INSTANTANEOUS OVERCURRENT

The HFC relay is a hinged armature instantaneous device with two electrically separate contacts, assembled in a C1 single end drawout case. Each unit contains a target, which is raised into view and latched when the relay is picked up. The targets are manually reset by a button on the front of the relay cover.

The HFC is generally applied where a direct trip instantaneous overcurrent function is required.

The relay can be used to provide differential protection of a motor usually by means of self balanced primary current scheme with the current transformers mounted at the machine terminals.

Table G.20 Selection guide

Current range		Number of units	Model number	Case size	Weight lbs (kg) NET
Minimum	Maximum				
0.5 2.0	4.0 50	3	12HFC23C1A 12HFC23C2A	C1	8 (3.6)

Table G.21 Tapped coil ratings

Instantaneous unit (amps)	Range Link position	Rating (amps)	Continuous 1-second (amps)	Rating	K
0.5-4	L	0.5-2	0.75	94	8,836
	H	2-4	1.5		
2-50	L	2-10	3.7	130	16,900
	H	10-50	7.5		

Table G.22 Burden 60 Hz unit

Instantaneous unit (amps)	Link position	Burden at minimum pickup (ohms)			Burden times pickup (ohms)		
		R	X	Z	3	10	20
0.5-4	L	10.63	9.77	14.44	9.81	8.56	7.8
	H	5.13	3.49	6.21	4.66	4.26	4.18
2-50	L	0.750	0.650	0.992	0.634	0.480	0.457
	H	0.070	0.024	0.074	0.072	0.071	0.070



IJD PERCENTAGE-DIFFERENTIAL

DESCRIPTION

The type IJD relays are induction disk units used to protect AC rotating machines, two winding transformers, and wye winding of power transformers. IJD relays protect against phase-to-phase faults within the AC machine and the lead in the differential zone, provided the fault current is above the minimum pickup value.

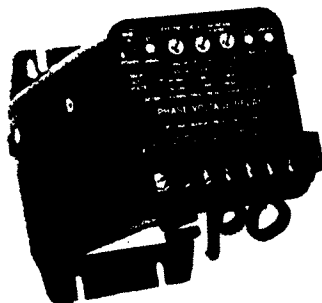
Model number	Frequency	Continuous rating (amperes)	Min. operating Current (amperes)	Min. operating Slope (percent)
Type IJD52A — 2 NO contacts, S1 case construction				
12IJD52A12A	60	5	0.5	25



THREE-PHASE VOLTAGE MONITORS

MODEL LPVR

UL-listed File number E103039

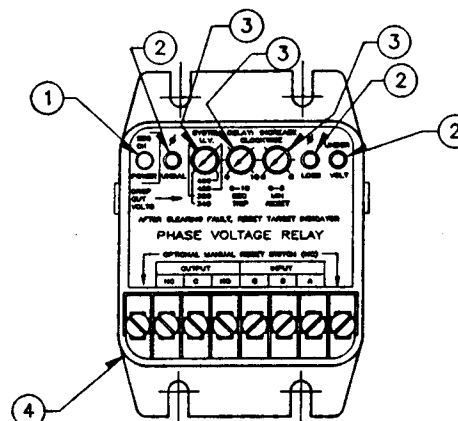


GENERAL

The model LPVR is a three-phase voltage monitor that uses negative phase sequence monitoring to protect against phase loss, phase reversal and undervoltage on the power system. Electromechanical diagnostic indicators (manually reset) show trip conditions due to phase unbalance, phase loss and undervoltage. A green LED indicates that the power system has no faults present and that the phases are in sequence.

Model LPVR specifications:

- Provides prestart and running protection
- Fully rated 600 volt contacts
- Diagnostic indicators continue to show cause of operation after voltage is removed
- Adjustable undervoltage trip point settable to 75% of nominal
- Adjustable trip delay from 50 milliseconds to 10 seconds
- Adjustable reset delay from 1 second to 5 minutes
- Operates at 6% phase unbalance
- Maintains operation with a 12.5% phase voltage loss
- Automatic or manual reset, local or remote
- Operational green LED indicator
- Fail-safe — will not operate if fault is present
- Isolated Form "C" output contacts
- Terminal screws are #6-32 nickel-plated brass



① GREEN LED INDICATOR:

- Power system condition

② ELECTROMECHANICAL DIAGNOSTIC INDICATORS:

- Phase unbalance
- Phase loss
- Undervoltage

③ ADJUSTABLE SYSTEM DELAYS:

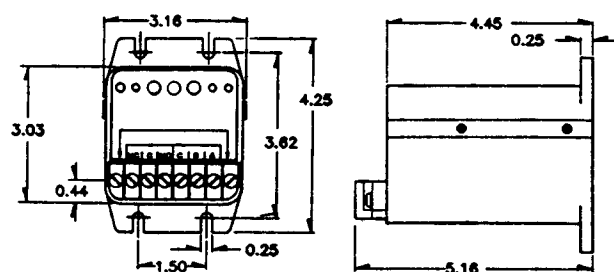
- Undervoltage trip point
- .05-10 second trip delay
- 0-5 minute reset delay

④ TERMINAL BLOCK:

- Automatic or manual reset
- Input voltage — 120-575 volts
- Output contacts — Form "C," 1 NO & 1 NC

Table G.23 Three-phase voltages available with Model LPVR

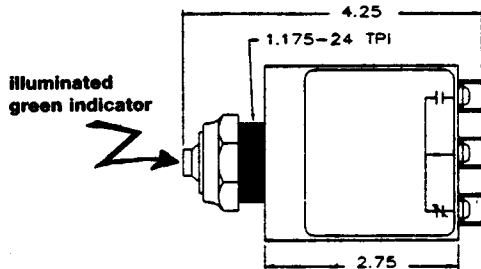
Catalog Number	Nominal rating	Voltage range
LPVR 120	120	90-125
LPVR 240	240	180-250
LPVR 480	480	360-500
LPVR 575	575	430-600





MODEL APVR

UL-listed File number E103039



GENERAL

The model APVR phase-sensing relay performs similarly to the model LPVR, except that the relay requires no adjustments. It will fit in the push button bracket, and thus does not increase the required unit spacing.

Model APVR specifications:

- Fail-safe — will not operate if a fault is present
- Manual or automatic reset
- Fixed undervoltage trip point: Approximately 90% pickup, 80% dropout
- Operates at 6% phase unbalance
- Maintains operation with a 6% phase voltage loss
- 3-second dropout delay to avoid nuisance tripping
- Operational green LED indicator
- Isolated Form “C” output contacts
- Output contact rating: 250 volts AC, 5 amperes (general use); 30 volts AC, 5 amperes (resistive)

Table G.24 Three-phase voltages available with Model APVR

Catalog number	Nominal rating	Voltage range	Frequency
APVR 120	120	95-135	60 Hz
APVR 240	240	190-270	60 Hz
APVR 480	480	380-530	60 Hz
APVR 575	575	455-600	60 Hz
APVR380	380	300-425	50 Hz



POWER LEADER™ EPM

GENERAL

The POWER LEADER EPM is a microprocessor-based device that displays a full range of over 50 metered values with revenue class accuracy of 0.5%. The PL-EPM is available with a communication option that is factory- or field-installable so that all data can be transmitted to a remote host computer.

FEATURES

The PL-EPM comes in the standard S1 case as the present DS-63 and DS-65 electromechanical watt-hour meters. This provides the user the ability to retrofit the electromechanical meters with the PL-EPM. Metered values cover a full range of parameters:

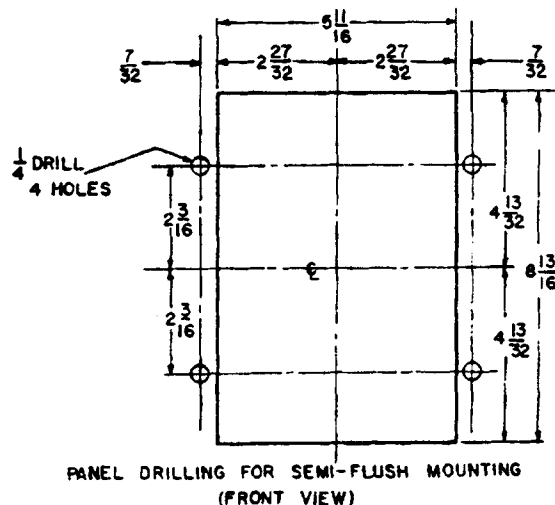
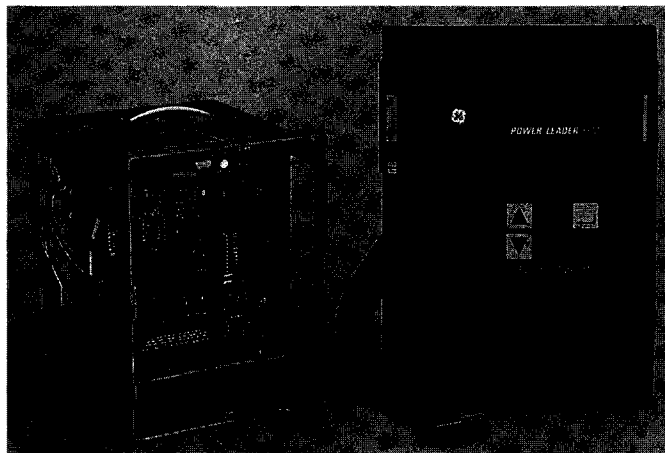
- Revenue Class accuracy of 0.5%
- Optional communications provide connectivity to POWER LEADER network (Commnet)
- Pulse initiation option with programmable outputs

(kWh, kVAh, kVAh, kQh)

Amperes	3-phase and neutral (0.25% accuracy)
Volts	L-L and L-N (0.25% accuracy)
Watts	per phase, 3-phase total, peak watts, watt demand, and watts at maximum kVA
Energy	kwh, kVAh, kVAh lag and lead, and kQh
Volt-amperes	per phase, 3-phase total, peak kVA and kVA demand
KVARs	per phase, 3-phase total, peak kVar, peak kVar lead, kVar demand, kVar demand lead
Power factor	per phase, 3-phase total, average, power factor at previous interval, power factor at maximum kVA
Frequency	60 Hz check factory for 50 Hz availability

INPUTS

The PL-EPM requires CT inputs with a 5-ampere secondary current. The meter can accept direct input voltages up to 600 volts and is self-powered from the voltage inputs. Three CTs are required for four wire wye-systems and two CTs are required for three wire delta-system.

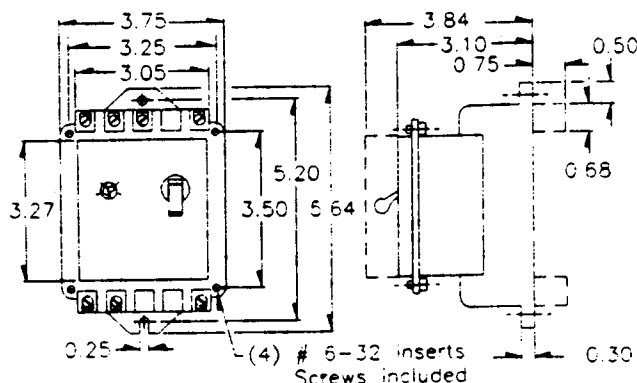
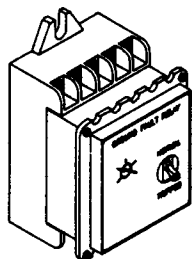




GROUND FAULT SYSTEM

MODEL GFM

UL-listed File number E110395



SENSORS

Model number	Trip current	Window size
GFM 250	3.5 to 11	2.5"
GFM 462	4 to 12	4.62"

- Self powered.
- Temperature range: -30° C to 75° C.
- Positive "ON" (green) and "OFF" (red) condition indication, manual reset.
- Instantaneous only (GFM-353) standard.
- Optional time delay from instantaneous to 36 cycles (GFM-363).

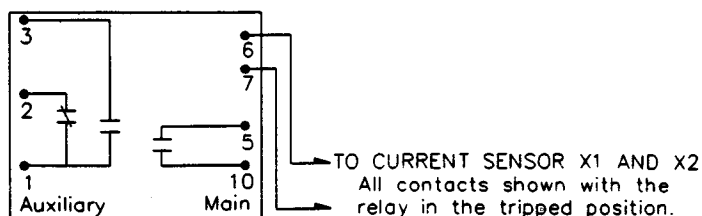
GENERAL

These Class 1 model GFM ground fault protection systems are designed to minimize damage or loss to equipment caused by destructive arcing ground faults. This GFM system is designed for all polyphase applications and is ideally suited for motor control, motor control centers and high-voltage starters. Systems can be wye or delta, grounded or resistance grounded. When the ground fault current exceeds a preselected condition (current only, or current and time settings), the relay trips. The relay contacts can be connected in the control circuit of a motor starter, to the shunt trip of a circuit breaker or similar disconnecting or alarm devices. The system has an inverse time characteristic to prevent nuisance tripping. The relay tripping current value is field adjustable over the trip current range of the sensor. The adjustable trip time delay relay, when specified, is field settable up to 36 cycles.

MODEL GFM 353

Main contact rated 30 amperes, 277 volts AC.

Auxiliary contacts rated 10 amperes continuous, 23 amperes inrush, 120 volts AC.





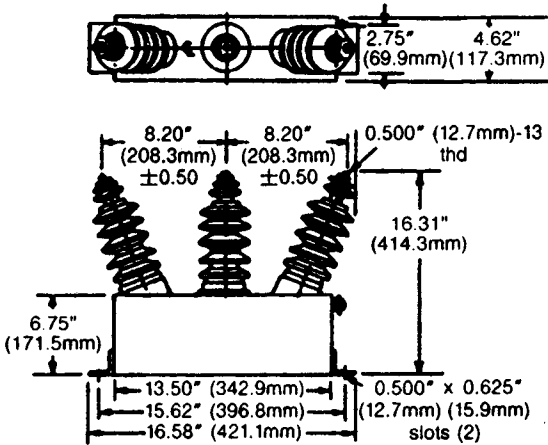
AC ROTATING-MACHINE PROTECTION

DIELEKTROL® PROTECTIVE CAPACITORS

0-18,000-ft. altitude

DIELEKTROL is the GE non-PCB power capacitor dielectric system, developed to provide an environmentally acceptable product with superior performance and reliability. The DIELEKTROL insulating liquid is a Class IIIB combustible fluid.

Protective capacitors contain a film dielectric and hermetically sealed bushings, which permit mounting of capacitors in an upright position or on the side.



Three-pole capacitor, 4160 volts

Table G.25 DIELEKTROL non-PCB dielectric protective capacitors with internal discharge resistors — indoor and outdoor mounting

Voltage rating RMS volts L-L	Maximum voltage RMS volts L-L	Catalog number	Poles per unit	Microfarads per pole	Approximate net weight	
					Lb	Kg
2400 or 4160	4576	18L15UJ	3	1.5	35	15.8



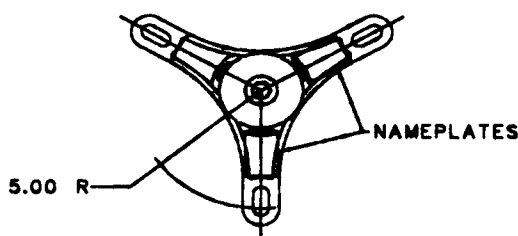
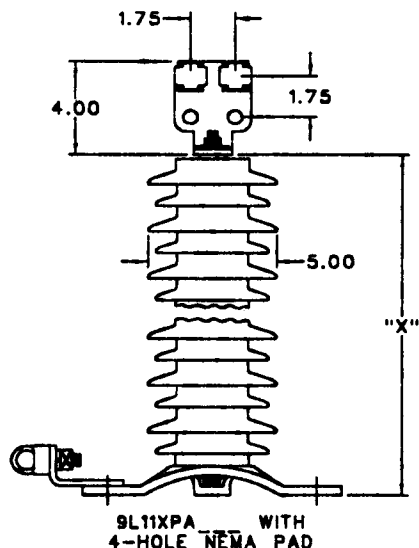
TRANQUELL® XEP™—STATION ARRESTERS

POLYMER HIGH-VOLTAGE

DESCRIPTION

Tranquell XEP polymer station arresters provide both excellent protective characteristics and temporary over-voltage capability. Gapless construction results in a design that is simple, reliable and economical while offering excellent pressure relief capability to meet the

most demanding service conditions. The GE arrester is based on the field-proven Zenox™ — metal oxide disks known for maintaining stable characteristics. Tranquell station arresters are designed and manufactured in accordance with ANSI/IEEE C62.11.



ALL LINE AND GROUND
TERMINALS ACCOMMODATE
CONDUCTOR SIZES
FROM #2 AWG TO 350 MCM

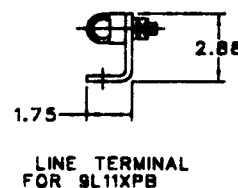
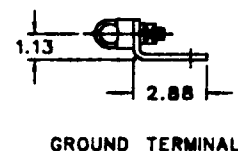


Table G.26 Polymer arrester (station-class) ratings

Arrester rating ① (kV RMS)	Maximum continuous operating voltage capability① (L-N) (kV RMS)	Normally used on system voltage class (L-L)		Single-pole arrester Catalog number Gray polymer housing with eyebolt (small diameter)
		Delta or impedance grnd. neutral sys. (kV RMS)	Solidly grnd. neutral sys. (kV RMS)	
3	2.55	2.4	4.16	9L11XPB003
6	5.10	4.8	—	9L11XPB006

① TRANQUELL arresters are designed to be operated at voltages equal to or less than their continuous capability. **Note:** For ratings above 360kV, contact factory.

② Application of specified rating is permissible for ungrounded or resistance grounded system where a single phase ground may be tolerated for a substantial period of time not to exceed the TRANQUELL arrester's overvoltage capability as described in GET-6951.

Note: Contact factory or GE Sales Office for Design Test data.

Table G.27 Polymer station arrester weights and dimensions

Catalog Number	Arrester Rating (kV rms)	Height (X)		Creep		Weight		Min. Clearance		Min. Mounting Spacing on Center			
		In	mm	In	mm	lb	kg	In	mm	Phase to Phase		Phase to Ground	
										In	mm	In	mm
9L11XPB003	3	7.9	200.7	17.2	436.9	7.9	3.6	2.0	50.8	12.3	312.4	7.7	195.6
9L11XPB006	6	7.9	200.7	17.2	436.9	8.1	3.7	3.0	76.2	12.3	312.4	7.7	195.6



STANDARD SERVICE CONDITIONS

Limitamp equipment is designed for the following standard conditions: Operating ambient temperature -20° C to 40° C. Storage ambient temperatures -40° C to 70° C; strip heaters with thermostat control are recommended at 0° C. One heater per enclosure. Thermostats may control up to 14 heaters.

- Altitude to 3,300 feet above sea level
- Humidity 0 to 90 percent (non-condensing)

SEISMIC CAPABILITY

Vacuum Limitamp Controllers can be used in various applications subject to shock and/or vibration. Certain controllers will withstand forces generated by a Zone 4 earthquake as defined in 1985 uniform building code for non-essential equipment when properly anchored at ground level.

For Limitamp control with seismic capability, or other vibration-type applications, refer your application details to the factory.

ALTITUDE DERATING

Vacuum Limitamp Controllers, including power fuses, require the following derating for use at high altitudes:

- For current — No derating required up to 6,000 feet above sea level.
- Above 6,000 feet, derate by 0.9 percent for every 1,000 feet above sea level.
- For voltage — No derating required up to 3,300 feet above sea level.
- Above 3,300 feet, derate by 2 percent for every 1,000 feet above sea level. BIL rating is also derated by the same percentage.

TEMPERATURE DERATING

Vacuum Limitamp Controllers require the following current derating for ambient temperature. Use only bolt-on fuses.

- Up to 40° C — No derating
- 40-45° C — Derate 10 percent
- 45-50° C — Derate 20 percent
- Above 50° C — Consult factory on the application

ESTIMATED HEAT LOSS

The following data can be used for estimating heat loss of Limitamp controllers at rated load amps. The esti-

mates are based upon a single full-voltage non-reversing 400 ampere induction motor controller with basic panel options.

- CR194 Vacuum - 370 watts per contactor
- CR7160 Air break - 670 watts per contactor

STANDARDS AND CODES

Limitamp controllers are designed to meet NEMA Standard ICS 3, Part 2 for Class E2 Controllers, and UL Standard 347 for high-voltage industrial control equipment under UL File E57411.

When specified, Limitamp control may be built to comply with the City of Chicago Code and the California Code.

Each UL-listed section includes a UL section nameplate and each UL-listed motor controller includes a UL controller label.

Additional information can be found in Table A.3.

GE UL-LISTED VACUUM CONTROLLERS

- A.** Full-voltage non-reversing induction motor starters, 2400-4800 volts, up to 400 amperes rating.
- B.** CR194 one-high NEMA 1 enclosure, 26W or 34W x 90H x 30D, with stationary mounted vacuum contactor and DC operating coil.

CR194 two-high NEMA 1 enclosure, 36W or 40W x 90H x 30D, with stationary or drawout mounted vacuum contactor and DC operating coil.
- C.** GE Type RA or RB current limiting power fuses.
- D.** Ambient compensated thermal overload relays (CR324C).
- E.** Solid state overload (CR324CX).
- F.** 1000 or 2000 amp copper main bus. (Refer to factory for 1200 amp main bus application)
- G.** Phase and ground current transformers.
- H.** Control power transformer with primary and secondary fuse protection.

GE UL-LISTED AIR MAGNETIC CONTROLLERS

- A.** Full-voltage non-reversing induction motor starters, 2400-4800 volts, up to 400 ampere rating.
- B.** CR7160 one- high construction in 34W x 90H x 30D or two- and three- high construction in 44W x 90H x 30D, in NEMA 1 enclosures.
- C.** Same as listed above for C, D, F, G.
- D.** 1000 or 2000 amp copper main bus, silverplated.



APPROVED COMPONENTS FOR GE CONTROLLERS

- A. Any UL-listed low-voltage component
- B. Current transformers
- C. Control wire, Type MTW, THW, SIS, XHHN
- D. Power wire — MV-90 Dry
- E. Control power transformers

See Table A.3 for details.

STANDARD PAINT SYSTEM — INDOOR & OUTDOOR EQUIPMENT

The standard Limitamp paint system consists of the following two processes:

Phase I — Cleaning

In a seven-stage spray washer, steel parts are cleaned and sprayed in controlled cleaning solutions.

Cleaned steel parts enter a drying oven at 300-350° F. The preceding operating parameters have been deter-

Stage	Temperature	Chemical Solution(s)
1 — Cleaning	115-120°	Ridoline
2 — Rinse	105-118°	Bonderite
3 — Iron Phosphate	90-105°	Bonderite, Soda Ash
4 — Rinse	Ambient	None
5 — Acidated Rinse	Ambient	Parcolene
6 — Rinse	Ambient	None
7 — Deionized Rinse	Ambient	None

mined to produce an Iron Phosphate coating of a minimum of 150 milligrams per square foot to meet MIL Spec. TT-C-490.

Phase II — Painting by electro-static powder process

670-011 ANSI-61 Polyester Finish Paint (Light Gray)

Metal parts will enter a drying oven at 375-400° F and remain for 20 minutes. The standard color finish is ANSI-61 light gray with a gloss of 60 plus or minus five and a thickness of 2.5 mils. This system will withstand a minimum of 1000 hours salt spray test.

H



STANDARD COMMERCIAL TESTS AND INSPECTIONS

GENERAL

The following summary description defines the standard factory tests and inspections performed during manufacture of Limitamp Control. All Limitamp equipment is tested and inspected for conformance with NEMA ICS 3 part 2 and UL347.

Production tests and inspections encompass the verification of physical configuration of assembly and workmanship, the mechanical adjustments of parts and components, and the sequencing and functional operations of the control systems. These tests and inspections are performed on manufactured products to verify conformance of the equipment to a previously qualified design. The tests do not include type testing or other destructive tests on equipment to be shipped to a customer.

Any additional factory tests beyond those listed in the following paragraphs must be referred to the factory to verify availability of test facilities and qualified manpower. Additional testing beyond the scope of the following standard commercial tests will affect normal shipment schedules.

PRODUCTION TESTS

The following list of inspection activities shall be performed to assure proper and correct materials, workmanship and for any damage conditions in accordance with the manufacturing documentation and drawings:

- Components, parts and material
- Physical condition of components, parts, wire insulation
- Location and orientation of components and parts
- Finish — plating — painting
- Wire/cable type, size, insulating and clamping support
- Wire terminations, insulation removal and crimping of terminals
- Tightness of electrical connections and torque of bus bar bolts
- Wire markers and terminal markers (where specified)
- Labeling of components, parts, etc.
- Tightness torque of assembly bolts and hardware
- Welds (spot only)
- Mechanical clearance
- Electrical clearance (potential hazards)

MECHANICAL OPERATION TESTS

Mechanical operating tests shall be performed to ensure proper functioning of operating mechanisms and interlocks. The operation of shutters, mechanical interlocks,

circuit-breaker-door interlocks, operating handles, trip mechanisms, solenoid armature travels, contact wipes, electro-mechanical interlocks, physical clearances for mechanical and electrical isolation including any additional mechanically related operating functions shall be verified.

CONTINUITY TESTS — CONTROL WIRING AND POWER CABLES

The correctness of the individual circuit wiring contained in each assembly and the assembly wiring interfaces shall be verified as in accordance with the connection diagram, wiring table, or elementary drawing. The continuity of each circuit shall be checked.

OPERATIONS TEST

All equipment shall be subjected to an operational test. The test shall verify the functional operation of the control and power circuits and related components, devices and subassembly-modules under simulated operating conditions (excluding loading of the power circuits).

a. Devices

All devices, including subassembly-modules, shall be operated, set and checked for their functional characteristics in accordance with the instructions for each and any additional characteristic peculiar to the device:

- Pick-up
- Drop-out
- Contact wipe
- Amperes
- In-rush current
- Time-delay

Contactors must pick-up and hold-in at or below the following percentage of rated coil voltage:

Device Type	Voltage Source	Pick-up (Percentage)
DC	DC	65
AC	AC	85 ^①
DC	AC with rectifier	70 with holding resistor
DC	AC with rectifier	70 with holding and pick-up resistor

^① If a CPT is used, apply 90% voltage to transformer primary.



b. Sequence and timing circuits

Assemblies and systems involving sequential operation of devices and time delays shall be tested to assure that the devices in the sequence function properly and in the order intended.

c. Polarity — phase-sensitive circuits

The polarity of direct-current circuits and phase connections of alternating-current circuits shall be verified by application of power and measurement of the relative polarities and phase sequence.

d. Grounding

The grounding circuits and buses shall be certified.

HIGH POTENTIAL — INSULATION TESTS

a. Control wiring insulation tests

A dielectric test (hi-pot) shall be performed on circuit wiring to confirm the insulation resistance to withstand breakdown to a selected test voltage. The test voltage — amplitude and waveshape, method of application and duration of time applied — shall be specified in UL347.

b. Power cable insulation and isolation test

Power cables and buses shall be tested, phase-to-phase and phase-to-ground for insulation breakdown resistance and circuit isolation as specified in UL347.

Note: These test conditions are as specified for newly constructed equipment and performed in a clean, temperature and humidity controlled factory environment.

Rated Circuit Voltage AC or DC	High Potential Test Voltage	Duration of Test
120	1500	1 second
140	1800	1 second
480/600	2700	1 second
2300	7200	60 seconds
5000	13,250	60 seconds
7200	18200	60 seconds

These test voltages include the standard test voltages:

a. For equipment rated under 600 volts RMS or DC:

Two times rated plus 1000, times 120 percent (for one-second application).

b. For equipment rated over 600 volts RMS or DC:

Two-and-a-fourth times rated plus 2000 (60 seconds only).

The frequency of the test voltage shall not be less than the rated frequency of the equipment tested and shall be essentially sinusoidal in wave shape.

Note: Consideration shall be made for low-voltage devices, semiconductors, meters, instruments, transformers, grounding circuits, etc., in preparation for the dielectric tests.

INSULATION RESISTANCE (MEGGER) TESTS

Insulation resistance tests measure the amount of circuit resistance to current leakage. This test is performed when this resistance measurement is desired and so specified.

The test voltage and minimum insulation resistance shall be selected as specified. Examples of test values are:

- a. 500 volts DC with 10 megohms minimum
- b. 1000 volts DC with 1 megohm minimum
- c. 1000 volts DC with 25 megohms minimum

Desired values must be specified by the customer, as no NEMA standard defines Megger values for motor controls.



ANSI STANDARD DEVICE FUNCTION NUMBERS

Dev. No.	Function
1	Master Element
2	Time-Delay Starting or Closing Relay
3	Checking or Interlocking Relay
4	Master Contactor
5	Stopping Device
6	Starting Circuit Breaker
7	Anode Circuit Breaker
8	Control Power Disconnecting Device
9	Reversing Device
10	Unit Sequence Switch
11	(Reserved for future application)
12	Over-Speed Device
13	Synchronous-Speed Device
14	Under-Speed Device
15	Speed or Frequency Matching Device
16	(Reserved for future application)
17	Shunting or Discharge Switch
18	Accelerating or Decelerating Device
19	Starting-to-Running Transition Contactor
20	Electrically Operated Valve
21	Distance Relay
22	Equalizer Circuit Breaker
23	Temperature Control Device
24	(Reserved for future application)
25	Synchronizing or Synchronism-Check Device
26	Apparatus Thermal Device
27	Undervoltage Relay
28	Flame Detector
29	Isolating Contactor
30	Annunciator Relay
31	Separate Excitation Device
32	Directional Power Relay
33	Position Switch
34	Master Sequence Device
35	Brush-Operating or Slip-Ring Short-Circuiting Device
36	Polarity or Polarizing Voltage Device
37	Undercurrent or Underpower Relay
38	Bearing Protective Device
39	Mechanical Condition Monitor
40	Field Relay
41	Field Circuit Breaker
42	Running Circuit Breaker
43	Manual Transfer or Selector Device
44	Unit Sequence Starting Relay
45	Atmospheric Condition Monitor
46	Reverse-Phase or Phase-Balance Current Relay
47	Phase-Sequence Voltage Relay
48	Incomplete Sequence Relay
49	Machine or Transformer Thermal Relay
50	Instantaneous Overcurrent or Rate-of-Rise Relay

51	AC Time Overcurrent Relay
52	AC Circuit Breaker
53	Exciter or DC Generator Relay
54	(Reserved for future application)
55	Power Factor Relay
56	Field Application Relay
57	Short-Circuiting or Ground Device
58	Rectification Failure Relay
59	Overvoltage Relay
60	Voltage or Current Balance Relay
61	(Reserved for future application)
62	Time-Delay Stopping or Opening Relay
63	Pressure Switch
64	Ground Protective Relay
65	Governor
66	Notching or Jogging Device
67	AC Directional Overcurrent Relay
68	Blocking Relay
69	Permissive Control Device
70	Rheostat
71	Level Switch
72	DC Circuit Breaker
73	Load-Resistor Contactor
74	Alarm Relay
75	Position Changing Mechanism
76	DC Reclosing Relay
77	Pulse Transmitter
78	Phase-Angle Measuring or Out-of-Step Protective Relay
79	AC Reclosing Relay
80	Flow Switch
81	Frequency Relay
82	DC Overcurrent Relay
83	Automatic Selective Control or Transfer Relay
84	Operating Mechanism
85	Carrier or Pilot-Wire Receiver Relay
86	Locking-Out Relay
87	Differential Protective Relay
88	Auxiliary Motor or Motor Generator
89	Line Switch
90	Regulating Device
91	Voltage Directional Relay
92	Voltage and Power Directional Relay
93	Field-Changing Contactor
94	Tripping or Trip-Free Relay
95	
96	Used only for specific applications in individual installations where none of the assigned numbered functions from 1 to 94 are suitable.
97	
98	
99	



Table H.1 Motor Current Limiting Fuse And Current Transformer Ratio Selection (For Estimating Only) Based Upon 600% Locked Rotor Current

Motor Horsepower	Typical FLA	CT Ratio	EJ2 Rating	Typical FLA	CT Ratio	EJ2 Rating
	2400 volts			4160 volts		
150	35	50/5	3R	20	25/5	3R
200	46	75/5	4R	25	40/5	3R
250	57	75/5	4R	33	50/5	3R
300	69	100/5	6R	41	75/5	3R
350	81	150/5	6R	47	75/5	4R
400	92	150/5	6R	54	75/5	4R
450	105	150/5	9R	60	75/5	4R
500	113	150/5	9R	66	100/5	6R
550	123	200/5	9R	73	100/5	6R
600	135	200/5	9R	80	100/5	6R
650	145	200/5	12R	87	150/5	6R
700	155	200/5	12R	93	150/5	6R
750	166	300/5	12R	100	150/5	9R
800	176	300/5	12R	106	150/5	9R
850	186	300/5	12R	113	150/5	9R
900	197	300/5	18R	120	150/5	9R
950	207	300/5	18R	126	200/5	9R
1000	218	300/5	18R	133	200/5	9R
1200	266	400/5	18R	152	200/5	12R
1250	279	400/5	18R	158	200/5	12R
1500				187	300/5	12R
1750				217	300/5	18R
2000				246	400/5	18R

Table H.2 CT Ratio Based on Rated Load Current

Current	CT Ratio	Current	CT Ratio
10-14A	20/5	121-160A	200/5
15-24A	30/5	161-255A	300/5
25-40A	50/5	256-355A	400/5
41-60A	75/5	356-480A	600/5
61-80A	100/5	481-670A	800/5
81-120A	150/5		

Table H.3 Fuse Selection Based On Full Load Current

FUSE SELECTIONS (Assumes 600% locked rotor)	
0- 44A	3R
45-62A	4R
63-94A	6R
95-140A	9R
141-184A	12R
185-276A	18R
277-360A	24R
361-408A	P425
409-510A	P550
511-630A	P630
631-800A	P800

Table H.4 Fuse Ratings For Transformer Feeders (For Estimating Only)

Three- Phase Transformer	2400 volts		4160 volts	
	Full Load Current	Fuse	Full Load Current	Fuse
9	2.16	7E	1.25	5E
15	3.6	10E	2.08	7E
30	7.2	20E	4.2	15E
45	10.8	25E	6.2	15E
75	18	30E	10.4	25E
112.5	27	40E	15.6	30E
150	36	50E	20.8	40E
225	54	65E	31.3	50E
300	72	100E	41.6	50E
500	120	150E	69.4	80E
750	180	200E	104	125E
1000	240	250E	139	150E
1500	361	400E	208	250E
2000	—	—	278	300E
2500	—	—	347	400E





ESTIMATING POWER FACTOR CORRECTION CAPACITOR RATINGS

Table H.5 2400-Volt and 4160-Volt Motors, Enclosure Open — Including Drip-proof and Splash-proof, GE Type K (NEMA Design “B”), Normal Starting Torque and Current

Induction Motor HP Rating	Nominal Motor Speed in RPM Number of Poles											
	3600 2		1800 4		1200 6		900 8		720 10		600 12	
	kVAr	% AR	kVAr	% AR	kVAr	% AR	kVAr	% AR	kVAr	% AR	kVAr	% AR
100	—	—	25	11	25	12	50	24	25	14	25	20
125	—	—	25	9	25	12	25	13	25	14	50	20
150	25	9	25	9	25	12	50	13	50	14	75	20
200	25	9	50	9	50	12	50	13	75	14	100	20
250	25	9	25	8	50	12	75	13	75	14	100	20
300	50	9	50	8	75	12	100	13	100	14	125	20
350	75	9	50	8	75	12	100	12	100	14	125	19
400	75	9	50	8	100	12	100	12	125	14	150	19
450	100	9	75	8	100	12	125	11	125	14	150	19
500	100	9	100	8	125	12	125	11	150	14	200	19
600	125	9	125	8	175	12	150	11	150	14	200	17
700	150	8	150	8	200	11	150	10	200	14	200	15
800	175	8	150	7	175	10	175	10	225	13	250	15

Table H.6 2400-Volt and 4160-Volt Motors, Totally Enclosed, Fan-cooled, GE Type K (NEMA design “B”), Normal Starting Torque and Current

Induction Motor HP Rating	Nominal Motor Speed in RPM Number of Poles											
	3600 2		1800 4		1200 6		900 8		720 10		600 12	
	kVAr	% AR	kVAr	% AR	kVAr	% AR	kVAr	% AR	kVAr	% AR	kVAr	% AR
100	—	—	25	17	—	—	50	22	25	12	50	15
125	—	—	50	17	25	15	50	17	25	12	50	15
150	25	6	25	12	50	15	50	17	50	12	75	15
200	25	6	50	12	75	15	50	17	50	12	100	15
250	25	6	50	11	75	15	75	17	75	12	100	15
300	50	6	50	11	75	13	125	17	100	12	125	15
350	50	6	60	11	75	13	125	17	125	12	150	15
400	75	6	125	11	125	13	150	17	150	12	200	15
450	75	6	125	10	150	13	175	17	200	12	225	15
500	75	6	125	8	175	13	225	17	225	12	225	15



Table H.7 2400-Volt and 4160-Volt Motors, Enclosure Open — Including Drip-proof And Splash-proof, GE Type KG (NEMA design “C”), High-starting Torque, Normal Starting Current

Induction Motor HP Rating	Nominal Motor Speed In RPM Number of Poles							
	1800 4		1200 6		900 8		720 10	
	kVA _r	% AR	kVA _r	% AR	kVA _r	% AR	kVA _r	% AR
100	—	—	—	—	—	—	25	14
125	25	10	25	11	25	13	25	14
150	25	8	25	9	50	13	50	14
200	25	7	50	12	50	13	75	14
250	25	8	50	12	75	13	75	14
300	50	8	75	12	100	13	100	14
350	50	8	75	12	100	12	100	14

Table H.8 2400-Volt and 4160-Volt Motors, Totally Enclosed, Fan-cooled, GE Type KG (NEMA Design “C”), High-starting Torque, Normal Starting Current

Induction Motor HP Rating	Nominal Motor Speed In RPM Number of Poles							
	1200 6		900 8		720 10		600 12	
	kVA _r	% AR	kVA _r	% AR	kVA _r	% AR	kVA _r	% AR
75	—	—	—	—	—	—	—	—
100	—	—	—	—	25	12	50	15
125	25	10	50	17	25	12	50	15
150	—	—	50	17	50	12	75	15
200	75	15	50	17	50	12	100	15





ESTIMATED TYPICAL KW RATINGS OF EXCITERS FOR 60-HERTZ SYNCHRONOUS MOTORS

When synchronous motors have individual exciters, the kilowatt ratings in Table H.7 represent typical kilowatt ratings for such exciters.

Table H.9 Exciter ratings for synchronous motors, 60 Hz, 1.0 power factor

HP	RPM	Exciter Ratings, kW												
		1800	1200	900	720	600	514	450	400	360	300	240	200	180
200		2.0	3.0	3.0	3.0	4.5	4.5	4.5	4.5	4.5	6.5	6.5	6.5	6.5
250		2.0	3.0	3.0	4.5	4.5	4.5	4.5	6.5	6.5	6.5	6.5	9.0	9.0
300		2.0	3.0	4.5	4.5	4.5	4.5	6.5	6.5	6.5	6.5	9.0	9.0	9.0
350		3.0	3.0	4.5	4.5	4.5	6.5	6.5	6.5	6.5	6.5	9.0	9.0	9.0
400		3.0	3.0	4.5	4.5	6.5	6.5	6.5	6.5	6.5	9.0	9.0	9.0	13
450		3.0	4.5	4.5	4.5	6.5	6.5	6.5	9.0	9.0	9.0	9.0	13	13
500		3.0	4.5	4.5	4.5	6.5	6.5	6.5	9.0	9.0	9.0	9.0	13	13
600		3.0	4.5	6.5	6.5	6.5	6.5	9.0	9.0	9.0	9.0	13	13	13
700		4.5	4.5	6.5	6.5	6.5	9.0	9.0	9.0	9.0	13	13	13	13
800		4.5	6.5	6.5	6.5	9.0	9.0	9.0	13	13	13	13	13	13
900		4.5	6.5	6.5	9.0	9.0	9.0	9.0	13	13	13	13	17	17
1000		4.5	6.5	9.0	9.0	9.0	9.0	12	13	13	13	13	17	17
1250		6.5	6.5	9.0	9.0	13	13	12	13	13	13	17	17	17
1500		6.5	9.0	9.0	13	13	13	12	17	17	17	17	21	21
1750		9.0	9.0	13	13	13	13	17	17	17	17	21	21	21
2000		9.0	13	13	13	13	17	17	17	17	21	21	21	25
2250		9.0	13	13	13	17	17	17	21	21	21	21	25	25
2500		13	13	13	17	17	17	21	21	21	21	25	25	25
3000		13	13	17	17	17	21	21	21	21	25	25	33	33
3500		13	17	17	21	21	21	25	25	25	25	33	33	33
4000		17	17	21	21	21	25	25	33	33	33	33	33	40
4500		17	21	21	21	25	25	33	33	33	33	33	40	40
5000		17	21	25	25	33	33	33	33	33	33	40	40	40
5500		21	25	25	25	33	33	33	33	33	33	40	40	40
6000		21	25	33	33	33	33	33	40	40	40	40	50	50



Table H.10 Exciter ratings for synchronous motors, 60 Hz, 0.8 power factor

		Exciter Ratings, kW												
HP	RPM	1800	1200	900	720	600	514	450	400	360	300	240	200	180
200	3.0	3.0	4.5	4.5	4.5	6.5	6.5	6.5	9.0	9.0	9.0	13	13	13
250	3.0	3.0	4.5	6.5	6.5	6.5	6.5	9.0	9.0	9.0	9.0	13	13	13
300	3.0	3.0	4.5	6.5	6.5	6.5	9.0	9.0	9.0	9.0	13	13	13	13
350	4.5	4.5	4.5	6.5	6.5	9.0	9.0	9.0	9.0	9.0	13	13	13	17
400	4.5	4.5	6.5	6.5	6.5	9.0	9.0	13	13	13	13	13	13	17
450	4.5	4.5	6.5	6.5	9.0	9.0	9.0	13	13	13	13	17	17	17
500	4.5	4.5	6.5	6.5	9.0	9.0	9.0	13	13	13	13	17	17	17
600	6.5	6.5	6.5	9.0	9.0	13	13	13	13	13	17	17	17	21
700	6.5	6.5	9.0	9.0	9.0	13	13	13	13	13	17	17	17	21
800	6.5	6.5	9.0	9.0	13	13	13	17	17	17	17	21	21	21
900	6.5	6.5	9.0	13	13	13	13	17	17	17	17	21	21	25
1000	9.0	9.0	9.0	13	13	13	17	17	17	17	21	21	21	25
1250	9.0	9.0	13	13	13	17	17	21	21	21	21	25	25	33
1500	13	13	13	17	17	17	17	21	21	21	25	25	25	33
1750	13	13	13	17	17	21	21	25	25	25	25	33	33	33
2000	13	17	17	17	21	21	21	25	25	25	33	33	33	40
2250	13	17	21	21	21	25	25	33	33	33	33	33	33	40
2500	17	17	21	21	21	25	25	33	33	33	33	40	40	40
3000	17	21	25	25	25	33	33	33	33	33	40	40	40	50
3500	21	25	25	33	33	33	33	40	40	40	40	50	50	50
4000	21	25	33	33	33	33	40	40	40	40	50	50	50	65
4500	25	33	33	33	33	40	40	50	50	50	50	50	50	65
5000	33	33	40	40	40	40	40	50	50	50	50	65	65	65
5500	33	33	40	40	40	50	50	50	50	50	65	65	65	65
6000	33	40	40	50	50	50	50	65	65	65	65	65	65	85





LIMITAMP CONTROL STANDARD NOMENCLATURE

μSPM	MICROPROCESSOR BASED STARTING & PROTECTION MODULE	GF	GROUND FAULT RELAY	RS	RESISTOR
1AM	AC AMMETER	GFX	AUX. RELAY TO GF	RTD	RESISTANCE TEMPERATURE DETECTOR
2AM	DC AMMETER	GIL	GREEN INDICATING LIGHT	RX	AUX. RELAY TO R
A	ACCELERATING CONTACTOR	GND	GROUND	S	START CONTACTOR
AIL	AMBER INDICATING LIGHT	GRB	GROUND BUS	SC	SURGE CAPACITOR
AM	AMMETER	GS	GROUND SENSOR	SFC	STATIC FIELD CONTACTOR
AMS	AMMETER SWITCH	H1.H2.H3	OUTGOING TERMINALS TO TRANSFORMER	S-GR	SLIP-GUARD RELAY
AT	AUTOTRANSFORMER	HAM	HEATER AMMETER	SH	SHUNT
AX	ACCELERATION TIMING RELAY	ISW	ISOLATING SWITCH	SHAM	SPACE HEATER AMMETER
BFI	BLOWN FUSE INDICATOR	IXR	INCOMPLETE SEQUENCE RELAY	SP HTR	SPACE HEATER
BFIPS	BLOWN FUSE INDICATOR POWER SUPPLY	KX	ANTI-KISS RELAY	SPR	STALL PROTECTIVE RELAY
BFT	BLOWN FUSE TRIP	L.O.	LATE OPENING	SR	STARTING REACTOR
BIL	BLUE INDICATING LIGHT	L1.L2.L3	INCOMING TERMINALS OR AC BUS	SR735	MULTILIN FEEDER RELAY
C	CAPACITOR	LA	LIGHTNING ARRESTOR	SR737	MULTILIN FEEDER RELAY
CC	CLOSING COIL	LIT	LIGHT	SS	SLOW SPEED CONTACTOR
CB	CIRCUIT BREAKER	LOR	LOCKOUT RELAY	SS1	SLOW SPEED SHORTING CONTACTOR
CD	CALIFORNIA DISCONNECT	LSW	LIGHT SWITCH	SSW	SELECTOR SWITCH
CH	CHOKE	LT-IV	LODTRAK 4 MOTOR PROTECTION RELAY	SSX	AUX. RELAY TO SS
CM	FIELD CURRENT CALIBRATION MODULE	LTAR	LODTRAK AUX. RELAY	ST	STAB
CPD	CAPACITOR TRIP DEVICE	M139	MULTILIN MOTOR PROTECTION RELAY	STB	SHORTING TERMINAL BOARD
CPI	CONTROL POWER INTERLOCK	M269	MULTILIN MOTOR MANAGEMENT RELAY	SX	AUX. RELAY TO S
CPIX	AUX. RELAY TO CPI	M269+	MULTILIN MOTOR MANAGEMENT & COMMUNICATION RELAY	T	TRANSFORMER
CPS	CONTACTOR POSITION SWITCH	M	MAIN CONTACTOR	TA	AUX. RELAY TO TIMING MODULE
CR	CONTROL RELAY	MDP200	DIGITAL TIME OVERCURRENT RELAY SYSTEM	TC	TIME CLOSING
CT	CURRENT TRANSFORMER	MOT	MOTOR	TDAD	TIME DELAY AFTER DE-ENERGIZATION
CTB	CURRENT TEST BLOCK	MOV	METAL OXIDE VARISTOR	TDAE	TIME DELAY AFTER DE-ENERGIZATION
CTD	CURRENT TRANSDUCER	MP4A	MULTILIN MOTOR PROTECTION RELAY	TO	TIME OPENING
CTM	CONTACTOR TIMING MODULE	MR	CONTACTOR HOLDING RESISTOR RELAY	T1.T2.T3	OUTGOING TERMINALS TO MOTOR
D	DIODE	MSW	MAIN DISCONNECT SWITCH	TB	TERMINAL BOARD
DCCT	DC CURRENT TRANSFORMER	MTM	MULTILIN METERING & TRANSDUCER MODULE	TH	THERMOSTAT
DMP	DIGITAL MOTOR PROTECTION AND CONTROL SYSTEM	MTM+	MULTILIN METERING & TRANSDUCER MODULE	THY	THYRISTE
DR	DIFFERENTIAL RELAY	MX	AUX. RELAY TO M	TIE	TIE SWITCH
DSTB	DISCONNECT TERMINAL BOARD	N	NEUTRAL CONTACTOR	TM	TIMING MODULE
DSW	DISCONNECT SWITCH	NX	AUX. RELAY TO N	TPI	TEST POWER INTERLOCK
EFR	EXCITER FIELD RELAY	OC	OPERATIONS COUNTER	TPIX	AUX. RELAY TO TPI
EPM	ELECTRONIC POWER METER	OCR	OVERCURRENT RELAY	TPSW	TEST POWER SWITCH
ETM	ELAPSED TIME METER	OL	OVERLOAD RELAY	TR	TIMING RELAY
EXC	EXCITER	OT	OVERTEMPERATURE RELAY	TRP	TRIP RELAY
EXC RHEO	EXCITER THEOSTAT	OTX	AUX. RELAY TO OT	TST	THERMOSTAT ON AT OR SR
F1.F2	SYNC. MOTOR FIELD LEADS	PM	POLARITY MARK	TSW	TEST-NORMAL SELECTOR SWITCH
FC	FIELD CONTACTOR	PB	PUSH BUTTON	UC	UNLATCH COIL OR CONTACT
FCX	AUX. FIELD RELAY	PFC	POWER FACTOR CAPACITOR	UL	UNLATCH RELAY
FCY	AUX. FIELD RELAY	PFM	POWER FACTOR METER	UV	UNDERVOLTAGE RELAY
FDRS	FIELD DISCHARGE RESISTOR	PG	PLUG	UVTR	UNDERVOLTAGE TIMING RELAY
FGRS	FIELD GROUND RESISTOR	PHA.PHB.PHC	INCOMING LINE TERMINALS	VCR	VOLTAGE CHECK RELAY
FLD	SYNC. MOTOR FIELD	PHF	OPEN PHASE & PHASE SEQUENCE RELAY	VDN	VOLTAGE DIVIDER NETWORK
FLR	FIELD LOSS RELAY	PLR	POWER LOSS RELAY	VFC	ELECTRONIC VARIABLE FIELD CONTACTOR
FLTR	FILTER	PRO	CT PROTECTOR (THYRISTE)	VFSM	VARIABLE FIELD SUPPLY MODULE
FRP	FIELD RECTIFIER PANEL	PST	PHASE SHIFTING TRANSFORMER	VM	VOLTMETER
FS	FAST SPEED CONTACTOR	PT	POTENTIAL TRANSFORMER	VMS	VOLTMETER SWITCH
FS1	FAST SPEED SHORTING CONTACTOR	PTB	POTENTIAL TEST BLOCK	VRM	VARMETER
FSX	AUX. RELAY TO FS	R	RUN OR REVERSE CONTACTOR	VRTD	VAR TRANSDUCER
FSW	FEEDER SWITCH	RC	RECTIFIER & VOLTAGE DROPPING CAPACITOR	VT	VARIABLE AUTOTRANSFORMER
FTRS	FIXED TAP RESISTOR	REC	RECTIFIER	VTD	VOLTAGE TRANSDUCER
FU	FUSE	RECP	RECEPTACLE	WHDM	WATTHOUR DEMAND METER
GCT	GROUND CURRENT TRANSFORMER	REV	REVERSE CONTACTOR	WHM	WATTHOUR METER
		RIL	RED INDICATING LIGHT	WM	WATTMETER
		RM	RECTIFIER CONTACTOR	WTD	WATTS TRANSDUCER

This diagram shows starter with the isolating switch in the disconnect position and the test power interlock in the test position.

To test: Handle must be in the disconnect (OFF) position, and test-normal selector switch (located in the low voltage compartment) must be in the TEST position. Purchaser is to connect his test power to the proper terminals and note that the control circuit is not grounded when disconnects are open. Be sure to turn the test-normal switch to NORMAL before moving the disconnect handle to the ON position.

CPI — Opens only when CPI release on isolating switch handle is pushed in. Can not be opened when main line contactor is closed.

△ — Start and stop push buttons are wired through terminal at "TB" in order that remote START-STOP buttons can be readily connected into the circuit when required.

□ — At a terminal on "TB", a loop in the CT secondary circuit wire permits insertion of a hook on ammeter for measuring line current.

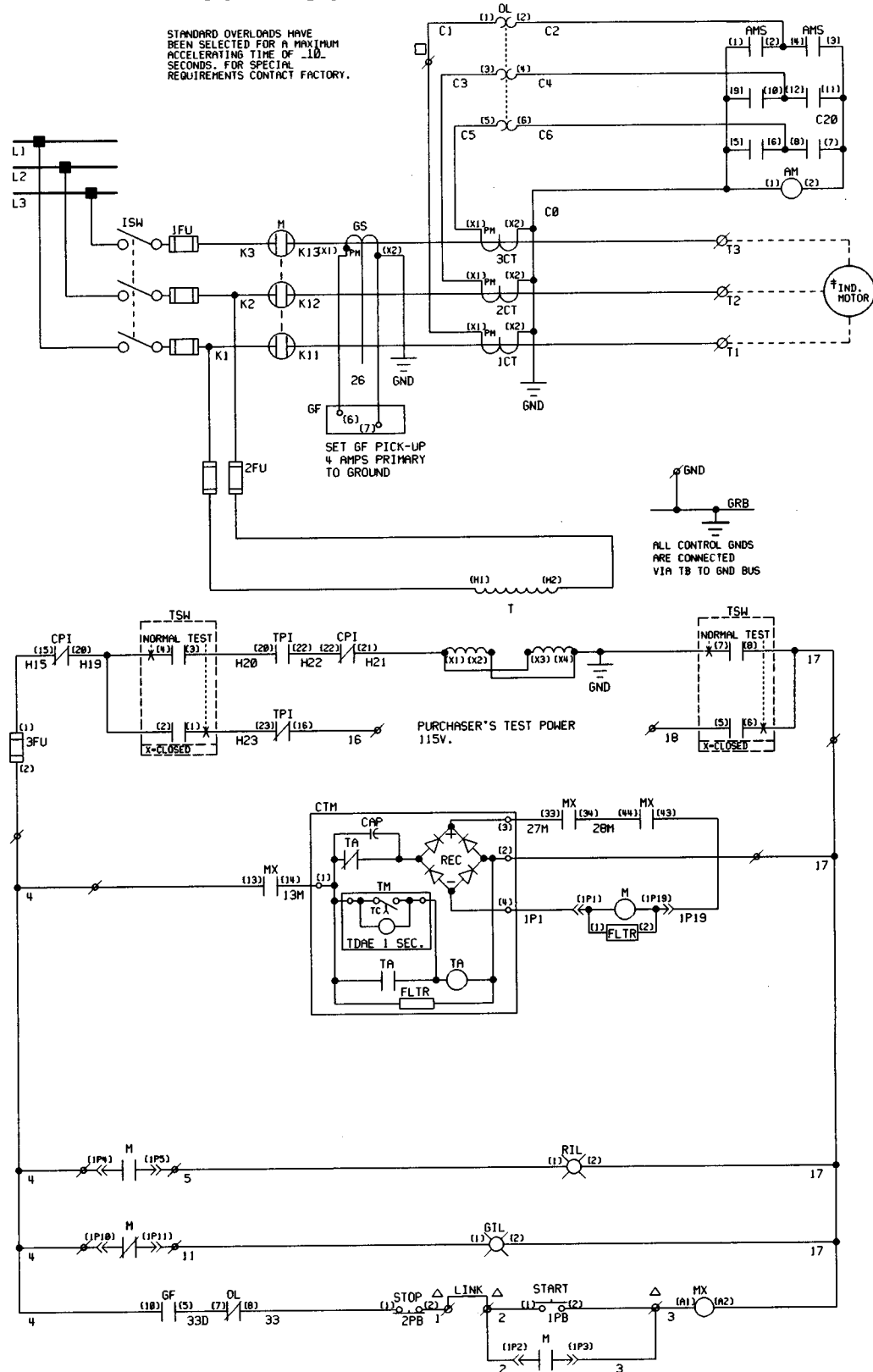
— Device furnished by others — mounted remote.

— Terminal board point.



FVNR INDUCTION

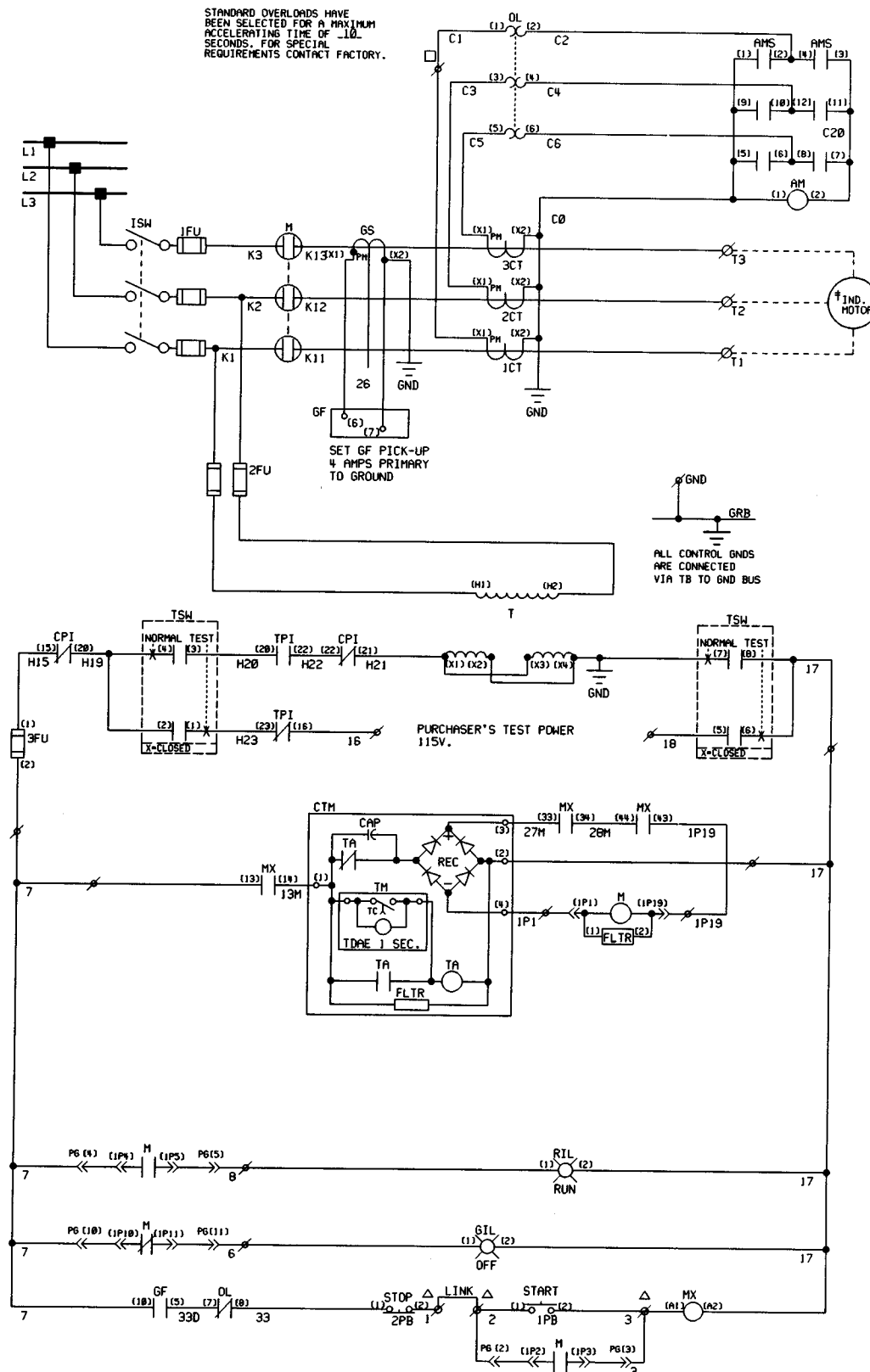
CR194 400-ampere Vacuum Stationary (Two-high)





FVNR INDUCTION

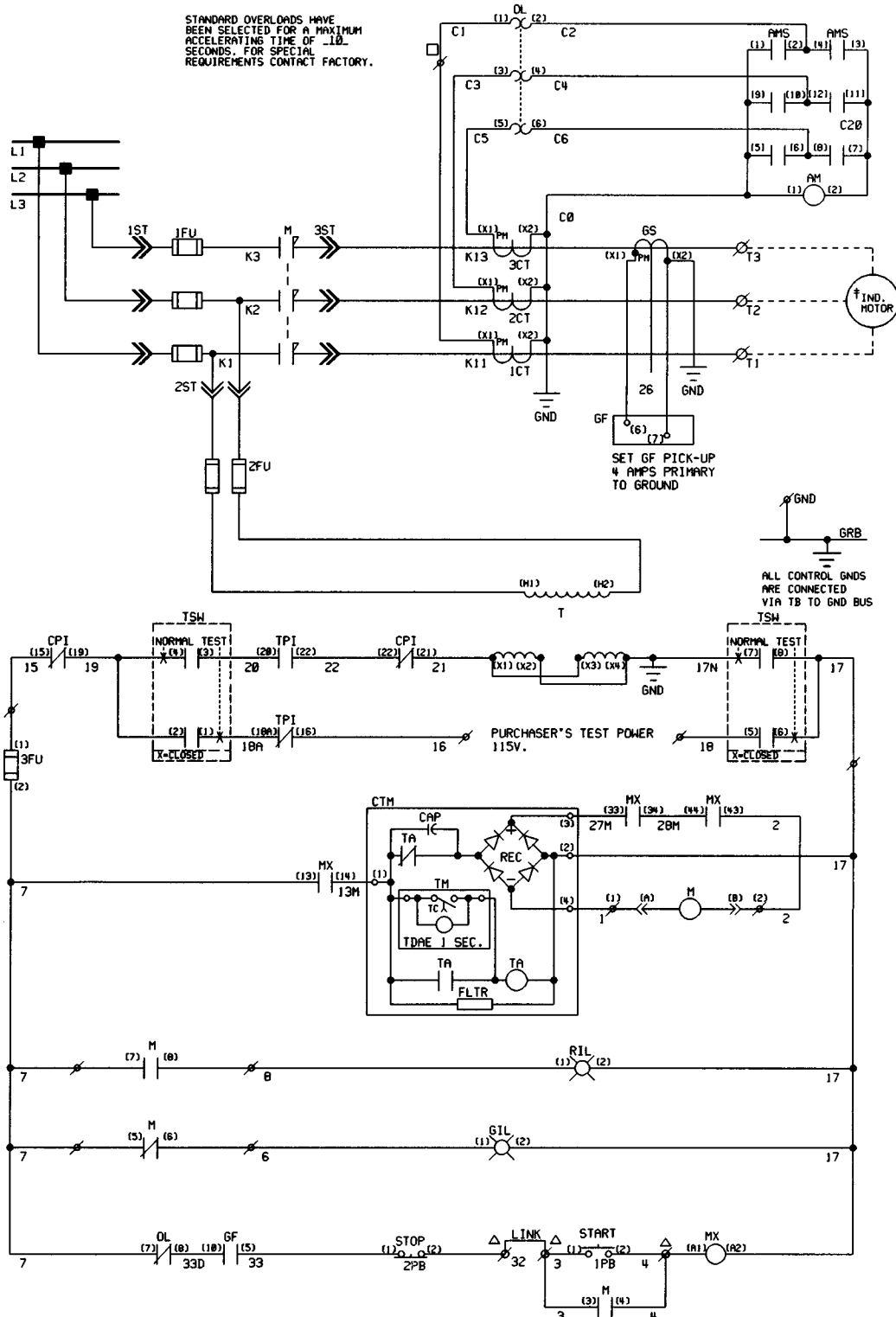
CR194 400-ampere Vacuum Stationary (One-high)





FVNR INDUCTION

CR7160 400-ampere Air-break (Two-high)





RVAT INDUCTION

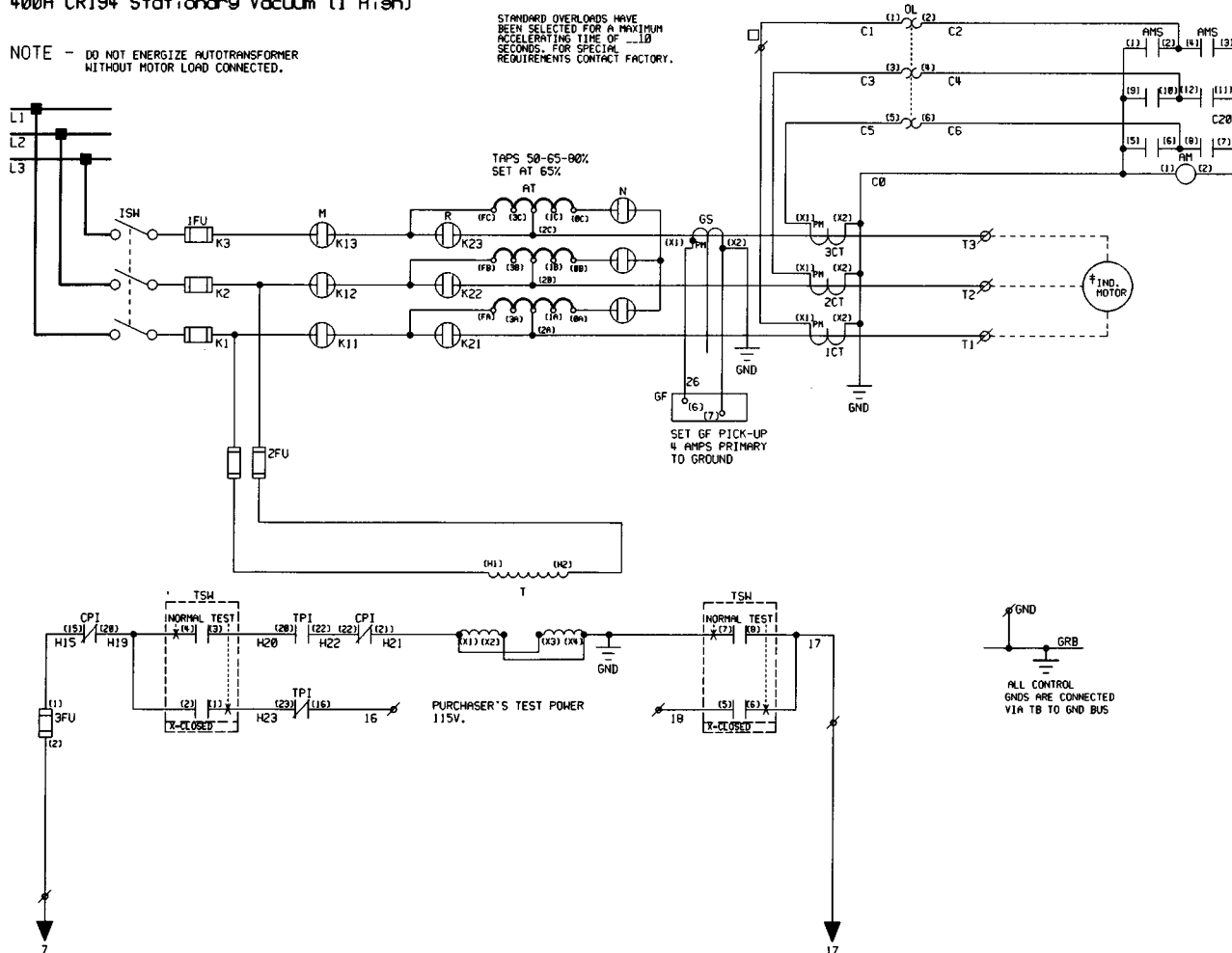
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RVAT INDUCTION

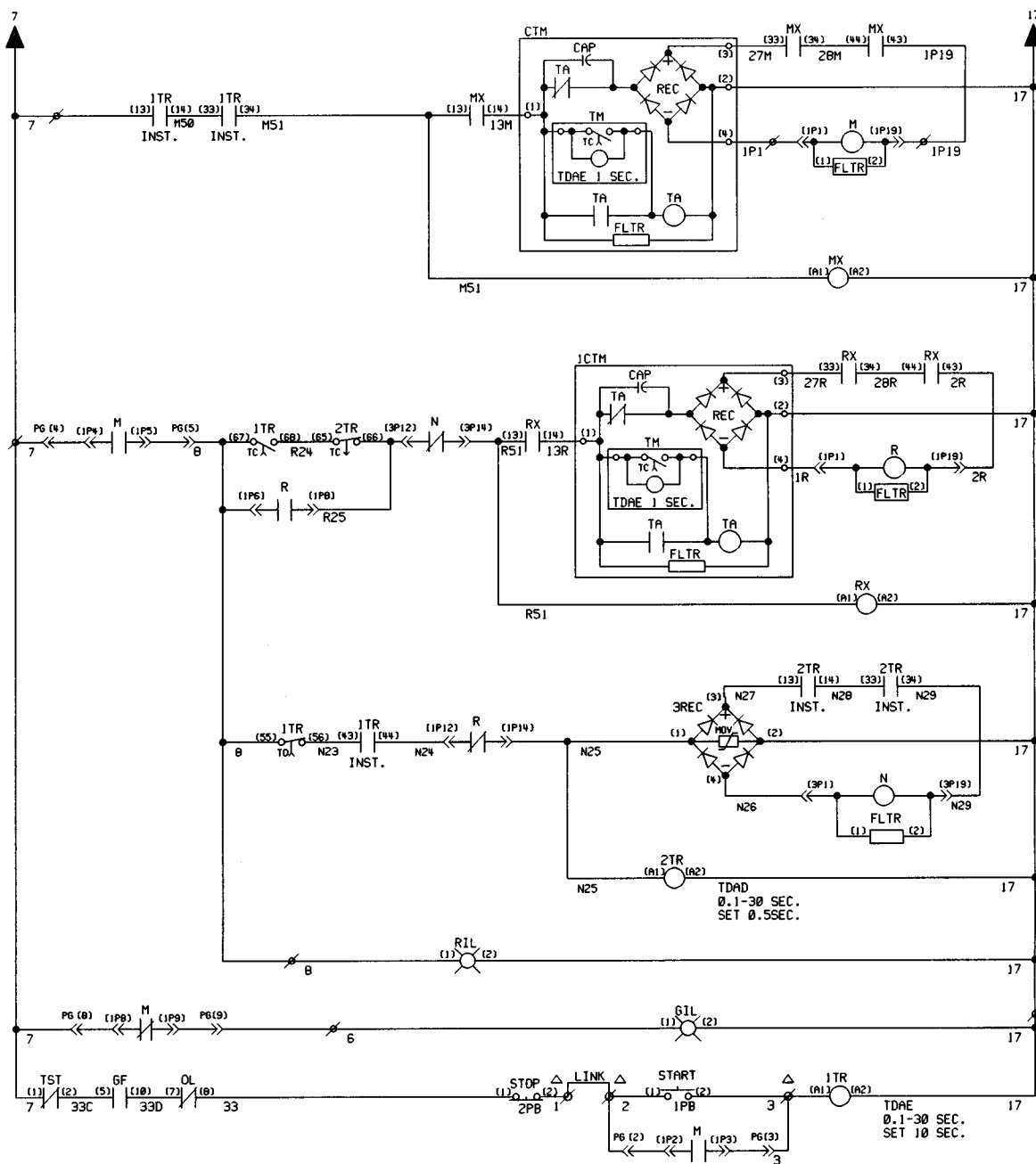
400A CR194 Stationary Vacuum (1 High)

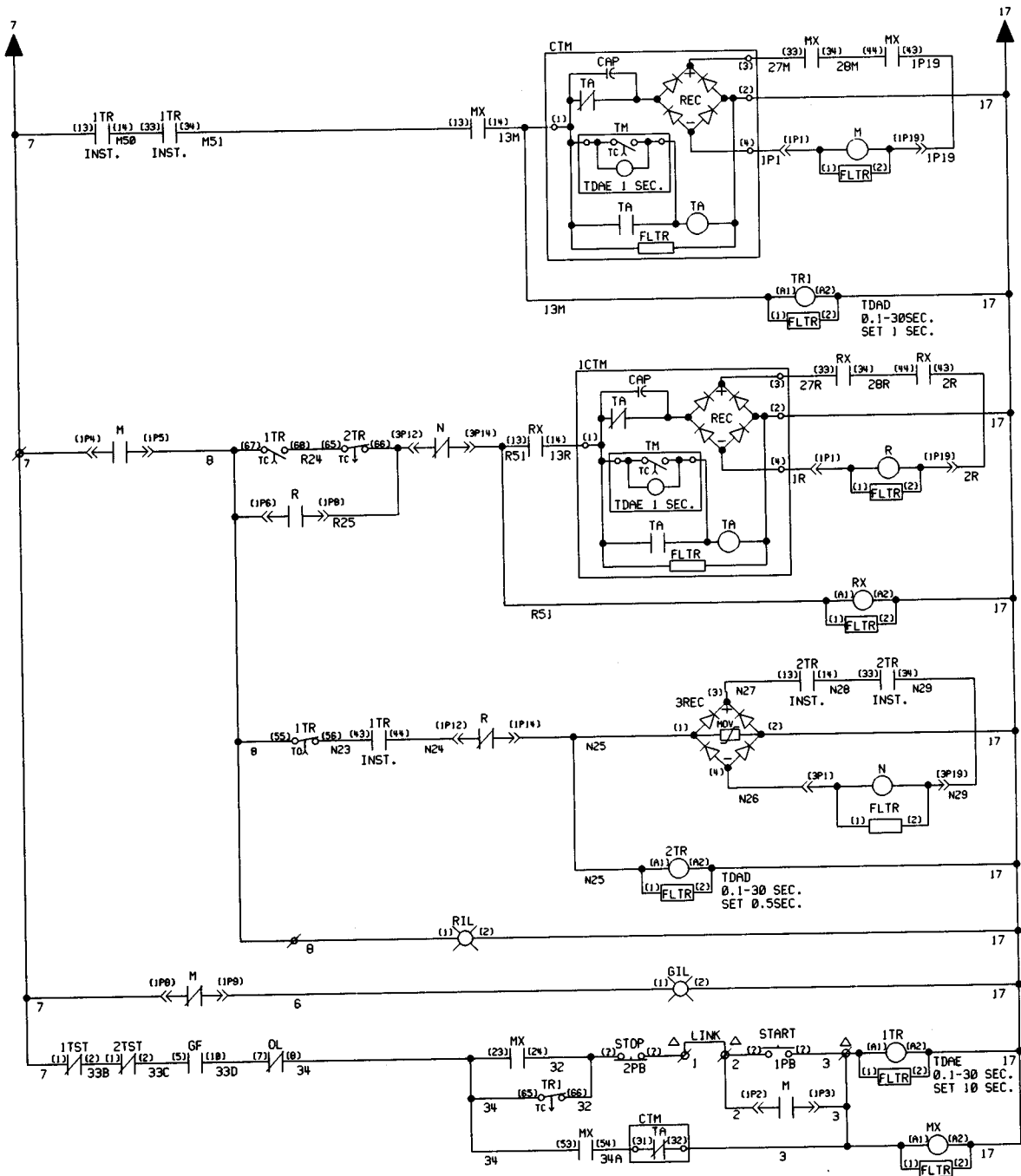
NOTE - DO NOT ENERGIZE AUTOTRANSFORMER
WITHOUT MOTOR LOAD CONNECTED.

STANDARD OVERLOADS HAVE
BEEN SELECTED FOR A MAXIMUM
ACCELERATING TIME OF 10
SECONDS. FOR SPECIAL
REQUIREMENTS CONTACT FACTORY.



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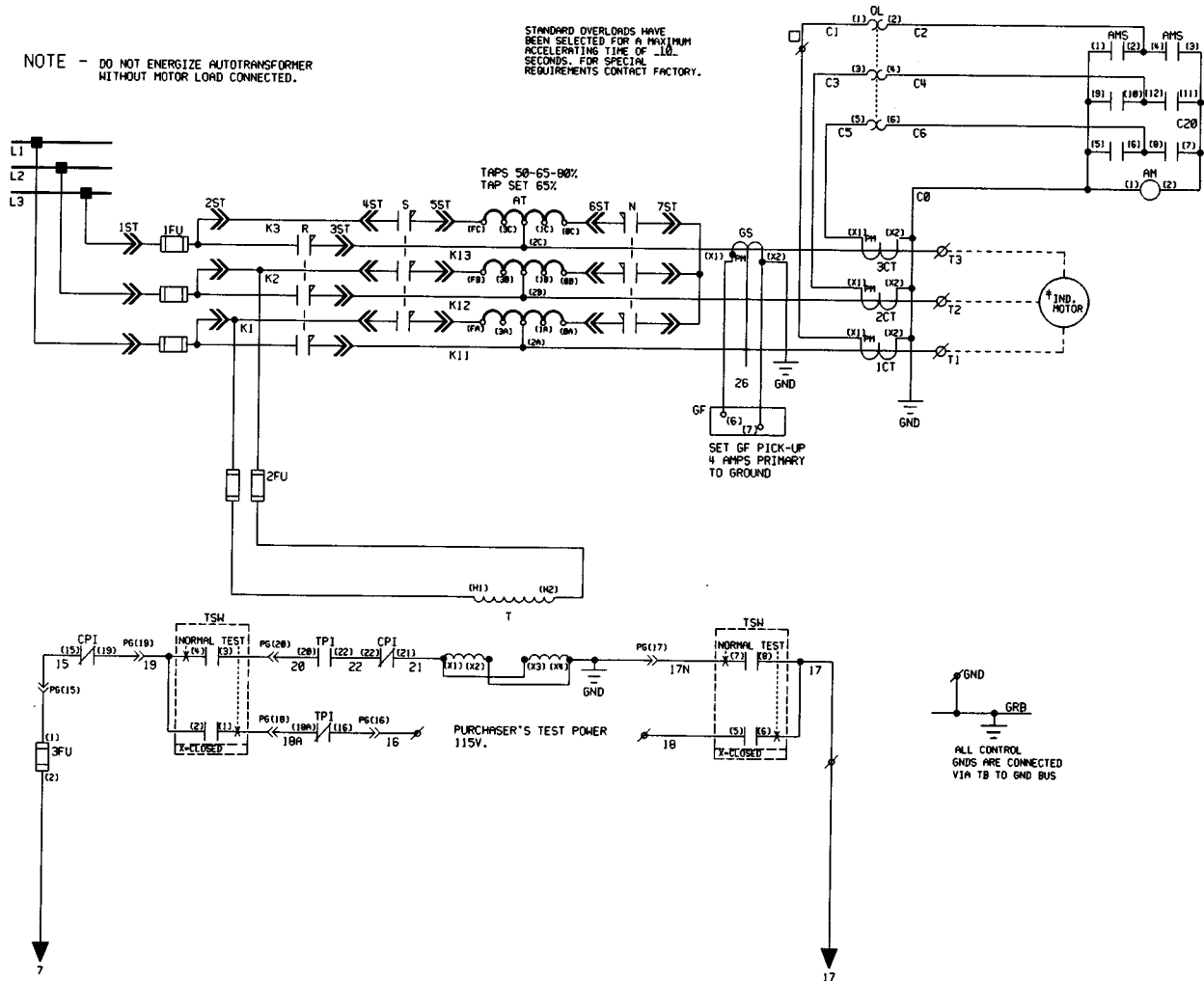


RVAT INDUCTION

CR7160 400- & 700-ampere Air-break (One-high)

NOTE - DO NOT ENERGIZE AUTOTRANSFORMER
WITHOUT MOTOR LOAD CONNECTED.

STANDARD OVERLOADS HAVE
BEEN SELECTED FOR A MAXIMUM
ACCELERATING TIME OF .10
SECONDS. FOR SPECIAL
REQUIREMENTS CONTACT FACTORY.





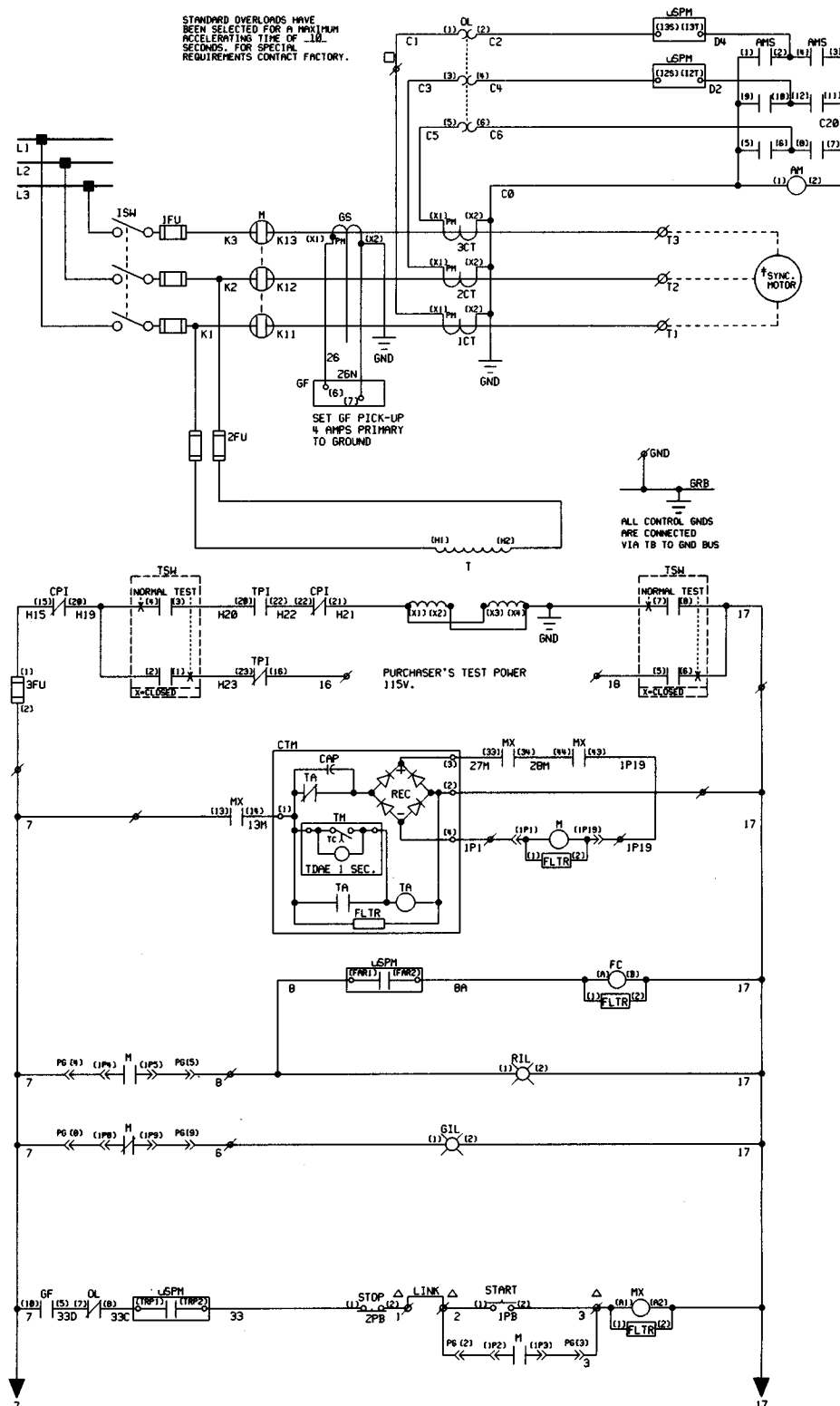
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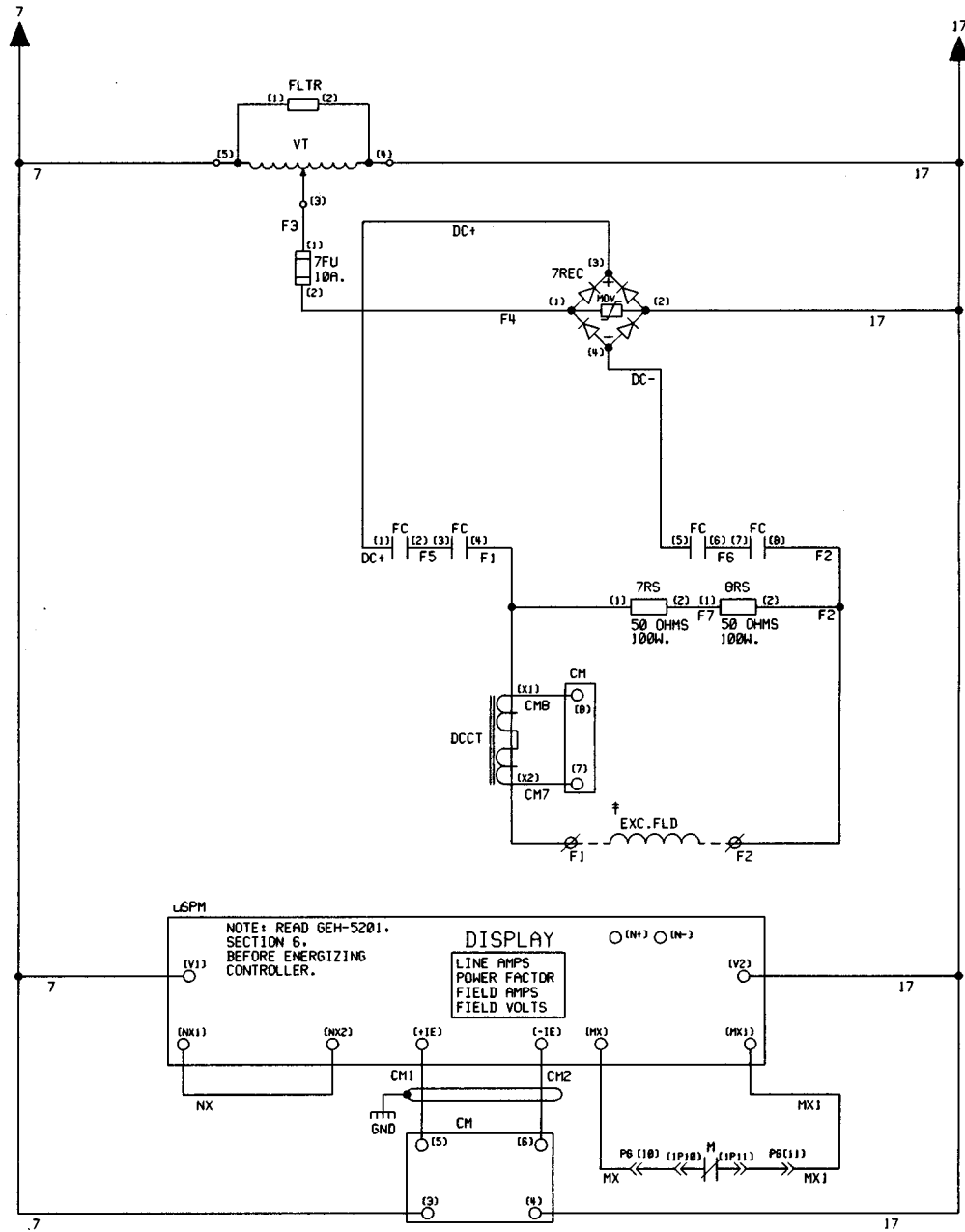


FVNR BRUSHLESS SYNCHRONOUS

CR194 400-ampere Vacuum Stationary (One-high)



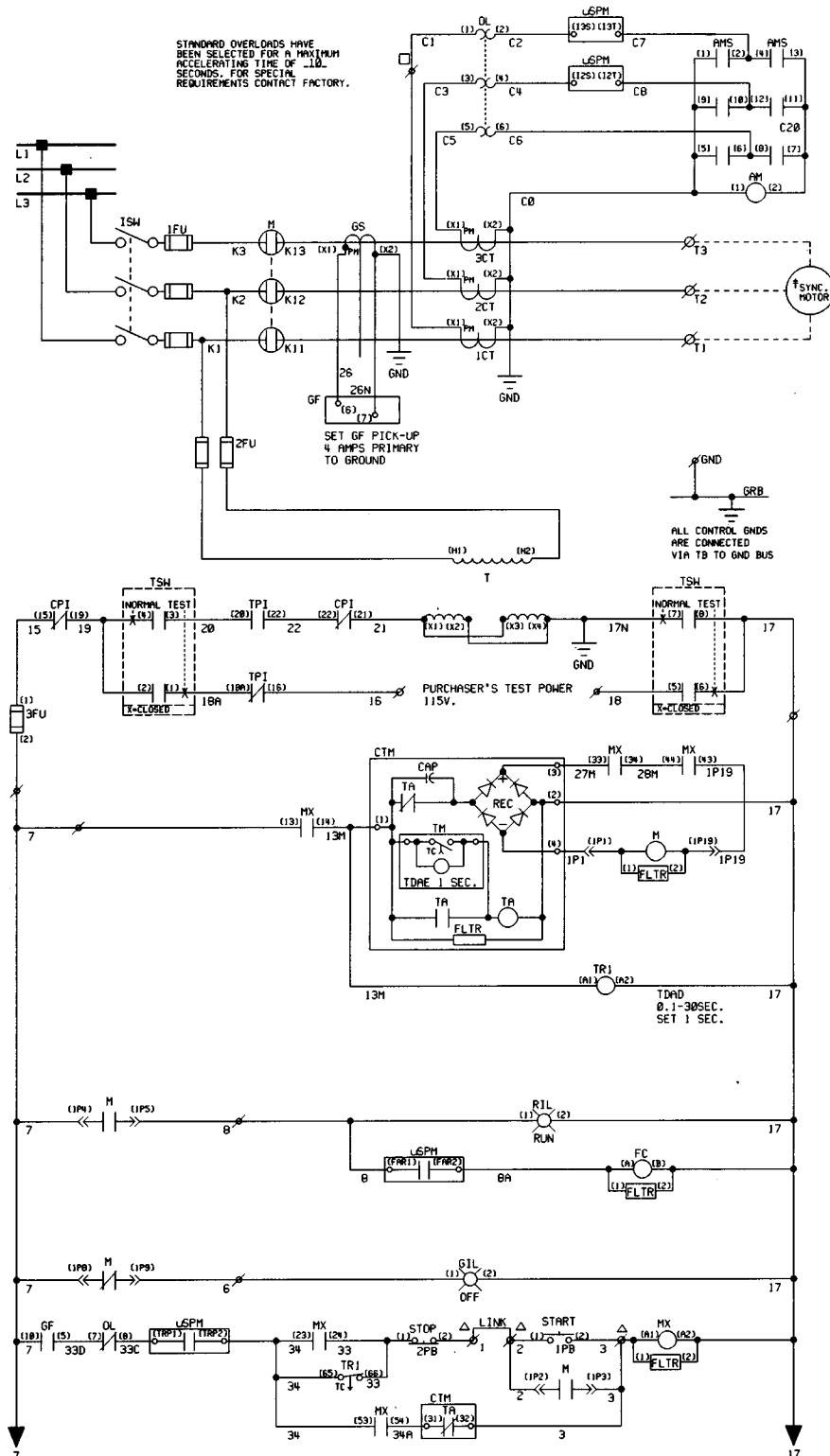
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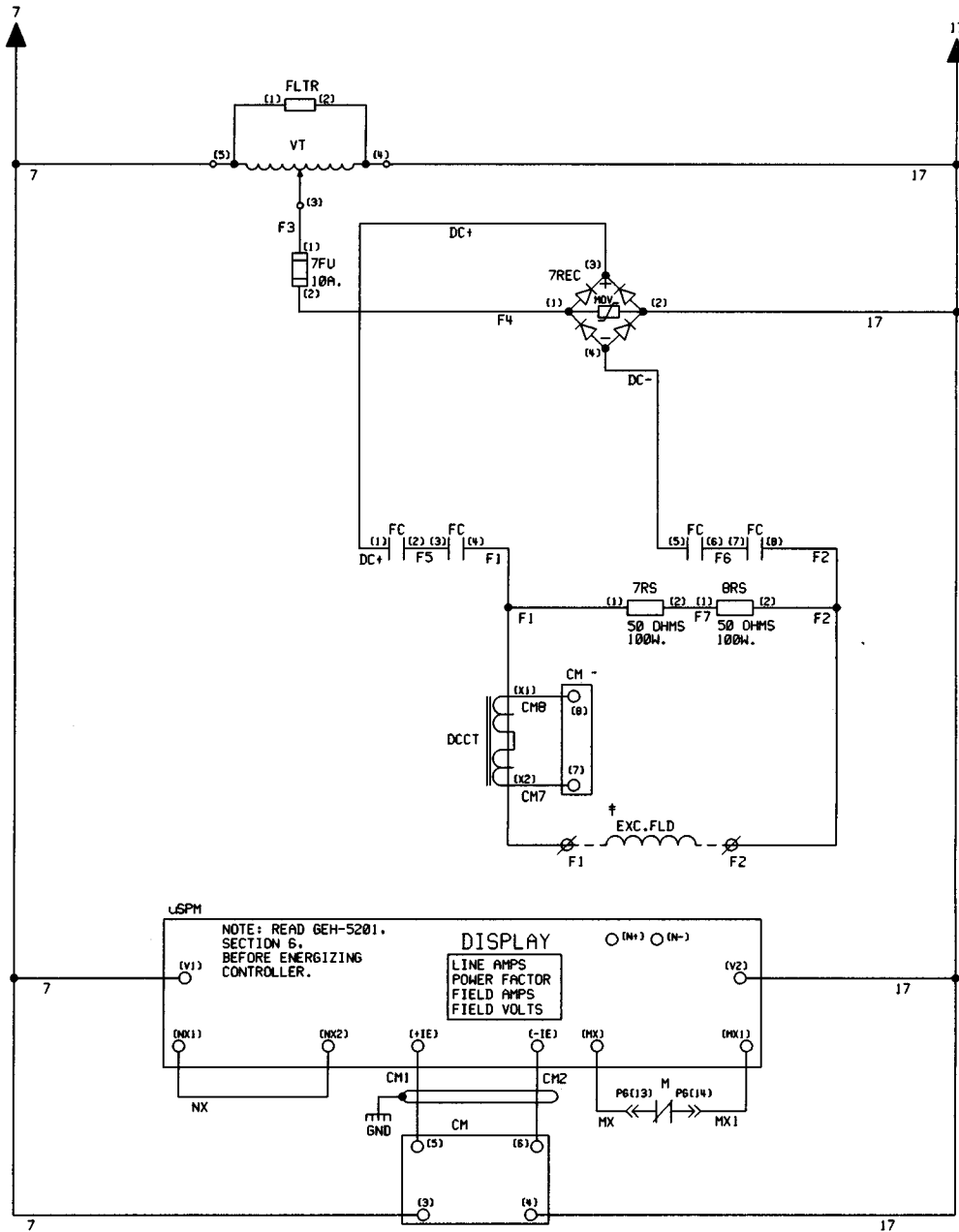
FVNR BRUSHLESS SYNCHRONOUS

CR194 800-ampere Vacuum Stationary (One-high)



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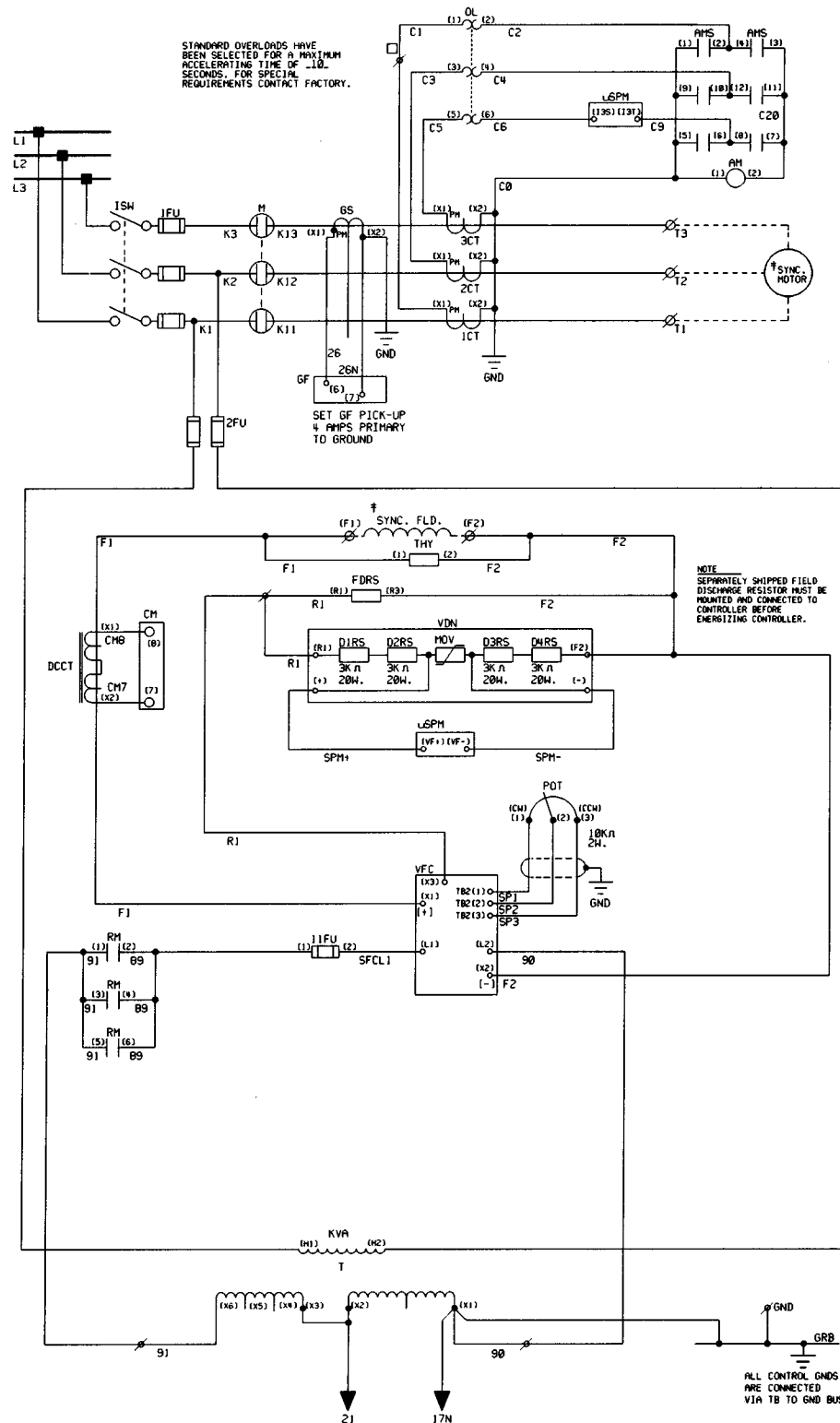




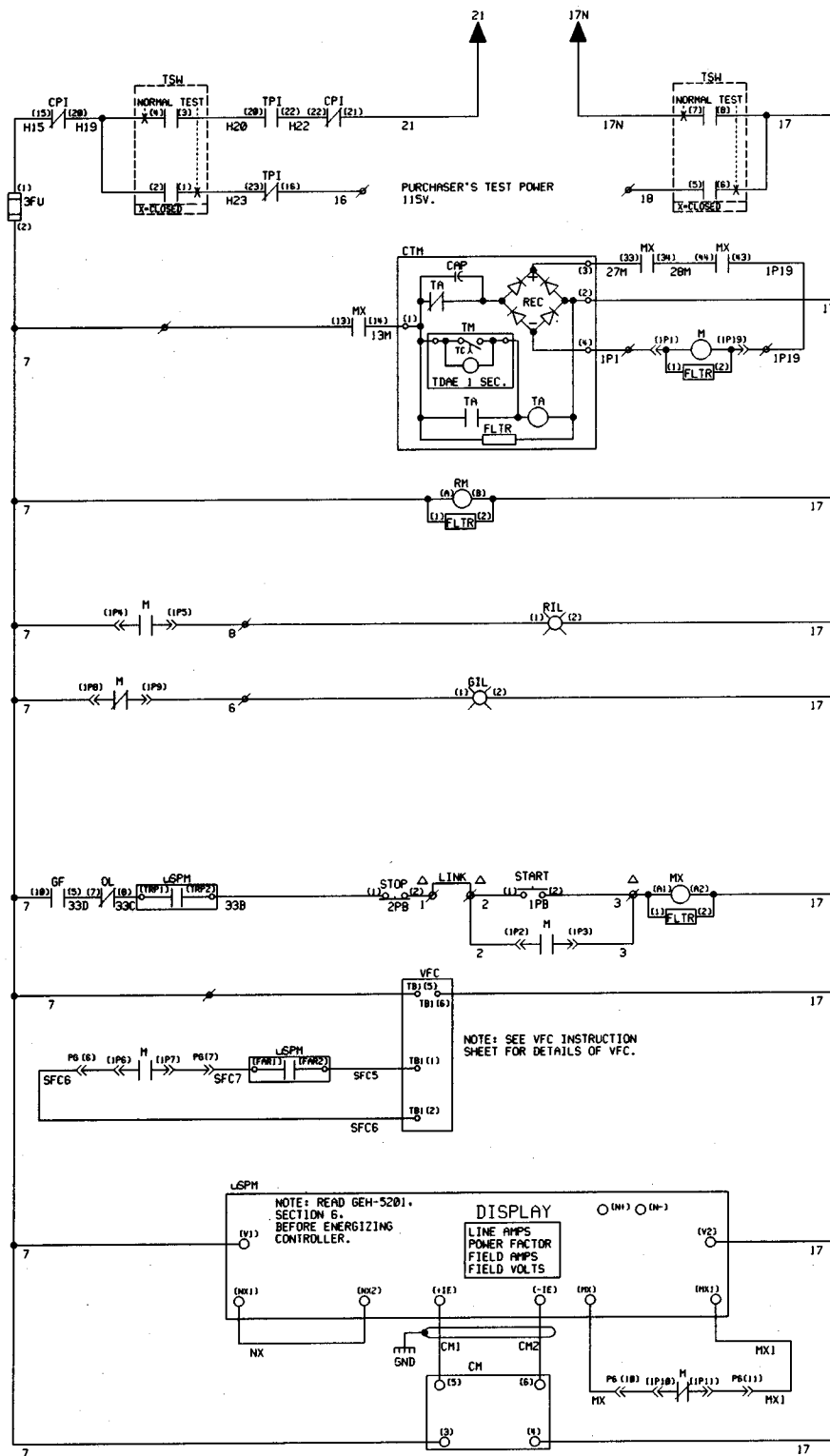


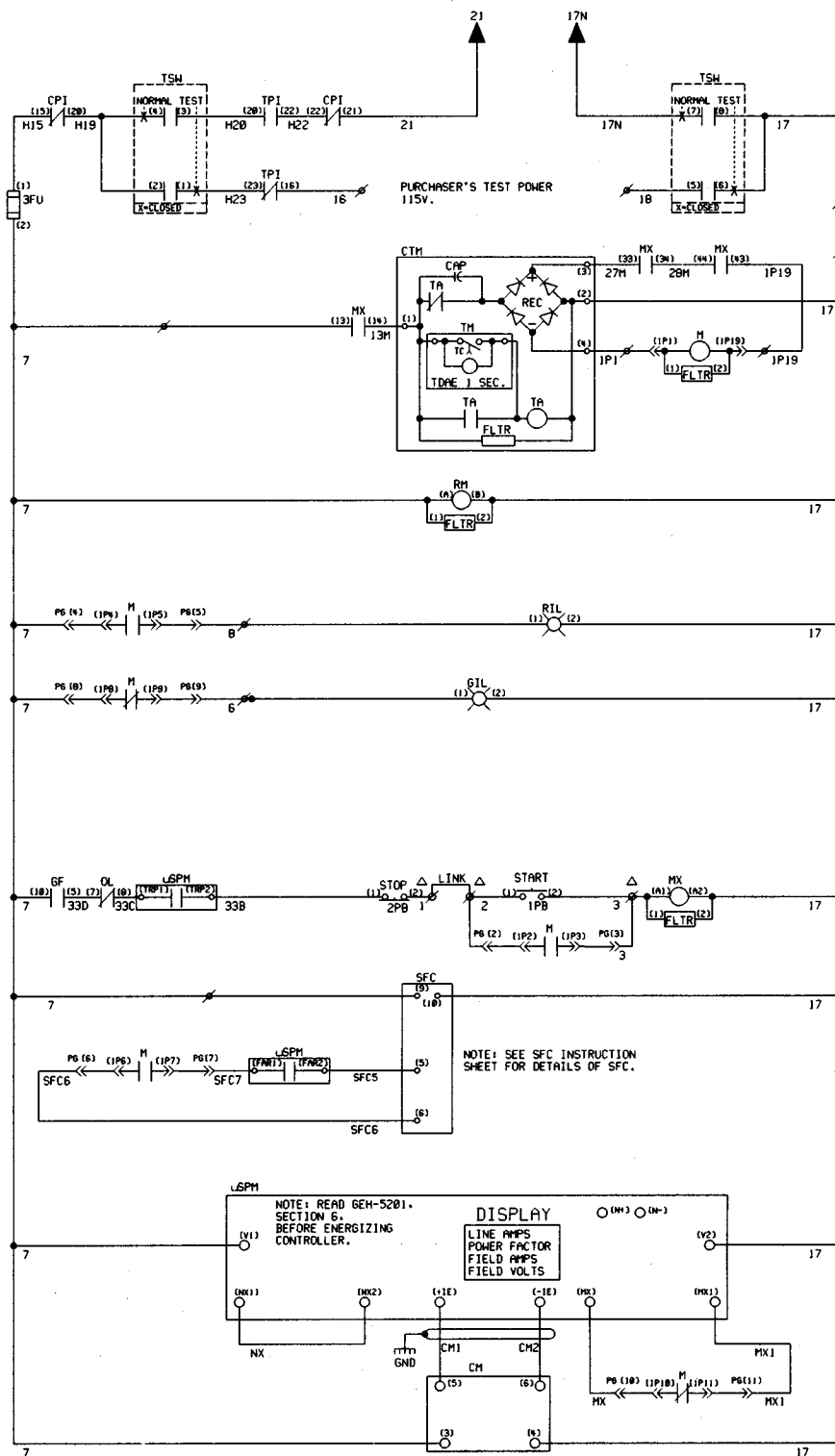
FVNR BRUSH-TYPE SYNCHRONOUS (With Variable Field Supply Contactor)

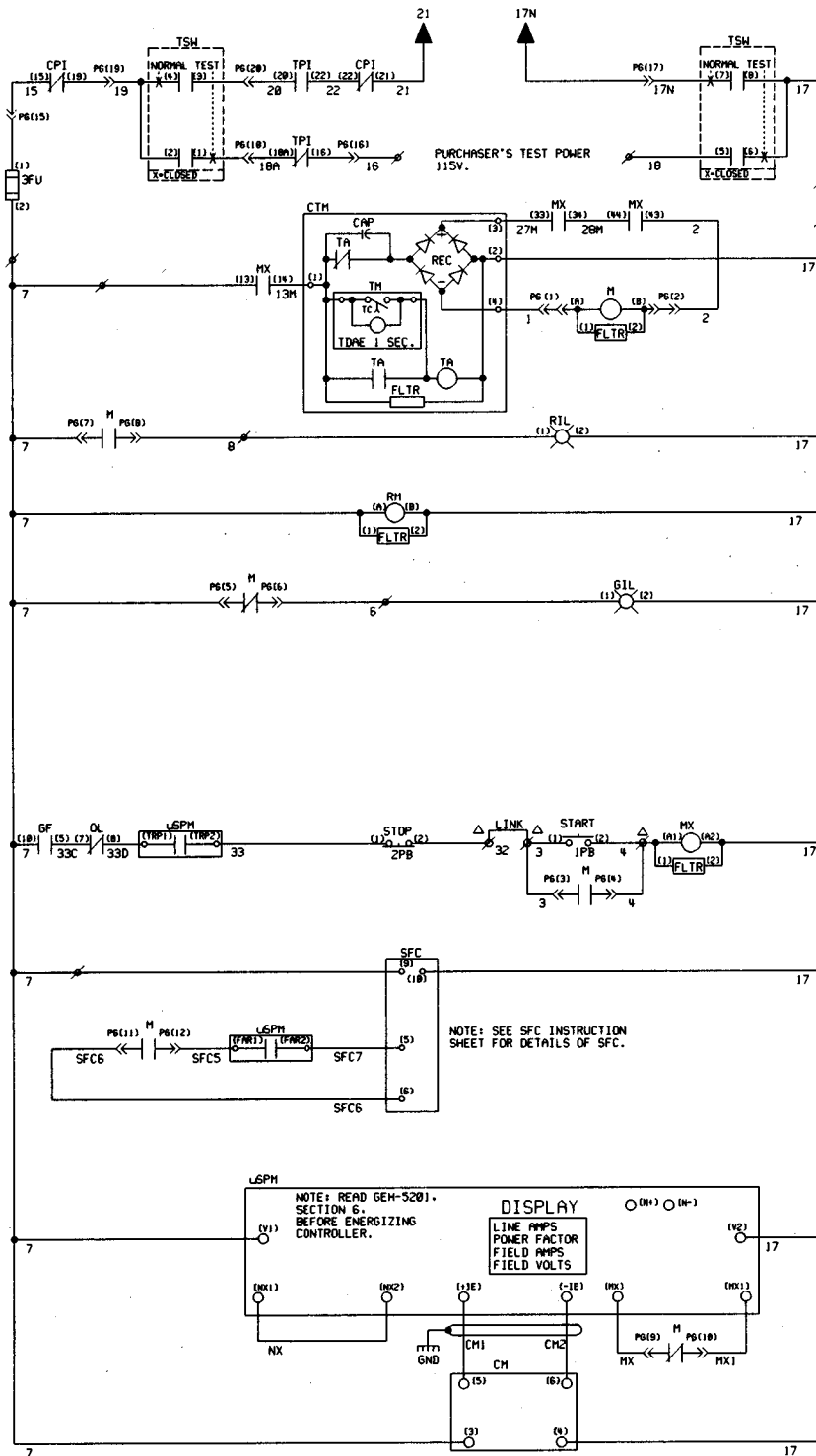
CR194 400-ampere Vacuum Stationary (One-high)



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CONTROLLERS-CR194 VACUUM STATIONARY & DRAWOUT CONTACTORS, 2400 - 7200 VOLTS

GENERAL

These specifications cover NEMA Class E2 high-voltage control for ____ volts, ____ phase, ____ Hertz as follows:

Controller #1:

(Full voltage)	(Non reversing)	controller for	(Squirrel-cage induction)
(Reduced voltage)	(Reversing)		(Wound-rotor induction)
			(Brush-type synchronous)
			(Brushless synchronous)

motor rated at ____ horsepower.

Controller #2, etc. (as shown above)

ALL CONTROLLERS

Controller(s) shall be fused type employing current-limiting and power fuses that give the controller an interrupting rating of:

- 200 mVA, 3 phase symmetrical at 2400 Volts, 50/60 Hz
- 350 mVA, 3 phase symmetrical at 4200 Volts, 50/60 Hz
- 400 mVA, 3 phase symmetrical at 4800 Volts, 50/60 Hz
- 600 mVA, 3 phase symmetrical at 7200 Volts, 50/60 Hz

CONTACTORS

Starter(s) shall employ magnetically held vacuum contactor(s) rated at:

for welded enclosure:

- 400 amperes at 7200 volts maximum, interrupting rating of 75 mVA, 3 phase symm.
- 800 amperes at 5000 volts maximum, interrupting rating of 75 mVA, 3 phase symm.

for bolted enclosure:

- 400 amperes at 5000 volts maximum, interrupting rating of 50 mVA, 3 phase symm. (2-high only)

Contactor(s) shall be stationary (drawout for 400 amp contactor only) and the coil shall be removable without removing the contactor from the enclosure. The vacuum interrupter wear checks shall not require removal of the contactor.

Controller(s) shall be in a:

for welded enclosure:

- One-high line-up of NEMA ____ enclosure(s) equipped with 3-ph (1000) (2000) amp horizontal AC bus

- One-high individual NEMA ____ enclosure(s) equipped with provisions for terminating incoming cable

for bolted enclosure:

- Two-high line-up of NEMA ____ enclosure(s) equipped with (1000) (2000) amp horizontal AC power bus

The power bus shall be braced for 80 kA RMS asymmetrical or 50 kA RMS symmetrical.

For safety to personnel, enclosure(s) shall be compartmented into low-voltage control compartment with separate door, high-voltage compartment with separate interlocked door, AC bus compartment with protective barriers and cable entrance compartment.



The controller shall be isolated by a quick-make quick-break switch operated by an externally mounted operating handle. The isolating device shall disconnect the secondary of the control power transformer before opening the main circuit contacts.

Mechanical interlocks shall be provided to prevent:

1. Closing the isolation switch with the high-voltage door open.
2. Operation of the isolation switch while under load.
3. Opening of the high-voltage door when isolation switch is on.
4. Operation of the contactor when the isolation switch is in an intermediate position.

NOTE: For overload protection, one three-pole ambient-compensated thermal-overload relay, manually reset, shall be included.

Controllers rated 400 and 800 amperes shall be rated 60 kV Basic Impulse Level (BIL).

OPTIONS:

Each controller shall contain protection against single-phasing due to a blown fuse and shall have blown fuse indication.

(Solid-state relay protection)

(Latched contactors)

Control for Wound-rotor Induction Motors

Secondary control shall be fully magnetic. It shall provide automatic acceleration through ____ starting steps with uniform torque peaks using a NEMA Class ____ resistor.

The control shall provide for continuous speed regulation with ____ points of speed reduction with a maximum reduction of ____ % from full-load speed at ____ % full load torque.

Control for Synchronous Motors

DC field control for synchronous motors shall consist of one General Electric CR192 starting and protection module equipped with digital displays for power factor, field current and line current, one field starting and discharge resistor and one electronic field contactor. Operation must be fully automatic.

Static field supplies shall be:

- (tapped transformer static field contactor [SFC])
- (adjustable silicon controlled rectified variable field contactor [SCR type VFC])
- (adjustable VFC with power factor regulation)
- (adjustable VFC with field current regulation)

Additional Functions

Control power at 120 volts shall be provided from a control power transformer in each controller. The transformer shall be protected by current-limiting fuses.

Controller(s) shall provide instantaneous undervoltage protection when momentary contact push button is used, undervoltage release when maintained contact push button is used.

(Push button) is to be (mounted on door)
(Switch) (remotely located)

Finish

Finish shall be:

- (ANSI-61 light gray over rust-resistant phosphate undercoat for indoor use.)
- (ANSI-61 light gray over one or more rust-resistant phosphate undercoats for outdoor use.)

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CONTROLLERS - CR7160 VACUUM OR AIR-BREAK DRAW OUT, 2400 - 7200 Volts

GENERAL

These specifications cover NEMA Class E2 high-voltage control for ____ volts,
____ phase, ____ Hertz motors as follows:

Controller #1:

(Full voltage) (Non reversing) controller for (Square wave induction)
(Reduced voltage) (Reversing) (Wound rotor induction)
(Brush-type synchronous)
(Brushless synchronous)

motor rated at ____ horsepower.

Controller #2, etc. (as shown above)

ALL CONTROLLERS

Controller(s) shall be fused type employing current-limiting power fuses that give the controller an interrupting rating of:

- 200 mVA, 3-phase symmetrical at 2400 volts, 50/60 Hz
- 350 mVA, 3-phase symmetrical at 4200 volts, 50/60 Hz
- 400 mVA, 3-phase symmetrical at 4800 volts, 50/60 Hz
- 600 mVA, 3-phase symmetrical at 7200 volts, 50/60 Hz

Starter(s) shall employ (vacuum) (magnetic air-break) line contactor(s) rated 400 amperes, 5000 volts and have an interrupting capacity of 50 mVA, 3-phase, symmetrical.

Starter(s) shall employ magnetic air-break line contactor(s) rated 700 amperes, 5000 volts and have an interrupting capacity of 80 mVA, 3-phase symmetrical.

Controller(s) shall be in a:

- one-high line-up of NEMA ____ enclosures with 3-phase (1000 amp) (2000 amp) AC power bus.
- free-standing one-high individual NEMA ____ enclosure(s) with provision for terminating incoming cable.
- two-high construction with NEMA ____ enclosure*, and with 3-phase (1000 amp) (2000 amp) AC power bus.
- three-high construction with NEMA ____ enclosure*, and with 3-phase (1000 amp) (2000 amp) AC power bus.

For safety to personnel, enclosure(s) shall be compartmented into low-voltage control compartment with separate door, high-voltage compartment with separate interlocked door, AC bus compartment with protective barriers and cable entrance compartment.

Line contactors shall be draw out type.

The controller shall be isolated by externally operated drawout stabs with shutter mechanism. The isolating device shall also open the secondary of the control power transformer. Interlocks shall be provided to prevent (1) inadvertent operation of the isolation mechanism underload, (2) opening the high-voltage compartment door without isolating the starter, and (3) closing the isolation switch with door open.

NOTE: For overload protection, one three-pole ambient-compensated thermal overload relay, hand-reset, shall be included.



OPTIONS

(Solid-state relay protection)

(Anti-single-phase trip bar)

(Mechanical latching)

Control for Wound-rotor Induction Motors

Secondary control shall be fully magnetic. It shall provide automatic acceleration through ____ starting steps with uniform torque peaks using a NEMA Class ____ resistor.

The control shall provide for continuous speed regulation with ____ point of speed reduction with a maximum reduction of ____ percent from full-load speed at ____ % full-load torque.

Control for Synchronous Motors

DC field control for synchronous motors shall consist of one General Electric CR192 starting and protection module equipped with digital displays for power factor, field current and line current, one field starting and discharge resistor and one magnetic field contactor. Operation must be fully automatic.

Static field supplies shall be:

(tapped transformer SFC - Static Field Contactor)

(adjustable SCR type VFC - Variable Field Contactor)

(adjustable SCR type VFC with power-factor regulation)

(adjustable SCR type VFC with field current regulation)

Additional functions

Control power at 120 volts shall be provided from a control-power transformer in each controller. Transformer shall be protected by current-limiting fuses.

Controller(s) shall provide instantaneous undervoltage protection when momentary-contact push button is used, undervoltage release when maintained-contact switch is used.

(Push button) is to be (mounted on door).

(Switch) (remotely located).

Finish

Finish shall be:

(ANSI-61 light gray over rust-resistant phosphate undercoat for indoor use.)

(ANSI-61 light gray over one or more rust-resistant phosphate undercoats for outdoor use.)



STARTERS - CR194 VACUUM

ALL STARTERS

Enclosure NEMA Type 1 general purpose, ventilated

Connections

- Incoming Line . . Entrance top or bottom. Cables separated by barrier from both low- and high-voltage compartments.
- Motor Cable . . . Entrance top or bottom. Cables separated by barrier from both low- and high-voltage compartments.

SQUIRREL-CAGE-MOTOR STARTERS

Full-Voltage Non-Reversing (FVNR)

High-voltage

- compartment . . 1-Set of bolt-in current-limiting fuses and supports
- 1-Externally operated disconnect switch
- 1-Three-pole vacuum contactor
- 1-Set of mechanical interlocks to prevent opening the disconnect when the contactor is on, to prevent opening the door when the disconnect is on, to prevent closing the contactor when the disconnect is in an intermediate position, and to prevent closing of the disconnect when the high-voltage door is open
- 1-Fused primary control power transformer (CPT)
- 3-Current transformers
- 3-Terminals for motor cable connections

Low-voltage

- compartment . . 1-Three-pole, ambient-compensated thermal overload relay, hand-reset
- 1-NORMAL-TEST selector switch
- 1-Control-circuit fuse

- On door 1-START-STOP push button, oil-tight, flush-mounted

Full-Voltage Reversing (FVR)

Same as for full-voltage non-reversing with addition of following:

Auxiliary

- enclosure 2-Three-pole vacuum contactors for reversing

- On door 1-FORWARD-REVERSE-STOP push button, oil-tight, flush-mounted (replacing START-STOP push button)

Reduced-Voltage Non-Reversing (RVNR) (Primary Reactor)

Same as for full-voltage non-reversing with addition of following:

- 1-Three-pole vacuum contactor used as a RUN contactor

Auxiliary enclosure

- (1-high) 1-Reduced-voltage starting reactor with taps for 50-, 65- and 80-percent line voltage

Low voltage

- compartment . . 1-Definite time transfer relay

Reduced-Voltage Non-Reversing (RVNR)

(Autotransformer closed transition)

Same as for full-voltage non-reversing with addition of following:

- 1-Three-pole vacuum contactor used as a RUN contactor

Auxiliary enclosure

- (1-high) 2-Three-pole vacuum contactor - neutral, and 80-percent line voltage

Low-voltage

- compartment . . 1-Definite time transfer relay

WOUND-ROTOR-MOTOR STARTERS

Non-Reversing

Same as for squirrel-cage FVNR with addition of following:

Secondary

- enclosure 1-Set of intermediate accelerating contactors
- 1-Final accelerating contactor
- 1-Set of definite time accelerating relays

Resistor

- enclosure 1-Set of starting-duty resistors, NEMA Class 135

Reversing

Same as for non-reversing with addition of following:

High-voltage

- compartment . . 1-Three-pole vacuum contactor used for reversing

- On door 1-FORWARD-REVERSE-STOP push button, oil-tight, flush-mounted (replacing START-STOP push button)



BRUSH-TYPE SYNCHRONOUS-MOTOR STARTERS

Full-Voltage Non-Reversing (FVNR)

Same as for squirrel-cage FVNR with addition of following:

Low voltage

compartment . . 1-Field application and discharge
contactor

On door 1-CR192 μ SPM solid-state synchronizing
device for precision-angle field appli-
cation, load-angle field removal and
squirrel-cage protection with built-in
digital power factor and line ammeter

1-Line amps display - digital readout
(part of CR192 module)

1-Field amps display - digital readout
(part of CR192 module)

On top 1-Field starting and discharge resistor

Reduced-Voltage Non-Reversing (RVNR)

*Same as for full-voltage non-reversing with addition of preceding
reduced voltage sections contactor*

BRUSHLESS, SYNCHRONOUS-MOTOR STARTERS

Full-Voltage Non-Reversing (FVNR)

Same as for squirrel-cage FVNR with addition of following:

Low voltage . . . 1-Brushless-exciter field supply (7 amps
maximum)

Compartment . . 1-Variable autotransformer for exciter
field supply

On door 1-CR192 μ SPM solid-state synchronizing
device for precision time-delay field
application, load-angle field removal
and squirrel-cage protection with
built-in digital power factor and line
ammeter

1-Line amps display - digital readout
(part of CR192 module)

1-Field amps display - digital readout
(part of CR192 module)

Reduced-Voltage Non-Reversing (RVNR)

*Same as for full-voltage non-reversing with addition of preceding
reduced voltage sections*

NOTE: Drawout contactor available only for FVNR applications.



STARTERS - CR7160 AIR-BREAK

ALL STARTERS

- Enclosure NEMA Type 1 general purpose, ventilated
- Connections
- Incoming Line . . Entrance top or bottom. Cables separated by barrier from both low- and high-voltage compartments.
- Motor Cable Entrance top or bottom. Cables separated by barrier from both low- and high-voltage compartments.

SQUIRREL-CAGE-MOTOR STARTERS

Full-Voltage Non-Reversing (FVNR)

- High-voltage compartment . . 1- Draw out contactor-and-fuse (DC coil) assembly consisting of :
- 1- Set of current-limiting fuses and supports
 - 1- Isolating mechanism, externally operated. Mechanism operates in sequence to (1) open secondary of control transformer, (2) withdraw stabs, (3) close shutters over power connectors.
 - 1- Three-pole contactor
 - 1- Set of mechanical interlocks to prevent withdrawal of stabs while contactor is closed
 - 1- Control-power transformer (115-volt secondary)
 - 3- Current transformers
 - X-Terminals for motor cable connections
 - 1- Set of mechanical door interlocks to prevent opening door to high-voltage compartment until panel is isolated and to prevent energizing panel until door to high-voltage compartment is closed
 - X-Incoming-line terminals
- Low-voltage compartment . . 1- Three-pole, ambient-compensated thermal overload relay, hand-reset
- X-Instantaneous undervoltage protection
- 1- Control-circuit fuse
- On door 1- START-STOP push button, oil-tight, flush-mounted

Full-Voltage Reversing (FVR)

- Same as for full-voltage non-reversing with addition of following:*
- Auxiliary enclosure
- (one-high) 1- Drawout three-pole reversing contactor
- On door 1- FORWARD-REVERSE-STOP push button, oil-tight, flush-mounted (replacing START-STOP push button)

Reduced-Voltage Non-Reversing (RVNR)

- Same as for full-voltage non-reversing with addition of following:*
- Auxiliary enclosure
- (one-high) 1- Three-pole RUN contactor
- 1- Primary starting reactor with taps for 50-, 65- and 80-percent line voltage
- Low-voltage compartment . . 1- Definite time transfer relay

WOUND-ROTOR-MOTOR STARTERS

Non-Reversing

Same as for squirrel-cage FVNR with addition of following:

- Secondary enclosure 1- Set of intermediate accelerating contactors
- 1- Final accelerating contactor
- Resistor enclosure 1- Set of definite-time accelerating relays
- 1- Starting-duty resistor, NEMA Class 135

Reversing

Same as for non-reversing with addition of following:

- Auxiliary enclosure 1- Drawout three-pole reversing contactor
- On door 1- FORWARD-REVERSE-STOP push button, oil-tight, flush-mounted (replacing START-STOP push button)

BRUSH-TYPE SYNCHRONOUS-MOTOR STARTERS

Full-Voltage Non-Reversing (FVNR)

Same as for squirrel-cage FVNR with addition of following:

- Low-voltage compartment . . 1- Field application and discharge contactor
- 1- CR192 μ SPM for precision-angle field application, load-angle removal, and squirrel-cage protection
- On door 1- Line amps display - digital readout (part of CR192 μ SPM)
- 1- Field amps display - digital readout (part of CR192 μ SPM)



- 1- Power factor display (part of CR192 μ SPM)

On top 1- Field starting and discharge resistor

Reduced-Voltage Non-Reversing (RVNR)

Same as for full-voltage non-reversing with addition of following:

Auxiliary

- enclosure 1- Three-pole run contactor
- 1- Primary starting reactor with taps for 50-, 65-, and 80-percent line voltage

Low-voltage

compartment . . 1- Definite time transfer relay

BRUSHLESS SYNCHRONOUS-MOTOR STARTERS

Full-Voltage Non-Reversing (FVNR)

Same as for squirrel-cage FVNR with addition of following:

Low-voltage

- compartment . . 1- CR192 μ SPM for pullout protection, timed exciter field application and stall protection
- 1- Brushless exciter field supply
- On door 1- Line amps display - digital readout (part of CR192 μ SPM)
- 1- Power factor display (part of CR192 μ SPM)
- 1- Field amps display - digital readout (part of CR192 μ SPM)
- 1- Variable autotransformer

Reduced-Voltage Non-Reversing (RVNR)

Same as for full-voltage non-reversing with addition of following:

Auxiliary

- enclosure 1- Three-pole RUN contactor
- 1- Primary starting reactor with taps for 50-, 65-, and 80-percent line voltage

Low-voltage

compartment . . 1- Definite-time transfer relay





GE Electrical Distribution and Control

GET-6840B 0496 BL

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