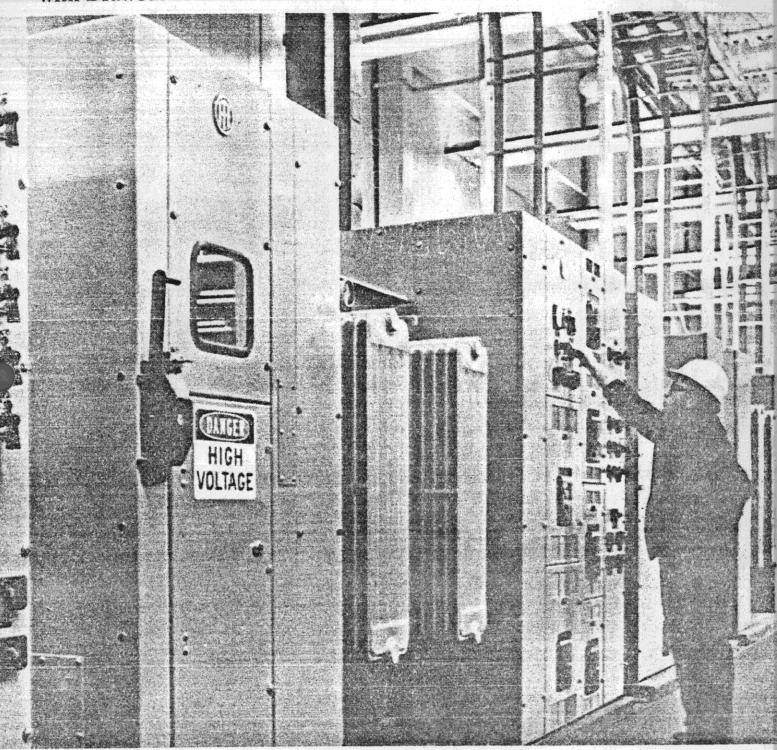
# SECONDARY UNIT SUBSTATIONS



Bulletin 10.2-1D

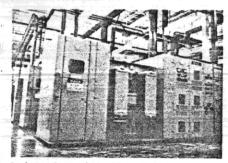
including Low-Voltage Metal-Enclosed Switchgear with Drawout K-LINE® and K-DON® Power Circuit Breakers



112½ - 2500 kVA

Primary Voltage: 2.4 kV - 13.8 kV

Secondary Voltage: 208/120 — 600 Volts
Indoor or Outdoor Sheltered-Aisle, Walk-In Liquid Ventilated or Sealed-Dry Transformers



Indoor Secondary Unit Substation consisting of Air Interrupter Switch, Askarel Transformer and Low-Voltage Switchgear.



Indoor Secondary Unit Substation consisting of Air Interrupter Switch, Ventilated-Dry Transformer and Low-Voltage Switchgear.



Outdoor Secondary Unit Substation installation.

# I-T-E SECONDARY UNIT SUBSTATIONS

## WHAT IS A UNIT SUBSTATION?

A unit substation is a substation consisting primarily of one or more transformers which are mechanically and electrically connected to, and coordinated in design with, one or more switchgear or motor control assemblies, or combinations thereof.

## SECONDARY UNIT

A secondary unit substation is a unit substation in which the outgoing low-voltage section is rated below 1000 volts. Principal areas of application include use in industrial plants, electric power generating stations, and commercial buildings.

An articulated secondary unit substation is a common type of secondary unit substation consisting of:

- An incoming line section which provides for the connection of one or more incoming high-voltage circuits, each of which may or may not be provided with a switching device or a switching and interrupting device.
- A transformer section which includes one or more transformers.
- An outgoing section which provides for the connection of one or more outgoing feeders, each of which is provided with a switching and interrupting device.

These sections are normally subassemblies intended for connection in the field.

## PURPOSE OF SECONDARY UNIT SUBSTATIONS

The trend towards location of electrical distribution systems close to the center of loads has become very prevalent in recent years. The secondary unit substation is compatible with this systems design concept because the wide array of components to select from allows tailoring it to your exact application needs. For example, the availability of askarel-filled and dry type transformers permit installation of secondary unit substations in buildings close to the load without the need of costly fire containment equipment. Secondary unit substations provide other benefits and advantages over older distribution methods:

- Reduced power losses.
- Improved continuity of service.
- Increased flexibility.
- Better voltage regulation.
- Less installation expense.
- Efficient space utilization.

#### FEATURES OF 1-T-E SECONDARY UNIT SUBSTATIONS

1-T-E has been designing, engineering and manufacturing secondary unit substations since 1943. Throughout this long history of product manufacture, 1-T-E has established itself as a reliable supplier of secondary unit substations. Some salient features of 1-T-E secondary unit substations are:

- Lower transformer and switchgear weight.
- Reduced floor space.
- Increased personnel safety.
- Coordinated engineering.
- Simplified purchasing.
- Prompt delivery.
- Design flexibility.

#### SEISMIC REQUIREMENTS

The Low-Voltage, Metal-Enclosed Switchgear has successfully passed a seismic test plan which was prepared in accordance with IEEE Std. 344-1971. Extensive testing has been accomplished as recently as 1974, and certified test results are available.

#### QUALITY ASSURANCE

The Atomic Energy Commission has issued regulations pertaining to Quality Assurance Criteria for Nuclear Power Plants (10 CFR 50 Appendix B).

Further ANSI N 45.2-1971 defines Quality Assurance Program Requirements for Nuclear Power Plants.

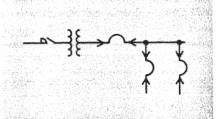
In addition, a working group has issued a draft of ANSI 45.2.14-1974 "Quality Assurance Program Requirements for the Manufacture of Class IE Instrumentation and Electrical Equipment for Nuclear Power Generating Systems." The last documentation has not been approved as yet but is being used as a guide.

These documents are used as references in the implementation of the I-T-E Imperial Corporation Switchgear Division Quality Assurance Program. Our quality assurance organization is aligned with the basic criteria of the documents mentioned above.

#### NEC & OSHA REQUIREMENTS

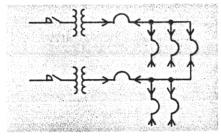
NEC generally describes parameters and techniques for a safe installation, which is also the concern of OSHA. I-T-E equipment is safe and reliable. If there are any questions regarding I-T-E equipment relative to above requirements, contact the Switchgear Division for latest information.

## SELECT THE SYSTEM



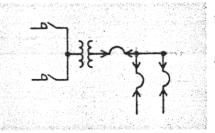
#### RADIAL

This system generally has a single incoming primary device, single stepdown transformer and an outgoing section for the connection of one or more outgoing power circuit breakers.



#### SECONDARY-SELECTIVE

This system generally has two incoming primary devices and two stepdown transformers. The outgoing side of each transformer is connected to a separate bus through a power circuit breaker. The two sections of bus are connected by a normally open power circuit breaker. Each bus has one or more outgoing power circuit breakers.



#### PRIMARY-SELECTIVE

This system contains two incoming primary devices connected to a single step-down transformer and an outgoing section for the connection of one or more outgoing power circuit breakers.

# SELECT THE COMPONENTS



# INCOMING LINE SECTION

Air Interrupter Switch
Fused or Unfused
Single or Duplex
Air Interrupter Selector Switch
Fused or Unfused
Air Terminal Chamber
Liquid Interrupter or Disconnect Switch
Oil Cutouts
Fused or Unfused
Metal-Clad Switchgear



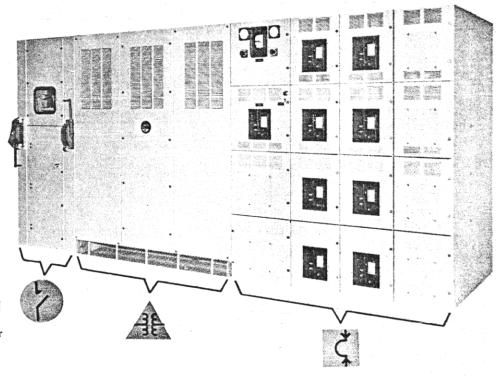
## TRANSFORMER SECTION

Liquid-Immersed Askarel Oil Ventilated-Dry Sealed-Dry, Gas-Filled



## **OUTGOING SECTION**

Low-Voltage, Metal-Enclosed Switchgear Drawout Air-Magnetic Power Circuit Breakers, Fused or Unfused Plug-in Molded-Case Circuit Breakers



#### INDEX - SECONDARY UNIT SUBSTATIONS

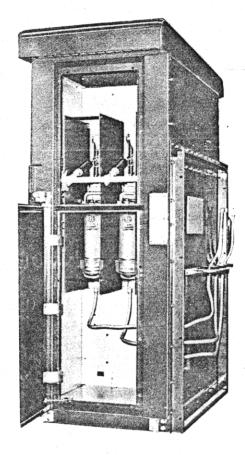
GENERAL INFORMATION 1- 3	GROUND-SHIELD® Ground Fault Protection
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Device	화물하실 왕은 동안의 전시 나왔다고 많이 다른데 보고 모르는데 없는데 되었다.
그래는 그는 그는 가장하다 하나 있다면 그 그리는 그리는 그리는 그리는 사람들이 살아왔다.	GUIDE SPECIFICATIONS



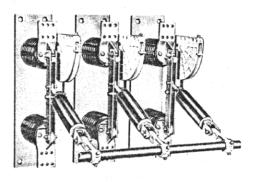
# INCOMING LINE SECTION

TABLE 1 — AIR INTERRUPTER SWITCH RATINGS

Nominal	Maximum Continuous	Fault Closing Rating, kA Asym.		
Voltage Rating, kV	Current Rating, A	Switch Unfused	Switch Fused	
4.8	600	40	Fuse Interrupting	
7.2	600	40	Rating	
13.8	600	40	(see Table 35, Page 32)	



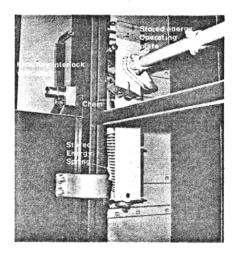
Outdoor Air Interrupter Switch



Three-Phase HPL-C Switch Assembly.

# AIR INTERRUPTER SWITCH— SINGLE OR DUPLEX

The I-T-E type HPL-C air interrupter switch is a stationary mounted, three-pole, two-position (on-off) device which utilizes a snap-action quick-make, quick-break blade in combination with an arc chute for safe closing and interruption. It is available with or without current-limiting fuses. Visual indication through the safety-glass front window and on the handle mechanism shows the blade position. Fused switches are Kirk<sup>TM</sup> key interlocked to



Stored-Energy Operating Mechanism.

Note: For complete information on HPL-C switches see I-T-E Bulletin 1630-1; for CL-14 fuses see I-T-E Bulletin 14.1-2

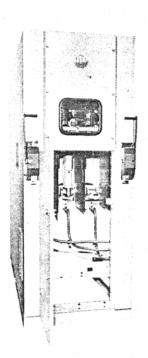
prevent opening of the fuse door while the switch is in the closed position. I-T-E type CL-14 current-limiting fuses are provided as standard. Fused or unfused switches are available with or without lightning arresters, can be equipped with cable lugs or potheads, and can be arranged for top or bottom entrance. (Lightning arresters are required for use with ventilated-dry type transformers).

Duplex switches are also available, consisting of two Kirk key-interlocked switches located side by side. These various switch assemblies are available in both indoor and outdoor construction, and can be applied to Secondary Selective or Primary Selective Systems.

For complete information on this type equipment refer to I-T-E Bulletin 8.1-1.

# AIR INTERRUPTER SELECTOR SWITCH

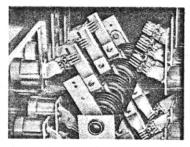
The air interrupter selector switch consists of a stationary rear-mounted, three-pole, two-position (Line 1—Line 2) switch, in series with a three-pole, two position (on-off) I-T-E type HPL-C interrupter switch. Visual indication on the front-mounted handle mechanism indicates Line 1 or Line 2.



The selector switch is Kirk<sup>TM</sup> key interlocked with the interrupter switch to prevent switching of lines with the load connected.

Fused arrangements are Kirk key interlocked to prevent opening of the fuse door while the interrupter switch is in the closed position. I-T-E type CL-14 current-limiting fuses are provided as standard. Fused or unfused switches are available with or without lightning arresters. Equipment may be supplied with cable lugs or potheads and arranged for top or bottom entrance. (Lightning arresters are required for use with ventilated-dry type transformers.

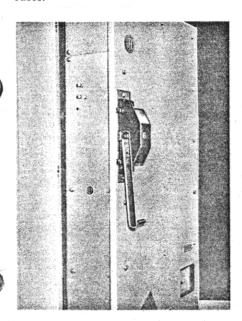
The selector arrangement is available in both indoor and outdoor construction, and is generally installed in Primary Selective systems.



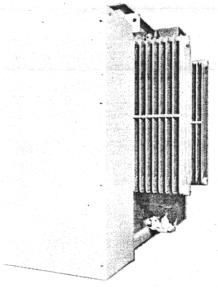
Cutaway of 3-pole selector switch shows blade positioned for connection to one incoming line.

# HPL-C DRAWOUT LOAD BREAKER

The load-breaker is a 600A, 15kV maximum, three-pole, two-position (on-off) device which utilizes snapaction, quick-make, quick-break contacts. It is available with or without fuses.

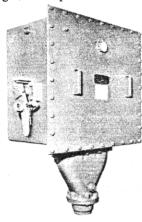


HPL-C Drawout Load Breaker



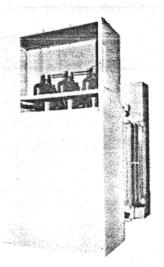
# AIR TERMINAL CHAMBERS

Floor-mounted air terminal chambers come equipped with cable lugs or potheads and are directly connected to the high-voltage side of the transformer. They are available in indoor or outdoor construction, and can be arranged for top or bottom entrance.



## LIQUID INTERRUPTER OR DISCONNECT SWITCH (OIL-ASKAREL)

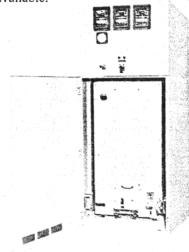
These switches can be provided on liquid-immersed transformers only. They are three-pole, two- or three-position assemblies. The switch enclosure is welded or bolted directly to the transformer tank. When oil filled, the switch can interrupt load currents up to 400 amperes. When filled with askarel, the switch has no interrupting capacity, but can be used as a disconnect switch to break magnetizing currents up to 10 amperes for five operations. After this the askarel must be replaced. Potheads are always provided for cable terminations. Oil or askarel is shipped in a separate container to eliminate the need of draining the switch to make cable connections.



## OIL CUTOUTS— FUSED OR UNFUSED

Oil cutouts are supplied mounted in an air terminal chamber and have provisions for terminating one threephase incoming cable. When fused, application of oil cutouts are limited to 500kVA at 2400 volts and 750kVA at 4160 volts and 1000kVA at 13.8kV. Unfused application as disconnects are limited to 750kVA at 2400 volts or 1000kVA at 4160 volts and 2000kVA at 13.8kV. Values are based on applying fuses at twice the full-load current rating of the transformer.

Indoor or outdoor construction is available.



## METAL-CLAD SWITCHGEAR

For the ultimate in primary protection and personnel safety, specify I-T-E type HK metal-clad switchgear with stored-energy, drawout power circuit breakers.

HK switchgear is available for systems ratings of 4.16, 7.2 and 13.8kV, 75 to 1000MVA. For complete information on this type equipment, refer to I-T-E Bulletin 8.2-1.



# TRANSFORMER SECTION

#### **GENERAL**

A complete line of secondary unit substation transformers is offered by I-T-E. Table 2 lists standard transformer ratings for the liquid-immersed (oil or askarel), ventilated-dry and sealed-dry units. Transformer dimensions and weights are given on pages 27 thru 29. Additional application data may be found on page 34.

Non-standard units are also available with special temperature rises, special insulation levels, special impedances and special voltages to meet specific application requirements. For weights, dimensions and performance characteristics contact factory.

#### LIQUID-IMMERSED

Liquid-immersed transformers have their core and coil immersed in either a flammable mineral oil or askarela synthetic non-flammable insulating liquid which is fire and explosion resistant. The oil-immersed transformer is generally applied outdoors but may also be used indoors when located in a vault designed to avoid any possible fire hazard. It is operated at 65°C rise and features lightweight and compact size. The askarel-immersed transformer is similar in construction and features to the oil-immersed type, except for the insulating liquid. It is intended primarily for indoor application, but can also be used outdoors near building walls or on roofs.

#### VENTILATED-DRY

A ventilated-dry transformer is one in which the windings are cooled by the natural circulation of ambient air through the transformer enclosure. While I-T-E ventilated-dry type transformers utilize a superior moisture resistant insulation system designed to operate at an average temperature of 150°C such units should not be applied in an area where heavy or conducting contaminates exist in the air. Ventilated type transformers feature reduced size and weight; and are fire, explosion and toxic resistant.

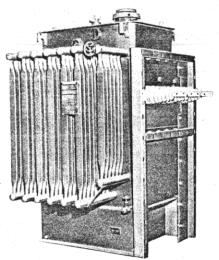
### SEALED-DRY TRANSFORMERS

The windings of the standard I-T-E sealed-dry transformers are immersed in a fluorocarbon gas which is contained in a sealed tank to prevent intermingling with outside air. The gas acts as an efficient heat transfer agent and dielectric medium. Sealed-dry transformers are generally applied indoors but can also be utilized outdoors.

TABLE 2 — STANDARD TRANSFORMER RATINGS

TYPE	Primary Voltage	kYA 3-Phase	kVA 3-Phase	SECO VOL	NDARY TAGE	Standard	N Sound	E M A Level, db
	Delta	Self- Cooled	Forced-Air Cooled	208Y/120 240 delta	480Y/277 488 delta	Impedance*	Self- Cooled	Forced- Air Cooled
Liquid- Immersed Oil or Askarel 65°C Rise †	2400 4160 4800 6900 7200 12000 12470 13200 13800	4160   225 4800   300 6900   500 7200   750 12000   1000 12470   1000 13200   1500		X X X X X	X X X X X X X	2.25‡ 3.0‡ 4.5 5.0 5.75 5.75 8.0 5.75 5.75 5.75	55 55 55 55 56 58 58 58 60 61	67 67 67 67 67 67
Ventilated- Dry 150°C Rise †	2400 4160 4800 6900 7200 12470 13200 13800	112½ 150 225 300 500 750 1000 1000 1500 2000 2500	667 1000 1333 1333 2000 2666 3333	X X X X X	x x x x x x x	3.0‡ 3.5‡ 4.5 5.0 5.75 5.75 8.0 5.75 5.75 5.75	50 50 555 555 60 64 64 65 66 68	67 67 68 68 69 71
Sealed-Dry Gas- Filled 150°C Rise †	2400 4160 4800 6900 7200 12000 12470 13200 13800	300 500 750 1000 1000 1500 2000 2500	_	X X X	X X X X X X	5.0 5.0 5.75 5.75 8.0 5.75 5.75 5.75	57 59 63 63 63 64 65 66	1111111

<sup>\*</sup> Standard Impedance tolerance is ±7½%. † For application where the average ambient temperature is 30°C. † Transformers with Impedances of 4.0% or less are designed to withstand 25 times normal current for two seconds.

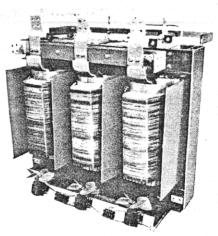


## LIQUID-IMMERSED TRANSFORMER

- Proven insulation system
- Low operating temperature
- Low sound level
- Lighter weight
- Less floor space
- Constant bushing height

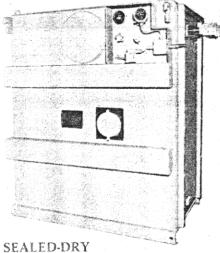


Table 3 below provides an easily comprehensible framework for comparing pertinent capabilities of liquid-immersed, ventilated-dry and sealed-dry transformers. A standard oil-immersed transformer rated 1500 kVA,



#### VENTILATED-DRY TRANSFORMER

- Moisture-resistant insulating materials
- Reduced size and weight
- Indoor application
- Toxic resistant
- Fire and explosion resistant

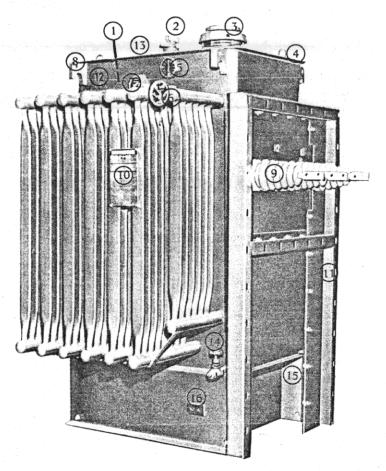


- SEALED-DRY TRANSFORMER
- Fluorocarbon gas
- Liquid filled dielectric levels
- Minimum maintenance
- Toxic resistant
- Fire and explosion resistant

13.8 kV to 480 volt, was chosen as the base transformer because of its common usage in secondary unit substations. Approximate values of various base transformer characteristics are as follows: Sound level (self-cooled)—60db Weight—8,700 lbs. Floor space—55" Wide x 87" Deep Height—80"

# TABLE 3—COMPARISON OF TYPICAL CHARACTERISTICS OF SECONDARY UNIT SUBSTATION TRANSFORMERS 1500 kVA 13.8 kV to 480 Volts, Oil-Immersed Transformer as Base (See above)

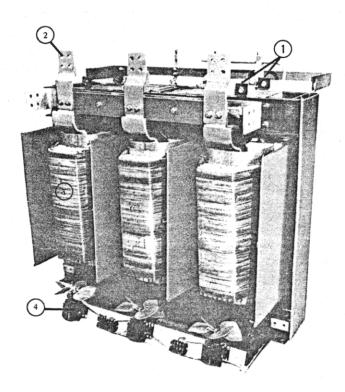
Characteristics	Liquid-im 65°C	mersed Rise	Ventilated-Dry 150°C Rise	Sealed-Dry 150°C Rise
Gilalacteristics	Oil Oil	Askarel	Air	Gas
Impulse Strength	95 kV	95 kV	65 kV	95 kV
Losses @ operating temp. (20°C Ambient) No Load Full Load	100% 100%	100% 100%	160% 130%	120% 110%
Temperature Ratings: Average Rise <sup>o</sup> , C Hottest Spot Rise <sup>o</sup> , C	<b>65</b> 80	<b>65</b> 80	150 180	150 180
Sound Level—Decibels	60	60	65	64
Weights	100%	116%	98%	166%
Dimensions: Floor Space Height	100% 100%	100% 102%	110% 112%	123% 130%
Application: Indoor, Outdoor	Indoor (vault only) Outdoor	Indoor Outdoor	Indoor (Limited)	Indoor Outdoor
Fire, Explosion Resistant	No	Yes	Yes	Yes
Toxic Resistant	No	No	Yes	Yes
Maintenance: Liquid Cleaning Internal External	Yes No Normal	Yes No Normal	No Yes Occasionally	No No Normal
Cost	100%	125%	125%	200%



Askarel-Immersed Transformer-Indoor

#### LIQUID-IMMERSED TRANSFORMERS

- Top Sampling Plug on Askarel Units Only (Not Visible)
- Padlockable No Load Tap Changer
- Mechanical Relief Device is Standard on Askarel Filled Units— Optional on Oil Filled Units
- Welded Tank Cover
- ③ Pressure Vacuum Gauge (Optional)
- ⑤ Dial Type Thermometer
- Magnetic Liquid Level Gauge
- S Lifting Hooks and Loops
- High Voltage Sealed Cast Resin Bushing
- Stainless Steel Diagrammatic Nameplate
- LV and HV Close Couple Molding
- Provision For Forced Air Cooling is Standard on Transformers 750 Kva and Above
- Upper Filter Press Connection (Not Visible)
- One Inch Drain Valve With3/8 Inch Sampler
- Base
- Copper Faced NEMA Ground Pad

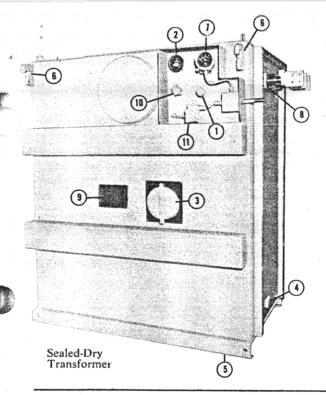


## VENTILATED-DRY TRANSFORMERS

- Lifting eyes on upper core clamp
- Secondary low-voltage connections
- 3 High-voltage winding
- ① Cooling fans

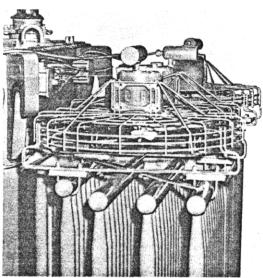
Ventilated-Dry Transformer Core and Coils Only





## SEALED-DRY TRANSFORMERS

- Filling and sampling valve
- ② Pressure-vacuum gauge
- ③ No-load, externally-operated tap changer\*
- (4) Ground pad
- Skid base with provision for jacking and towing
- Transformer lifting hooks
- ① Temperature indicator (optional)
- Hermetically-sealed bushings
- Diagrammatic nameplate
- Pressure-relief valve
- (1) Pressure switch
- \*Accessible under sealed cover



Typical Radiator Fan Installation— Liquid-Immersed Transformer.

# PROVISIONS FOR FUTURE FORCED-AIR COOLING

All liquid-immersed transformers, 750kVA and above, and ventilated-dry transformers 500kVA and above, have provisions for the future installations of fans for forced-air cooled operation.

These provisions include:

- Full forced-air cooled capacity in all current-carrying parts, including high-and low-voltage bushings.
- 2. Provision for mounting the balance of required equipment in the field.
- Provision for the future automatic control of the fans as follows:
  - a. Liquid-immersed units—provision for incorporating a thermometer with contacts for control of the future fans from top liquid temperature.
  - Ventilated-dry units—provision only for mounting winding-temperature relay for control of future fans.
- 4. Control Voltage 240V AC

#### STANDARD PRODUCTION ELECTRICAL TESTS

The following tests are performed on each transformer in accordance with the ANSI Standard Test Code:

- 1. Resistance Measurements
- 2. Ratio
- 3. Polarity and Phase Relation
- 4. No Load Loss
- 5. Exciting Current
- 6. Impedance and Load Loss
- 7. Applied Potential
- 8. Induced Potential
- Temperature test or tests will be made on one unit of an order covering one or more units of a given rating. Tests will be made only when there is not available a record of a temperature test made in accordance with ANSI standards on a duplicate or essentially

#### OPTIONAL ACCESSORIES

Winding-temperature equipment
Gas absorbers for askarel-filled transformers.
Tap changer interlocks for liquid-immersed
and sealed-dry transformers

Alarm contacts for:

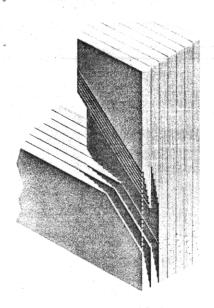
Thermometer

Liquid-level gauges

Pressure-relief device Sudden-pressure relay on liquid-immersed

transformers

## DETAILS OF CONSTRUCTION — LIQUID-IMMERSED TRANSFORMERS



#### CORE CONSTRUCTION

The core of each I-T-E transformer is made of non-aging, high permeability, grain-oriented, cold-rolled, silicon steel specifically processed for optimum loss and noise performance.

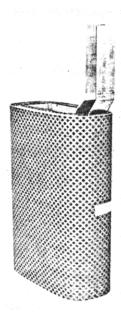
The thin gauge laminations are sheared with special high quality shear blades in such a manner that the flux path will be aligned with the axis of highest permeability in the steel. Each lamination is flat and free from burrs and is inorganically insulated on both surfaces to minimize eddy-current loss.

Core legs are assemblies of laminations with cross sections designed to accommodate the coils with the optimum combination of high space factor and coolant flow.

The upper and lower core yokes are rigidly clamped by welded assemblies of steel members consistent with bracing and supporting requirements. Core clamps are chemically cleaned to remove any dirt or impurities from the forming and welding operations. This assures that only clean, bright metal will be in contact with the cooling medium. Core clamps and all structural parts are insulated to prevent local circulating currents and are solidly bonded to ground and to the core to prevent development of potential in any part.

#### COIL CONSTRUCTION

The coil is of rectangular construction with sheet wound aluminum secondary windings and insulated wire wound aluminum primary windings.



This construction meets the following requirements:

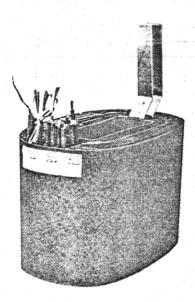
1. Stresses: Axial short-circuit stresses are virtually eliminated by the use of sheet-wound secondary and wire wound primary windings with no interleaved components. Coils are, therefore, wound with the secondary coil nearest the core and supported by a strong insulating cylinder. The primary is wound directly over the secondary coil with a suitable insulating full-length barrier between the primary and secondary windings. The coil wire is wound tightly and uniformly thru a tension device to insure maximum short-circuit strength.

Short circuit tests have been made on completed units in accordance with the latest test code for short circuit testing prepared by the IEEE Transformer Committee.

 Cooling: The coils are equipped with cooling channels in both the high and low voltage windings in order to dissipate the heat generated in the coils. Sufficient cooling ducts are located throughout the coils to avoid hot spots in winding and to assure overload capability.

#### INSULATING MATERIAL

All insulating materials used have been thoroughly tested and proven with respect to their electrical and mechanical characteristics and are stable at operating temperatures and



compatible with the cooling medium.

In liquid-filled transformers, the insulation system is thermally upgraded. It is chemically modified to resist the effects of high temperature. The improved insulation enables the new, compact transformers to maintain full load-carrying ability at their higher operating temperature without affecting life expectancy.

Thermally-upgraded pressboard insulation is used for coil spacers, both longitudinal and radial, as well as ends. It is also used between layers and between high- and low-voltage coils. The porosity of the insulating materials permits the insulating liquid to penetrate the insulating materials giving it a high dielectric strength.

#### TAP CHANGER

The externally operated tap changer provides positive sequence line voltage changes under no-load conditions. The in-line assembly features throughtype stationary contacts rigidly supported by a molded plastic channel. Moving contacts are spring loaded, silver plated copper which move along the stationary line by means of a rack and pinion.

The design has no rivets, bolts or nuts, thus assuring the proper contact of current carrying parts when taps are changed.

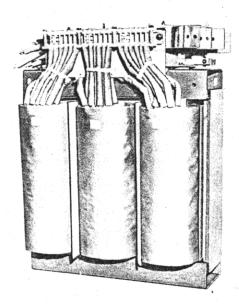
#### TANK

The transformer tank is fabricated of heavy-gauge steel plates. A minimum number of plates are used to reduce the number of welded seams.

The tank base is fabricated of formed steel to receive and transmit



# DETAILS OF CONSTRUCTION —VENTILATED-DRY-TYPE TRANSFORMERS



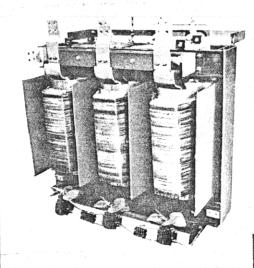
the core and coil weight to the mounting pad or foundation and provide for skidding or rolling in any direction. Facilities for jacking are at the ends of the base.

Formed structural members are welded to the side walls so that the complete tank will be sufficiently reinforced to withstand a test pressure 75% greater than normal operating pressure. This will prevent permanent tank distortion during operation or pressure testing. The top of the tank is fully strengthened by a flange which is used as a welding ring for securing the tank cover. An asbestos-type gasket is provided between the reinforced cover and the top flange and is compressed during the welding operation to prevent weld spatter from entering the tank. Lifting hooks are provided at the corners of the tank to permit the finished transformer, complete with liquid, to be handled by a crane.

Adequate convection surface is provided by cooling tubes to assure that the temperature rise of the liquid will not exceed the specified limit when the transformer is continuously operated at full load.

The entire tank is chemically cleaned before painting to remove any oil, dirt or other impurities from the forming and welding operation. Each tank is painted with a rust inhibiter prime coat and a finished coat in accordance with ANSI standards.

A flange is provided on the primary and secondary sides of the transformer for bolting to the primary and secondary sections to provide an uninterrupted lineup of equipment without openings.



#### CORE CONSTRUCTION

The core construction of each I-T-E transformer is made of non-aging, high-permeability, grain-oriented, cold-rolled, silicon steel specifically processed for consistently low losses.

The thin-gauge laminations are sheared with special high-quality shear blades in such a manner that the flux path will be aligned with the axis of highest permeability in the steel. Each lamination is flat and free from burrs and is inorganically insulated on both surfaces to minimize eddy-current losses.

Laminations are hand stacked on a specially designed table which ensures flatness and prevents the introduction of bending stresses while the finished core is being set in an upright position. Careful positioning of each lamination produces close fitting joints to fully minimize core loss and noise.

Core legs are assemblies of laminations with cross sections designed to accommodate the coils with the optimum combination of high space factor and air flow.

#### COIL CONSTRUCTION

The coil may be of rectangular or circle construction depending upon the kVA size. Where possible rectangular construction is used with sheetwound aluminum secondary windings and insulated, wire-wound primary windings. This construction meets the following requirements:

 Stresses: Where sheet windings are employed axial short-circuit stresses are virtually eliminated. The primary is wound directly on the low-voltage winding with a suitable insulating barrier between the coils consisting of spacers and sheet insulation builtup to the proper thickness.

Where the coils are wire wound adequate bracing is supplied at the end of the coils to assure full short circuit capability. Primary coils may be of the disk type construction with suitable disk spacers to provide coil to coil cancellation.

All coils are dried and compressed in preparation for varnish impregnation. A suitable varnish for the temperature rating of the unit is applied by dipping to provide a coil with moisture and dirt resistance. Extreme care is taken to avoid tiny air pockets in the coils where corona might start.

After dipping the varnish is completely cured in ovens to achieve the highest possible dielectric strength.

2. Cooling: Cooling is achieved in all ventilated dry type transformers by generous cooling ducts in both the primary and secondary coils. When forced air

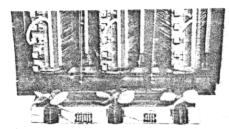
cooling is required the air is directed through the cooling ducts to achieve the forced air rating.

#### INSULATING MATERIAL

All insulating materials used have been thoroughly tested and proven with respect to their electrical or mechanical characteristics and are stable at operating temperatures and compatible with the cooling medium. All wire is Nomex paper-wrapped. All other insulating material in the core and coil is chosen for the temperature system of the transformer and capability for that point of application.

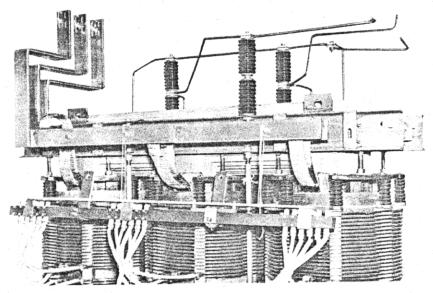
#### TAPS

Taps are applied on the face of the coil for link or cable connection to provide for adjustment in the primary winding to accommodate system voltage.



# DETAILS OF CONSTRUCTION —SEALED-DRY-TYPE TRANSFORMERS

#### SEALED-DRY



Core and Coils-Sealed-Dry Assembly



Bushings

#### CORE CONSTRUCTION

The core construction for sealeddry type transformers is similar to both the liquid-filled and ventilateddry type transformers. The major exceptions being where a circular coil is applied.

Where a circular coil design is applied a cruciform core is used to achieve a high space factor.

#### COIL CONSTRUCTION

The coil construction for sealeddry transformers is similar to the coil construction of the ventilated type transformers. Generally, circular coils are applied with disk type primary coils.

#### TAP CHANGER

A tap changer of the in-line type is supplied with an operating mechanism extending through the tank wall with a sealing means to prevent the loss of gas from the unit.

### FLUOROCARBON GAS

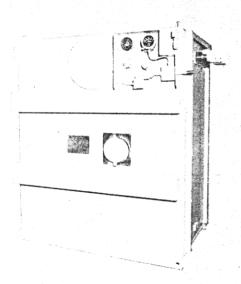
Fluorocarbon gas is applied as the dielectric medium for sealed-dry type transformers. Such gases have a dielectric capability in excess of 2 times the dielectric capability of air. This high dielectric capability results in di-

electric levels normally achieved in liquid-filled transformers.

In addition to being an excellent dielectric medium the gas has good heat transfer capability due to its higher molecular weight. In comparison to nitrogen the use of the fluorocarbon gas permits a smaller tank and a lighter unit for the same rating.

#### TANK

The tank of the sealed-dry type transformer is similar in construction to the liquid filled type. It, however, is designed to withstand 15 lbs. pressure or vacuum. Other features include; protective instrumentation, external stiffeners and welded bushings.





## I-T-E COST-SAVING LOGICAL-SEQUENCE ASSEMBLY FOR VENTILATED-DRY TYPE TRANSFORMER ENCLOSURES

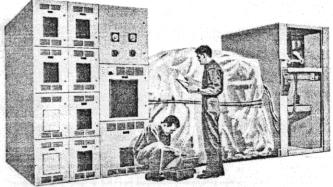
Saves installation time, money and floor space. Instead of shipping the enclosure already assembled around the transformer, I-T-E ships it ready to assemble.

You unpack the components in a logical sequence for easy assembly. That way you don't have to do the

double work of taking the enclosure apart, making the connections in tight quarters, then assembling it again. Installation is faster, easier, more economical—and you have a far better assurance of good results. Rigging is simplified and the transformer can more easily be moved under pipes,

through doors, onto elevators and into position. Just follow these simple steps.

If project requirements dictate, transformer and enclosure can be shipped assembled for additional cost.



 First step—position all components. Transformer is delivered wrapped in plastic to protect it from dirt.



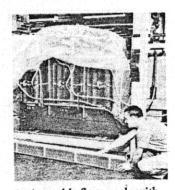
Make low-voltage connections.



Make high-voltage connections.



Connect low-voltage ground.



Assemble floor angle with screen attached.



6. Assemble corner panels.



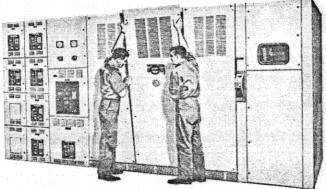
7. Assemble top cross angles.



8. Assemble temperature panel (if furnished).



9. Assemble top sheets.

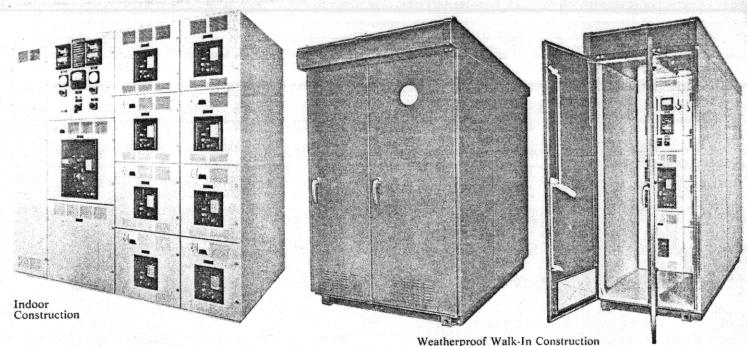


10. Assemble center panels. Job's done.



## OUTGOING SECTION

## LOW-VOLTAGE SWITCHGEAR



Compact I-T-E low-voltage metal-enclosed, drawout switchgear features time-tested, field-proven manually or electrically operated stored-energy K-LINE® and K-DON® air-magnetic power circuit breakers. The standard design offers various size circuit breakers mounted in 4-high compartments (see page 30 for low-voltage switchgear arrangements). In addition, modern insulating materials with high strength-to-weight ratios allow significant reduction in weight and floor space.

#### INDOOR CONSTRUCTION

Free-standing, indoor units offer complete isolation of breaker and instrument compartments. The versatility of compartments, frames and breaker ratings enables meeting your exact application requirements. Notice the semi-flush circuit breaker handles do not project into the aisle, thereby reducing accidental breakage or false tripping. Also each feeder may be equipped with a panel-mounted ammeter and pushbutton phase selector for convenient reading.

# WEATHERPROOF WALK-IN CONSTRUCTION

Weatherproof walk-in construction provides all-weather protection when the switchgear must be located outdoors. The same arrangement principles are used in weatherproof as in standard indoor construction. In addition, this construction provides approximately three feet of aisle space on the breaker side to protect equip-

ment and personnel from inclement weather. Also provided are large areas at the top and bottom of each frame for cable entry. Large working area, is provided in the rear compartment for pulling and connecting cables.

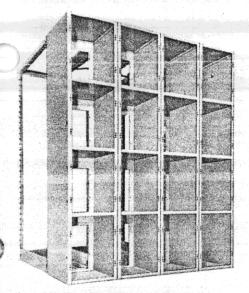
Standard outdoor construction provides:

- 1. Manually-operated lifting device.
- Filtered louvers and vents, front and rear.
- Strip heaters to reduce condensation.
- Convenience outlets and interior lighting.
- Weatherproof gasketing throughout.

A control-power transformer may be mounted in an auxiliary compartment, if required, to furnish power to outlets and strip heaters.

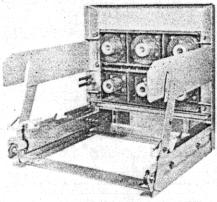
TABLE 4 — SWITCHGEAR RATINGS

	①	Nominal	Maximum		Insulation Levels, kV	Limit of He	ottest Spot		
Switchboard Construction	Circuit Breaker Type	Voltage Rating, V	Voltage Design Maximum		Voltage Design Maximum Power Frequency Voltage, Continuous Power Frequency		Power Frequency Withstand (rms)	Temp. Rise (°C)	Total Temp. (°C)
Indoor	K-LINE	600	630	4000	2.2	∘ 65	105		
Outdoor	K-DON	600	600	1600	2.2	65	105		



#### SWITCHGEAR FRAME

Individual frame consists of a bus and cable area and up to four circuit breaker compartments. Switchboards are assemblies of multiple individual frames. Each frame is welded in a fixture which assures rigid construction, strong enough to support switching equipment. Frames are erected and securely bolted to each other. This type of construction permits versatility in selecting unit sizes for shipment and duplicate manufacturing ensures complete interchangeability in field installations.



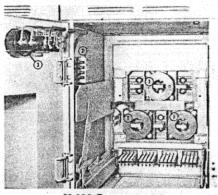
#### CIRCUIT BREAKER CRADLE

A cradle comprises main and secondary separable contacts, current transformers (if required) and all other drawout mechanisms in a complete jig-welded rigid assembly. There is no dependence upon the switch-board frame for any critical alignment. Any size cradle can be installed into any compartment of its own size or larger. Blank compartments not required for other functions may be converted to a circuit-breaker compartment by the installation of a cradle and necessary riser bus modifications.

### CIRCUIT-BREAKER COMPARTMENT

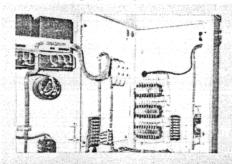
All individual circuit-breaker compartments are isolated from each other and from the bus area. Front door louvered grilles are scientifically designed to allow full air circulation. Hinged doors are flanged for greater rigidity. Hinges are completely concealed by being mounted inside the enclosure, and are adjustable for perfect door alignment. A removable pin within the hinge assembly provides easy door removal. Knurled panel screws fit easily into floating retainer nuts for quick, easy alignment. These screws offer the utmost in safety in keeping the doors securely closed even under the most severe fault conditions.

Control separable contacts are tiered, upper and lower, so you can mount twice as many within the narrower dimensions—as many as 32 in each compartment. This means auxiliary circuits for your use. Standardized wiring of circuit breakers and



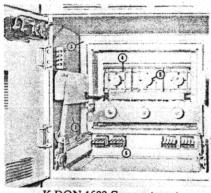
K-600 Compartment

- Current transformers are front mounted and easily accessible from the circuit-breaker compartment.
- © Current transformer short-circuiting block is conveniently located behind circuit-breaker compartment door.
- Feeder ammeter is located directly on feeder compartment door for easy reading and space saving. Rear view of ammeter is shown.
- Modern polyester-glass insulation



devices to particular terminals makes maintenance far easier. Notice also that the control contacts are located at the bottom where they are safe. They are front removable to make replacement or modification easily accomplished from within the circuit-breaker compartment.

Fully-insulated, high-dielectric epoxy-molded toroidal current transformers are located on the stationary primary leads within the circuit-breaker compartment. Convenient location and accessibility makes changing a minor maintenance procedure. Standard low-voltage current transformers have metering accuracies in conformance with ANSI C37.20. Current transformer short-circuiting block has safe, convenient location. It is placed at front of circuit-breaker compartment and can be easily reached with circuit breaker still in compartment.



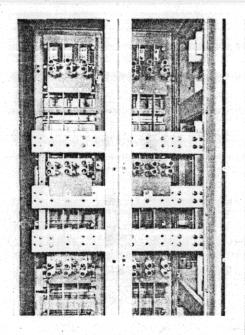
K-DON-1600 Compartment

system is used throughout switchgear.

- Stationary primary leads mate with movable primary leads mounted on circuit breaker.
- Secondary disconnects are removable from the front for ease of accessibility.
- ① Complete compartment isolation is provided between each K-LINE® or K-DON® circuit breaker and main bus compartment.

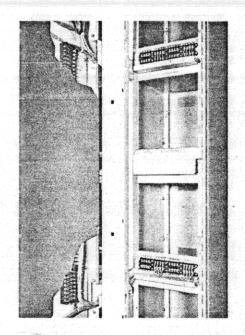
Low-Voltage Metal-Enclosed Switchgear with Auxiliary Instrument Compartment Showing Electrical Connections.

### BUS AND CABLE COMPARTMENT



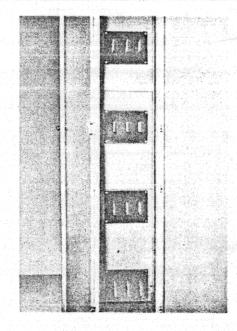
#### POLYESTER-GLASS INSULATION SYSTEM

All insulating parts of the switchgear are made of high-strength polyester glass. Each insulated part is specially designed in shape and strength to fulfill its part of a totally integrated insulation system.



# ENCLOSED SECONDARY WIRING TROUGHS (optional)

All secondary wiring and terminal blocks located in the bus compartment are enclosed in completely covered metal troughs to afford complete isolation from the switchgear bus.



## REAR BARRIERS (optional)

For those who prefer to have a completely isolated cable area, rear barriers are available. The primary leads are extended through slotted polyester-glass inserts which are mounted in a solidly-grounded metal isolating panel. Note that hinged rear doors are standard.

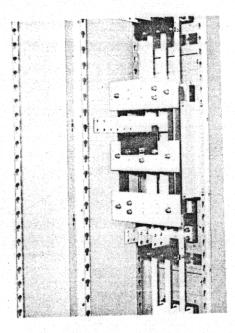
#### OVERHEAD LIFT DEVICE

For ease of handling K-LINE circuit breakers, a traveling overhead lift device can be provided. This device is supported from the front section of the switchgear assembly and will not affect any incoming power or control cables at the rear bus section. The hoist can be moved the full length of the switchgear and with the aid of a lifting yoke, the breaker can be

lifted from the floor or from the completely withdrawn breaker cradle. Lifting power is provided through a removable hand-crank, worm-driven mechanism and sturdy flexible cable. Although the driving mechanism is designed for easy hand operation, the weight of the breaker cannot accidently move the mechanism even when the crank is unattended or removed.



Overhead Lift Device on Indoor Switchgear



## VERTICAL BUS ARRANGEMENT

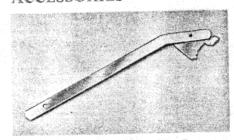
The three-phase main horizontal bus is vertically arranged one above the other and is located as close to front of switchgear as possible, providing large area for auxiliary equipment and cable makeup. Vertical mounting of bus provides maximum

ventilation, and freedom from dust. Bus is designed for an allowable temperature rise of 65°C above an average 40°C ambient. All insulating parts of the switchgear are made of highstrength polyester-glass. Each insulated part is specially designed in shape and strength to fulfill its part of a truly integrated insulation system. A section of the top sheet of each frame is removable to facilitate installation of overhead conduit and cable. All rear leads are easily accessible for simple connection with a minimum of cable bending.

Aluminum bus is silver-plated and is braced against movement in any direction under all possible short-circuit conditions. Pre-slotted mounting members permit flexibility to add mounting supports when required in the field for incoming cables, etc. Vertical risers connecting breakers to the main bus are welded for space saving. The connections of the vertical risers to the main bus and breaker

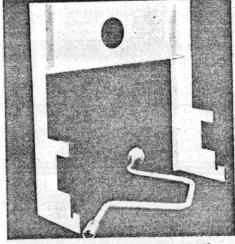
terminals are bolted.

#### ACCESSORIES



Spring-Charge Maintenance Handle

Each factory-assembled switchgear is shipped with circuit-breaker racking crank and lifting yoke as standard accessories. A maintenance handle for manual spring charging is included on electrically-operated breakers only.

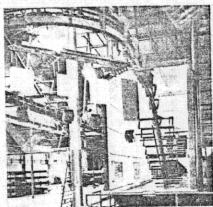


Circuit Breaker Racking Crank and Lifting Yoke.

### A PAINT FINISH TO MATCH TRADITIONAL I-T-E QUALITY

- Smooth, uniform paint finish
- Complete paint penetration
- Corrosion-resistant
- Electro-chemical bonding of paint to metal
- Long-lasting paint finish

All standard low-voltage switchgear frames are painted by an automated, industry-first electro-deposition paint process. This multi-stage cleaning and painting operation is automatically controlled to provide uniform paint thickness throughout. The metal frame is completely immersed in a huge, electrically charged "gray river" of light gray, ANSI #61, epoxy enamel paint. Current flow from paint to part immediately bonds the epoxy paint to every exposed surface of the metal. Termed "electrocoating", this process provides an attractive and durable paint finish of the highest quality.



Switchgear Being Immersed in "Gray River"

The electrocoating process entails preparation of the metal and application of the color coat. The metal receives a series of alternate alkaline cleansing and water rinse operations, followed by a phosphatizing treatment. After the metal is properly prepared, the frame is immersed in light gray, ANSI #61, epoxy enamel paint for a specified time period. Following another water rinse, the paint finish is baked dry.

All standard switchgear frames and other metal work used in outdoor switchgear are painted in the manner described. In addition, the weather-proof enclosure for outdoor low-voltage switchgear also receives a spray application of dark gray, ANSI #24,

baked acrylic enamel.

## POWER CIRCUIT BREAKERS

TABLE 5 - K-LINE® POWER CIRCUIT BREAKER RATINGS

① Circuit	Maximum Continuous	Interrupting Cap	acity, Symmetrica	I RMS Amperes
Breaker Type	Current Rating, A	240 Volts	480 Volts	600 Volts
( K-225	225	25,000	22,000	14,000
K-600	600	42,000	30,000	22,000
K-1600	1600	65,000	50,000	42,000
K-2000	2000	85,000	65,000	55,000
K-3000	3000	85,000	65,000	65,000
K-4000	4000	130,000	85,000	85,000
K-600S	600	42,000	30,000	22,000
K-1600S	1600	65,000	50,000	42,000
K-2000S	2000	85,000	65,000	55,000
K-3000S	3000	85,000	65,000	65,000
K-4000S	4000	130,000	85,000	85,000

O K-LINE breakers equipped with a POWER-SHIELD solid-state overcurrent trip device have their normal designations suffixed with an S.

#### K-LINE®

K-LINE circuit breakers have been developed for the protection of feeder circuits and for use as main breakers where the interruption requirements are within the ratings shown in Table 5.

This modern line of low-voltage, air-magnetic, drawout power circuit breakers offers a selection of either manually or electrically (motor charged) operated spring-closing mechanisms, which provide positive quick-make operation. K-LINE circuit breakers can be provided with either a direct-acting, electro-mechanical or a solid-state overcurrent trip device. They are compact and come equipped with many other features which are particularly adaptable to general lowvoltage switchgear applications.

For application information on K-LINE circuit breakers, refer to pages 35 and 36.

#### K-DON B

The K-DON circuit breaker is a compact, versatile protective device which incorporates all of the features of the K-LINE circuit breaker and the current-limiting characteristics of the Amp-Trap† fuse. The current-limiting fuses are integrally mounted on, and physically connected in series with, the breaker. Each K-DON circuit breaker is equipped with an antisingle-phase device to prevent single phasing. No external tripping power is required to operate the anti-singlephase device.

The circuit breaker performs its normal function of time delay and instantaneous tripping throughout its entire range of interrupting capacity. When properly applied, the fuse takes over protection for currents at or above the circuit-breaker short-circuit current rating up to 200,000 amperes. For currents within the circuit-breaker interrupting capability, the fuse will not open unnecessarily thus saving nuisance replacements. This system affords vast flexibility in applying pinpoint protection to any type of electrical apparatus. For application information on K-DON circuit breakers, refer to Pages 37-41.

† Registered Trademark-Chase-Shawmut Co.

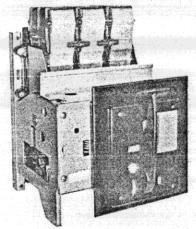
#### TABLE 6 - K-DON® POWER CIRCUIT BREAKER RATINGS®

①	Maximum	Interrupting Capacity,
Circuit	Continuous Current	Symmetrical RMS Amperes
Breaker Type	Rating, A	240, 480, and 600 Volts
K-DON-600	600	200,000
K-DON-1600	<b>1</b> 600	200,000
K-DON-600S	600	200,000
K-DON-1600S	<b>1</b> 600	200,000

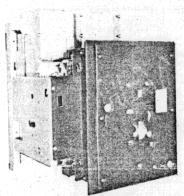
Fused circuit breakers with 2000, 3000 and 4000A continuous current ratings are available with separately mounted, drawout, current-limiting fuses. Refer to Page 30 for arrangement information and Page 40 for application data.

 K-DON breakers against a state of the Page 30 for arrangement information and Page 40 for application data.

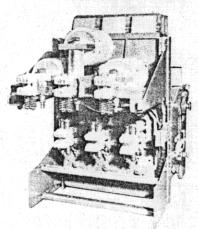
K-DON breakers equipped with a POWER-SHIELD solid-state overcurrent trip device have their normal designations suffixed with an S.



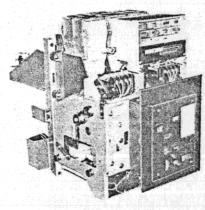
Manually Operated K-600



Electrically Operated K-3000

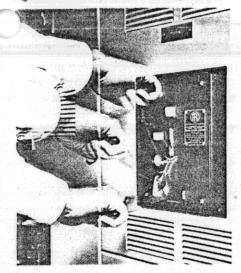


Rear View Manually Operated K-Don-600



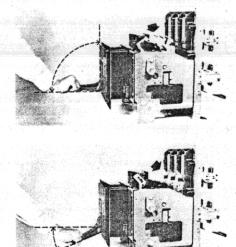
Electrically Operated K-Don 1600S with SS5 Power Shield Unit

# MANUAL STORED-ENERGY GIVES QUICK-MAKE, QUICK-BREAK OPERATION



#### LESS UPKEEP, LONGER CONTACT LIFE

Manually-charged, stored-energy breakers offer many advantages to its users. Of primary importance is the added safety for operating personnel. This quick-make mechanism also provides longer contact and breaker life and increases the scope of application for manual breakers. K-LINE® breakers cannot be teased into the closed position. A pair of powerful springs actually close the contacts. For breakers with frame size ratings from 225 through 2000 amperes, the operator simply supplies energy to the device



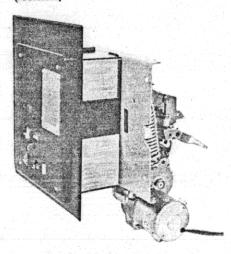
by pulling the semi-flush closing handle downward to approximately 100°. The initial 90° fully charges the closing springs and the remaining motion releases the spring energy to drive the contacts into the closed position by a smooth cam action. The fully-charged springs develop sufficient energy to close and latch the breaker safely under any conditions within the breaker rating. A flushmounted manual trip button is located on the easily-accessible breaker escutcheon. It is also equipped with a hand-reset automatic trip indicator which provides for visual indication of automatic trip operation.

### ELECTRICAL OPERATION

All K-LINE circuit breakers are also available with motor-charged, stored-energy closing mechanisms to be used when remote control or local electrical control is required. The normal control power required by this mechanism is only a fraction of the power requirement for a solenoid closing mechanism.

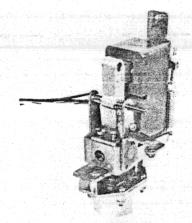
A fractional-horsepower motor with enclosed speed-reduction gears provides the closing energy. The high-torque, high-speed output easily charges the powerful closing springs. The springs are retained in a fully-charged condition until the energy is required for closing. Upon tripping, the springs are again recharged automatically by the mechanism. An emergency charging handle is provided for manual charging if control power is lost. A manual closing lever on the escutcheon permits simple manual close with the compartment door

closed. All stored-energy springs are automatically discharged for safe breaker maintenance when the circuit breaker is racked to the disconnect position.

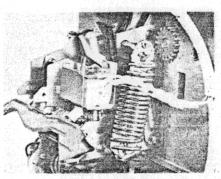


Electrical-Operating Mechanism

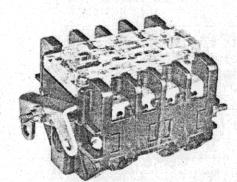
### BREAKER COMPONENTS



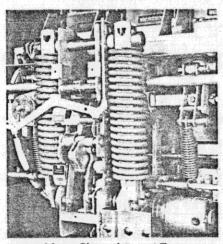
Undervoltage Trip Device



Shunt Trip Device



**Auxiliary Switch** 

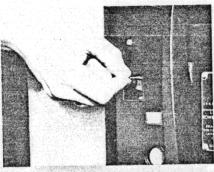


K-3000 Motor-Charged Stored-Energy Operating Mechanism

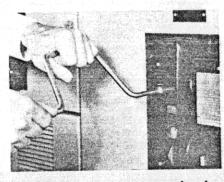
## SAFE, EFFICIENT, CLOSED-DOOR DRAWOUT

The circuit-breaker compartment door need never be opened while moving the K-LINE® circuit breaker from the completely connected through test into the disconnected position. Unique construction reduces I-T-E switchgear to three basic components: frame, breaker and a removable cradle on which the breaker rolls for drawout. The mechanism permits racking the breaker into connected, test and disconnected positions without ever opening the compartment door. It facilitates testing and maintenance and promotes safe operation. A lift shutter is provided on the breaker escutcheon which permits insertion of a racking crank to move the breaker. It is completely interlocked, i.e., the shutter cannot be lifted while the circuit breaker is closed and the circuit breaker cannot be closed while the shutter is lifted. When open, the breaker can be padlocked in the connected, test or disconnected positions. When padlocked, the breaker cannot be closed or moved to any other position.

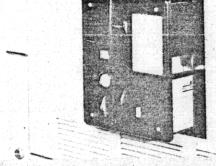
The extendable escutcheon mounted on the circuit breaker slides through an opening into the compartment door while the spring-loaded cover plate surrounding the escutcheon is held in place by the door. Visual indication on the side of the breaker denotes all three positions. Compartment doors may be opened, if desired, when the breaker is in any position. To remove the breaker from its compartment, it must be racked to the fully-disconnected position, the door opened and the breaker pulled manually to the fully-withdrawn position while it is supported by extended sliding rails. After release of the safety latch, the breaker may be lifted directly from the rails by means of an overhead lift device and moved with a transfer truck or be handled completely with a combination lift device and transfer truck.



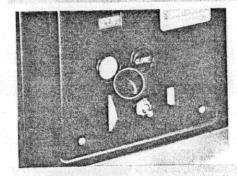
LIFT SHUTTER must be raised to insert breaker racking crank. It cannot be raised when breaker contacts are closed.



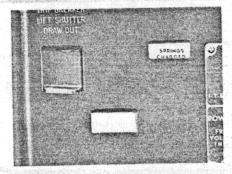
INSERT CRANK to move breaker between positions. Crank cannot be inserted without raising lift shutter.



READ BREAKER POSITION from target on the right side of escutcheon. When breaker is in disconnected, test or connected positions, lift shutter will close. Breaker contacts cannot be closed until lift shutter is closed.

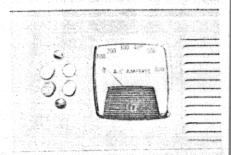


MANUAL CLOSING LEVER. All electrically operated breakers can be closed manually with the compartment door closed, if control power is lost, by simply pulling the closing lever. Closing springs can also be charged manually with a hand lever.

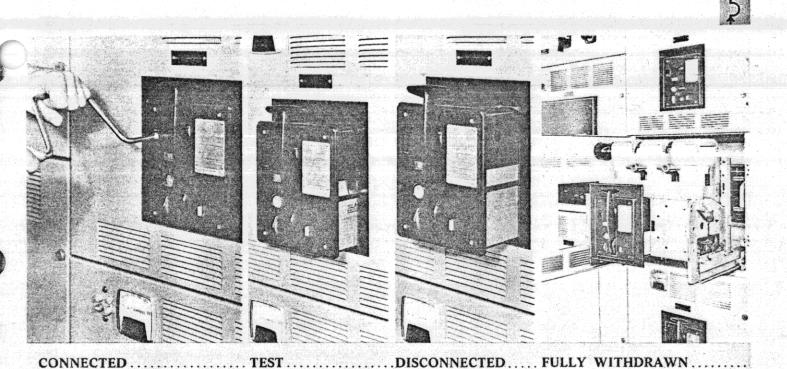


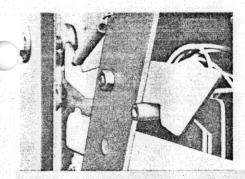
SPRING-CHARGED INDICATOR shows condition of stored-energy springs on electrically-operated breakers.

OPEN-CLOSED INDICATOR visually shows position of breaker contacts directly on front of escutcheon.

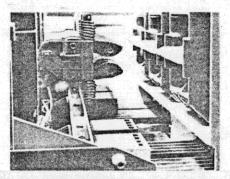


FEEDER AMMETER. Each feeder compartment can be equipped with a door-mounted ammeter and push-button switch for easy, convenient reading and space saving.

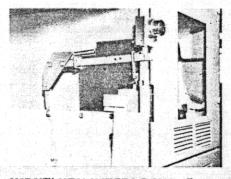




RAIL LATCH prevents breaker from rolling off track when breaker is fully withdrawn. Latch must be released to lift breaker from rails.



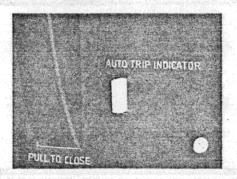
PRIMARY, SECONDARY AND GROUND CONTACTS on the circuit breaker mate sequentially in a straight-line motion with counterparts within the switchgear. This insures proper breaker operation at each position.



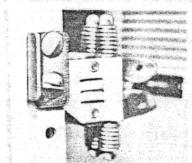
KIRK<sup>TM</sup> KEY INTERLOCKS offer an unlimited number of interlocking arrangements between all components of the switchgear. They are particularly adaptable to sequential operations or prevention of unauthorized operation.



PADLOCK PROVISION. The circuit breaker, when open, can be padlocked (with up to three locks) in all three positions. When padlocked, it cannot be closed or moved to any other position.



AUTOMATIC-TRIP INDICATOR gives visual indication when the breaker has tripped from a fault or other overcurrent conditions.



INTERFERENCE KEY on the breaker mates with slot on cradle allowing only the proper rated breaker to be inserted into the compartment. It is virtually impossible to insert a lower rating into any compartment.

## OD—ELECTRO-MECHANICAL OVERCURRENT TRIP DEVICE

'K-LINE® type OD electro-mechanical overcurrent trip devices have been designed to provide dependable performance with virtually noiseless and vibration-free operation. I-T-E low-voltage power circuit breakers equipped with this rugged device are available in any desired combination of long-time delay, short-time delay and instantaneous tripping. Each overload is individually calibrated, tested and certified by Quality Control to assure "as designed" performance and service.

OD-3 and OD-300 Dual-Magnetic Direct-Acting Trip Device

The OD-3 and OD-300 are fully adjustable, dual-magnetic overcurrent trip devices. They employ a dual armature. One is connected to an oil-displacement dashpot to provide long-time delay. A second armature provides instantaneous trip characteristics. The overload on each pole has independent adjustment for long-time delay pick-up, instantaneous pick-up, and the amount of time delay. It is a self-contained, direct-acting, electromechanical device which depends on its own circuit for tripping power. No external tripping power is required.

Expanded-range calibration is incorporated to provide a greater number of usable calibrated long-time pick-up settings. Conventional trip devices provide only two calibrated pick-up settings (80% and 100%) which may be used continuously without excessive overheating. Table 59, page 43, shows the increased number of calibrated long-time pick-up settings within 100% of the continuous current rating of each trip coil. This feature permits a user to select a device with a trip coil rating which provides adequate protection for present power requirements and also permits an increase in capacity by means of simple adjustments.

A wide range of adjustment makes this rugged unit ideal for protection of motors and equipment which require close protection.

Production units have been subjected to more than 4,000,000 welding type pulse test cycles without failure—thus proving a long-life design! OD-3 and OD-300 units now in service have proven themselves in many difficult application including heavy-duty welding circuits.

OD-4 and OD-400 Dual-Selective Direct-Acting Trip Devices

The OD-4 and OD-400 direct-acting trip devices combine the fluid-displacement type time delay with mechanicalescapement time delay to provide a composite time-delay device in which it is possible to closely control the time-delay over a range of current values from normal load current to the full interrupting current rating.

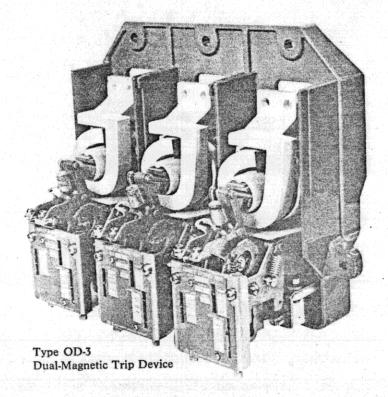
This allows the direct-acting trip devices of circuit breakers in series to be set so as to permit selective tripping of the circuit breaker closest to the fault. Thus maximum continuity of electrical service may be provided where such continuity is mandatory.

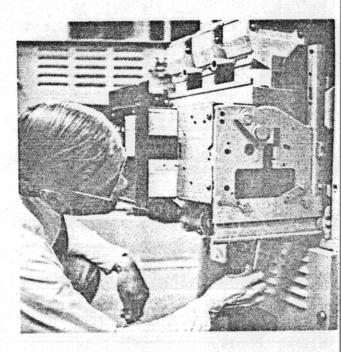
#### EASY TO ADJUST

Trip devices are clearly visible and within easy reach from the front of the circuit breaker. Even on electrically-operated circuit breakers, they are readily accessible to the operator for quick, easy adjustment.

#### EASY TO SERVICE

The three-phase overcurrent trip device assembly is mounted on a one-piece, impact-resistant polyester-glass molding for breaker sizes up to K-600. On larger size breakers the overcurrent trip device assembly consists of three individual units. If repair or replacement is required, the assembly is easily removed from the back of the breaker. Associated devices need not be disturbed.





Adjusting and servicing OD device is simple and convenient.

## POWER-SHIELD® — SOLID-STATE OVERCURRENT TRIP DEVICE

## GENERAL INFORMATION

POWER-SHIELD is a three-phase solid-state, overcurrent trip device designed for low-voltage power system protection against damage caused by overload and short-circuit conditions. It can be integrally mounted on K-LINE® and K-DON® low-voltage power circuit breakers. The logic assembly of the POWER-SHIELD system is mounted on the shelf above and behind the breaker escutcheon for easy accessibility to the control panel. POWER-SHIELD is suitable for application on low-voltage circuits rated up to 600V ac, 50/60 Hertz. Available standard types and their related trip functions are shown in Table 61 page

The POWER-SHIELD solid-state overcurrent trip system consists of current sensors, logic assembly, magnetic latch release and interconnecting wiring. There are two current sensors mounted on the breaker lower base molding around each primary conductor. One sensor supplies the logic assembly with a signal current proportional to the primary current, and is referred to as the signal sensor. The other sensor, designated the power supply sensor, supplies the power required to operate the magnetic-latch release and solid-state circuitry. The logic assembly contains the circuitry and various tap-blocks used to set the overcurrent trip levels and time delays. A transparent cover is provided over the tap blocks. The magnetic-latch release is similar in function to a shunt-trip device, but is powered by the fault current through the power-supply sensors, and is actuated by the logic assembly system.

## SIMPLE TAP CHANGING

The wide rating range of each device, coupled with its simplified field adjustment, allows almost unlimited load growth within each breaker frame size. Only seven different sizes are required for the full range of 35 thru 4000 amperes (see page 44). Field setting is accomplished by insertion of tap plugs into the front of the logic unit. All settings are made in this fashion, including the ampere tap which selects the continuous rating of the current sensor. This setting is shown directly in primary amperes, giving the user a positive indication of the continuous current rating of his circuit breaker. The long-time, shorttime and instantaneous functions are then adjusted by tap plugs which are a percentage of this ampere tap setting. In addition, three time-delay bands, minimum, intermediate and maximum can be selected for both the long-time and short-time functions. All

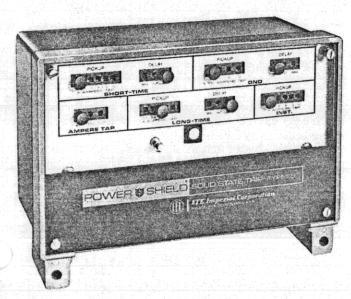
time-current curves are straight lines, asymptotic at the pick-up point to produce optimum coordination with other protective devices. Coordination is made even more positive by the wide separation between all time-delay bands.

Optional ground and/or short timeinstantaneous operation indicators are available.

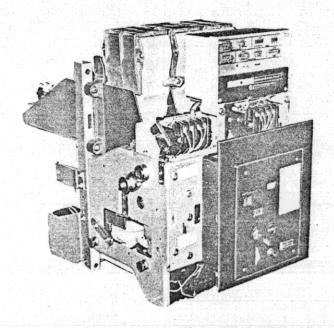
Also available as an option is an alarm contact for remote indication.

## GROUND-FAULT PROTECTION

POWER-SHIELD is available with multiple ampere taps for a wide range of pick-up currents. The ground function can be included in the logic assembly for those applications in which it is desirable to protect the system against faults to ground. These are often damaging arcing faults which result in current magnitudes below the pick-up of the long-time trip function. 3-wire applications with ground protection do not require any additional sensors. For 4-wire applications, one ground sensor is remotely mounted around the neutral conductor and is wired to the logic assembly through a breaker secondary disconnect. The ground function is tap selected directly in amperes, and is independent of the ampere tap setting.



Front view of SS-5G POWER-SHIELD logic assembly.



Front view of K-DON-1600 S electrically-operated breaker equipped with SS-5 POWER-SHIELD unit.

# GROUND-SHIELD® - SOLID-STATE GROUND FAULT PROTECTION

GROUND-SHIELD is the registered family trademark for a variety of solid-state relay systems designed to protect electrical distribution circuits and electrical loads from the damage caused by the inadvertent flow of ground-fault currents. Three (3) systems are offered: (1) GR-5 and GR-200, (2) GRM-motor circuit applications, and (3) GRD-three-phase differential.

The GR-5 and GR-200 GROUND-SHIELD Systems offer fast, sensitive protection against ground-faults including destructive, low-magnitude, arcing ground-faults in solid and resistance grounded distribution systems. They consist of a special-design, corebalancing current transformer (sensor) and a low-burden, solid-state ground relay.

The ground sensors are available with small or large-window configurations designed to enclose all phase and neutral bus or cable conductors. These sensors will respond only to groundfault currents. Balanced or unbalanced load currents, two-phase or threephase short circuits not involving a ground return conductor, will have no effect on the sensor. Two (2) pickup ranges are available, one with 5 ampere minimum sensitivity, and one with 200 ampere minimum sensitivity. The 5A system (GR-5 relay) with 5-50A pickup adjustment (special pickup ranges of 2-40A and 20-200A are also available) is used for protection of individual loads such as motors and transformers. On high-resistance grounded systems the 5-50A relay is used for both circuit and load protection. The 200 ampere system (GR-200) relay with 200-1200A pickup adjustment is used for circuit protection.

The 5A system provides five timecurrent curves of definite time shape. Four time-current curves are available for the 200A system. All relay calibrations are in primary amperes. Tripping of the desired breaker (coordination) is obtained by applying relays with successively faster curves progressing from source to load circuits. Relays are available for surface mounting and semi-flush panel mounting.

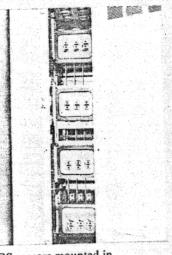
GRM System offers fast, sensitive and inexpensive protection against ground faults in individual motor starter and contactor circuits (type GRM-NC) and electrical distribution

systems using molded-case circuit breakers with shunt trips (type GRM-

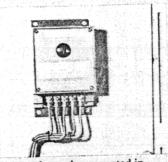
The system consists of a special small diameter current transformer (sensor) and an instantaneous, mechanically latched ground relay with a 10 ampere sensitivity. The ground sensor, which encircles all phase conductors, comes in 2" (GSM-1) and 3" (GSM-2) inside diameters.

GRD Differential System provides fast, sensitive protection against phaseto-phase or phase-to-ground faults occurring in 3-phase motors, generators, reactors, etc. This system consists of three solid-core current sensors type GS-5 and one 3-phase, solid-state ground differential relay type GRD, which operates the shunt-trip device on the circuit breaker. The ground differential relay and the associated current sensors are connected in a selfbalancing scheme. The GROUND-SHIELD differential system has a sensitivity of 2 amperes primary fault current, operates in 2 cycles, and is significantly more economical than comparable conventional differential relays operated from current transformers.





GS sensors mounted in cable compartment.



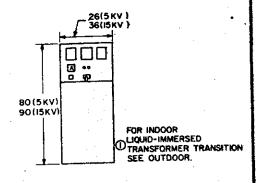
GR surface relay mounted in instrument compartment.

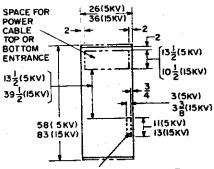
## FEATURES OF STORED-ENERGY K-LINE<sup>®</sup> AND K-DON<sup>®</sup> CIRCUIT BREAKERS

	STANDARD FEATURES INCLUDE:	K-225 K-600 K-1800 K-2000	K-3000 K-4000	K-DON- 600 1600	K-600S K-1600S K-2000S	K-3000S K-4000S	K-DON-600S K-DON-1600S
1		×	No	х	X	No	X
MANUALLY OPERATED	Springs charged and breaker closed with manual handle Springs charged only with manual handle	Ño	X	No	No	X	No
	Manual close lever—door closed	No No	X	No No	No No	X	No No
<u> </u>	Springs-charged indicator	-	<del></del>				
.	Springs charged with motor—after trip	X	., X	X	X X X X X X	X	X X X X X X
	Electrical closing release Manual close lever—door closed	X	$\hat{\mathbf{x}}$	Ŷ	x	Ŷ	x
OPERATED	Shunt-trip device	Ŷ	Ŷ	X	Ŷ	X	X
	Control relay Charging-motor disconnect switch	Ŷ	Ŷ	â	â	â	Ŷ
ELECTRICALLY	Springs-charged indicator	X X X X	X	X	X	X X X X X	X
5	Secondary disconnects (operating and test position) 4-Contact auxiliary switch	X	X X X X X X	X X X X X X	×X	X	X
5	Provision for manual spring charge	X	Х		X	Х	
		(Door Open)	(Door Closed)	(Door Open)	(Door Open)	(Door Closed)	(Door Open)
		·····	<u></u>				
	Manual trip button Breaker contact-position indicator	X X X	X X X X	X X X	X X	. X	X X X
<b>a</b>	Breaker racking-position indicator	ÿ	<u>X</u> :	ä	X	, X	X
OPERATED	Racking interlock (breaker must be open prior to racking)	X No	X ·	X No	X No	X	X No
<b>≥</b>	Positive racking stops  Padlock hasp—up to three locks (locks breaker trip-free and in position)	X	x	X	X	X	X
ELECTRICALLY	Padlock hasp—up to three locks (locks breaker trip-free and in position)  Breaker interchangeability interlock	X	X	, <b>X</b>	, X	X	. <b>X</b>
	Direct-acting overcurrent trip devices (dual-magnetic, other combinations, except dual-selective)	X	X	X	No	No	No
	Solid-State overcurrent trip device (long-time and instantaneous, SS-3)	No	No	No	X	. X	X
OR E	Automatic trip indicator (overcurrent and undervoltage trip)	X X	X	X ·	X X X	X	X
	Primary disconnects—(operating position only) Ground disconnect—(operating and test position only)	Х	Ŷ	X X X X X	x	X	X X X X X X
	Manual slow-close provision	X	X X X	X.	X X	X	X
MANUALLY	Actuator to discharge springs on withdrawal from switchboard Amp-trap, current-limiting fuses	X No	. No	â	Ño	Ño	â
≨	Anti-single-phase device	No	No	X	No	No	X.
	Local electrical trip button—(on escutcheon)	X	X	X	Х	X	х
	I Shunt trip with 4-contact auxiliary switch (2 spares)—M.O. only	X	X	X	X No	X No	X No
	Dual-selective, direct-acting overcurrent trip device Solid-State overcurrent trip device (Dual-Selective, SS-4 and SS-5)	Ño	No	Ño	X	X	X
	Operation indicator (target) and load alarm for solid-state trip	No	No	No	X	. X	X
	Mechanical lockout on automatic trip (reset by indicator)  —Overcurrent and undervoltage trip	X	· <b>x</b>	X	Х	X	<b>X</b> .
ន	Overcurrent alone (special trip for undervoltage)	X	×	X	X	X	. <b>X</b>
<b>5</b> 6	Alarm switches—1 N.U. and 1 N.C. (reset by indicator)		Y	¥	¥	X	x
IL FEATURES t as noted)	—Overcurrent and undervoltage trip —Overcurrent alone (special trip for undervoltage)	X	X	X X	X	X	×
- S	Auxiliary switches—spares			<b>.</b> .	J.	v	v
るか	4 or 8 Contacts—E.O. only	X X	X X	X	X	X	X
FX	—4, 8 or 12 Contacts—M.O. only Undervoltage-trip device				•		
2.5.	iInstantaneous	X	χ̈́	X	X X X	X	X
ADDITIONAL OPTIONA (E.O. of M.O. except	—Time delay—Adjustable 0 - 15 sec. Operation counter	X X	X X X X	X	Ŷ	X X X X	X
	Remote electrical-close releaseM.O. only	No	x	No	No X	X	No X
퉏	Wiring change to charge springs when breaker closes Hinged door interlock—door locked when breaker closed	X	X	X	â	· ŝ	â
-	Mechanical-transfer interlock—two breakers using flexible						
,	cable arrangement	X X X	X X	X X X	X X X	X X X	X X
	Additional secondary disconnects up to 32 maximum total Secondary disconnects—operating and/or test position only	â	Х	× x	X	ÿ	X
	Key interlocks—switchboard mounted—2 maximum	X	X	<del></del>			X
55	Racking crank	X	X	X	X	. X X	X
ĕ88	1 Lifting voke	X X X	X	X	X	â	â
STANDARD ACCESSORIES	Maintenance spring-charge handle—E.O. only Slow-close bracket	Ño	X	Ño	Ño	X	X No
ES.	Tourist and life house	~	×	х	У	¥	Y
OPTIONAL ACCESSORIES	Transfer and tift truck Overhead lift device—(standard outdoor)	X X X	Χ.	X	X	X X	X X X
	Floor dolly	X	X	X	· X	X	X
تة 👊	Test set for solid-state trip	. No	No	No	X	X	

# DIMENSIONS \*

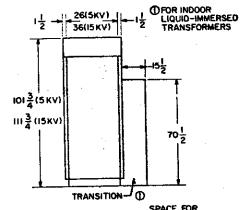
# METAL-CLAD SWITCHGEAR Indoor

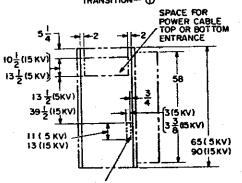




SPACE FOR CONTROL CONDUIT (PROVISIONS FOR (3) 2" PURCHASERS CONDUIT WITH A 3" MAXIMUM EXTENSION ABOVE FLOOR)

### Outdoor





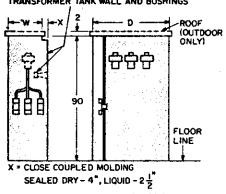
SPACE FOR CONTROL CONDUIT (PROVISIONS FOR (3) 2" PURCHASERS CONDUIT WITH A 3" MAXIMUM EXTENSION ABOVE FLOOR)

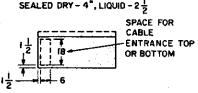
## **INCOMING LINE SECTION**

## OIL CUTOUTS

Indoor - Outdoor

TRANSFORMER TANK WALL AND BUSHINGS





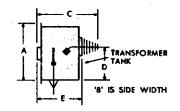
#### TABLE 7 - OIL CUTOUTS

	Liq	við	Ventilated and Sealed-Dry		
Device	W	D	W	D	
5 kV — 100, 200A	221/2	48	21	48	
5 kV 300A 15 kV 100, 200A	441/2	58	43	58	

## LIQUID SWITCHES

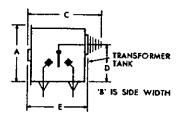
Indoor - Outdoor

#### TWO POSITION



kV	TA S	* B *	· C	D	E
5	211/8	301/2	23	13¾	173%
15	26	341/2	24	161/4	1836

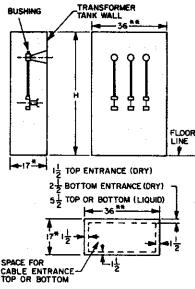
#### THREE POSITION



∴ kV	PASS	В	* C	<b>€</b> B′	E
5	221/6	28	253/4	143/4	201/4
15	26	32	283/4	171/4	231/8

#### AIR TERMINAL CHAMBER

Indoor - Chadoor

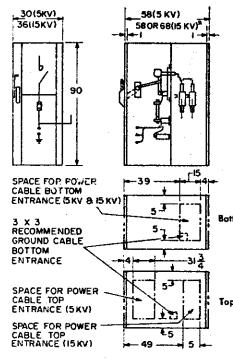


\*ADD I\* ON ALL VENTILATED-DRY TRANSFORMERS
\*\*\*WHEN USED WITH VENTILATED-DRY
TRANSFORMER-MATCH TRANSFORMER DEPTH

## TABLE 8 — AIR TERMINAL CHAMBER

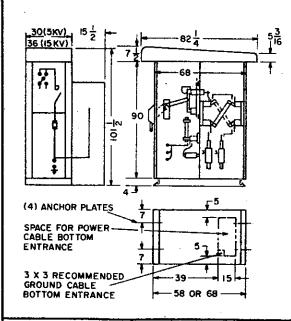
	Trsfr. Liquid Dim. H		Sealed-Dry H	VentDry H	
kVA	kV	Top or Bott Entrance	Top or Bott Entrance	Top or Bott Entrance	
500 to 2500	5 or 15	94	110	90	

# AIR INTERRUPTER SWITCH—Indoor

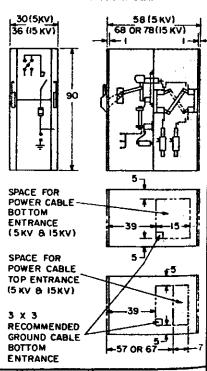


\*DOUBLE POTHEAD TOP ENTRANCE

## SELECTOR SWITCH-Outdoor



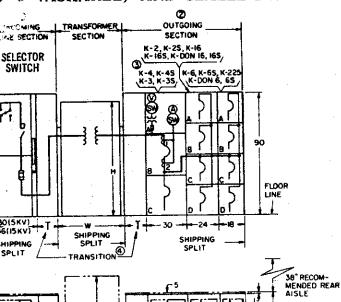
## SELECTOR SWITCH-Indoc



Dimensions are in inches. Both Dimensions and Weights are approximate

## CONDARY UNIT SUBSTATION ARRANGEMENTS

## コロ (ASKAREL) AND SEALED-DRY—Indoor



FLUOROCARBON BAS TRANSFORMERS

ONLY, CENTER LINE FOR SWITCH FRAME, TRANSITION, & SWITCHBOARD

TO BE IN LINE

SPACE FOR

POWER CABLE TOP

ENTRANCE

①③ OUTGOING

48" RECOM-MENDED

AISLE SPACE FOR BREAKER

WITHDRAWAL

D

3 X 3 RECOMMENDED

GROUND CABLE BOTTOM

ITILATED-DRY— Besselve

**(1)** 

TRANSFORMER

ENTRANCE

①② OMING LINE

### TABLE 9 — AIR INTERRUPTER SELECTOR SWITCH

OLDEO I O II								
(Voliator	Cable Entrance	G		e als <sub>i</sub> .				
5kV	Bottom	·58	39	15				
5kV	Тор	68	57	7				
15kV	Bottom	68	39	15				
15kV	Тор	78	67	7				

- incoming Section (15kV) must be 68" deep when furnished with 2 3/c potheads for top entrance. When main bus is over 4000 amperes, consult 1-T-E district sales office. K4000 (2-45" high compartments) breaker located in bottom

- compartment.
  Transition units are supplied assembled to the Incoming Line Section and Outgoing Section.

TABLE 10-ASK

AVA.	hicomia Section
500	
750	·
1000	5 kV or
1500	or 15 kV
2000	
2500	

\* For 208Y/120 volts Δ For 8% impedance

TABLE 13 - VENTILATED-DRY	TRANSFORMER
150°C RISE	

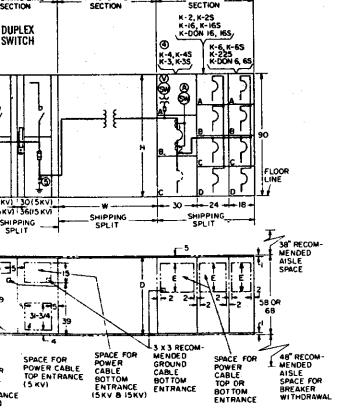
kVA Incoming Section	Incoming	Dimensions, in.				
	Section	Wt	н	D		
500				,		
750	1	78	90	58		
1000	5 kV	<b></b> -				
1500	or 15 kV	90	96	İ		
2000	1	<b></b>		68		
2500		102	108			

† An 18" wide transition unit must be supplied when no main breaker is used.

#### TARLE 14 - LOW-VOLTAGE SWITCHGEAR

	]	"E" DIMENSION, in.								
Circuit	Frame	With	out	Wit	th		r with	Neutra	3ø4w	
Breaker	Width	M	ain Bus	Barrier			Sensor	with Main Bus Barrier f		
Туре	Inches			Sw	itchgea	r Depth,	in.			
		58	68	58	68	58	68	58	68	
K3 & K3S, K4 & K4S	30	21*	31*	12	22	-	171/2	71/2	171/2	
K2 & K2S, K16 & K16S	24	21	31	12	22	_	171/2	71/2	171/2	
K-225 K6 & K6S,	18	21	31	12	22	_	171/2	7½	171/2	
K-DON 16 & 16S	24	161/2	261/2		171/2	—	13	-	13	
K-DON 6 & 6S	18	161/2	261/2		171/2	I —	13		13	

- \* With bottom entrance to K-3000 in compartment C, subtract 6".
- † For main breaker unit or with K-3000 in compartment C.
- ① Incoming, Transformer and Outgoing Sections will always have their fronts aligned. ② Incoming Section (15 kV) must be 68" deep when furnished with 2—3/c potheads for top
- When main bus is over 4000 amperes, consult I-T-E district sales office.
   K-4000 (2-45" high compartments) breaker located in bottom compartment. Distribution-type lightning arresters are always required.



## "NO SEALED-DRY TRANSFORMER

ر 2.59 2.59	arel Rise			Sealed-Dry 150°C Rise						
	Y. H	D	100			8				
46		68		82	84	58				
49		84	15 <del>1/</del> 2	84	04	30				
54	86	97		88	94	60	14			
55		100		96	104	62				
61		105		100	104	65				
65		110		104	114	68				

tion, add 8".

## TABLE 11 - LOW-VOLTAGE SWITCHGEAR

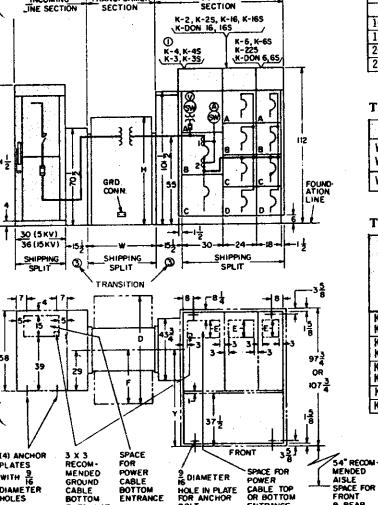
A SA CALLINGTEDIA	
Without Main Breaker with K-LINE® Feeders With Main Breaker with K-LINE or K-DON Feeders	32
Without Main Breaker with K-DON® Feeders	361/2

#### TABLE 12 -- LOW-VOLTAGE SWITCHGEAR

				E Dia	ension.		100
Circuit	Frame	With	out   Main Bus			Feeder	enuor ?
Breaker Type	Width,	2,834.1		or Neut Sensor; in.			
		58	. 68	58	68	58	<b>68</b> (
K3 & K3S, K4 & K4S	30	21*	31*	12†	22†		171/2
K2 & K2S, K16 & K16S	24	21	31	12	22	-	171/2
K6 & K6S, K-225	18	21	31	12	22	_	171/2
K-DON 6, 6S	18	161/2	261/2		171/2		13
K-DON 16, 16S	24	161/2	261/2		171/2	-	13

<sup>\*</sup> With bottom entrance to K-3000 in compartment C, subtract 6". † With K-3000 in compartment C & 3φ, 4w system, subtract 41/2".

### IQUID (OIL & ASKAREL) Outdoor OUTGOING TRANSFORMER SECTION INCOMING



## TABLE 15-OIL & ASKAREL TRANSFORMER -65°C RISE

kYA	W	OIL OIL	H ASK.	D
500	46			68
750	49			84
1000	54	84	86	97
1500	55	Ŭ.		100
2000	61			105
2500	65			110

### TABLE 16 -- LOW-VOLTAGE SWITCHGEAR

"Y" Dimension	
Without Main Breaker with K-LINE Feeders With Main Breaker with K-LINE or K-DON Feeders	691/2
Without Main Breaker with K-DON Feeders	74

#### TABLE 17 — LOW-VOLTAGE SWITCHGEAR

			"E" Dimension							
Circuit		With	Without Wit		th	Feeder with				
Breaker Type	Frame Width	,	Aain Bus I	Ground or Neutral Sensor						
iype			Sw	itchgea	in.					
	1	973/4	107%	9734	1073/4	973/4	16734			
K3 & K3S, K4 & K4S	30	18*	18*	11†	18†		131/2			
K2 & K2S, K16 & K16S	24	18	18	11	18		131/2			
K6 & K6S, K-225	18	18	18	11	18	_	131/2			
K-DON 6 & 6S	18	151/2	18		161/2	<u> </u>	12			
K-DON 16 & 16S	24	151/2	18	_	161/2	_	12			

With bottom entrance to K-3000 in compartment C subtract 6".
 † With K-3000 in compartment C & 3φ 4w system subtract 4½".

K-4000 (2-45" high compartments) breaker located in bottom compartment. When main bus is over 4000 amperes, consult I-T-E district sales office.

Transitions shipped disassembled.

# **WEIGHTS**

## INCOMING LINE SECTION

TABLE 18 - PRIMARY DEVICE WEIGHTS, LBS.

Type Primary Device	The second second	Depth loor			3	3	13/6 31/6
and the state of t	<b>58</b> 58	68	· • 58 ···	∞ 68 ∞	Fuses	بالباد	Pothead
5 kV Unfused Switch	900	1000	1350				
15 kV Unfused Switch	1200	1300	1800	<u> </u>			
5 kV Unfused Selector	1100	1200	1550				
15 kV Unfused Selector		1600		2250			
Air Terminal Chamber			i				
Liquid Switches	2-Po	sition	3-Position		. :		
5 kV		50	500		200	50	100
15 kV		15	640				100
Oil Fused Cutout 5 kV—100, 200A	900						
Oil Fused Cutout 5 kV—300A 15 kV—100, 200A	1300						

## TRANSFORMER SECTION

TABLE 20 - TRANSFORMER WEIGHTS, LBS.

Transformer	Volts,	TRANSFORMER KYA					
Type	kV	500	750	1000	1500	2000	2500
Ventilated-Dry	5 or 15	5000	5800	7000	8500	10000	11500
Liquid-Askaret	5 or	5900	6900	8400	10100	12100	14500
Liquid-Oil	15	4900	5900	7200	8700	10500	12600
Sealed-Bry	5 or 15	8500	10000	12500	14400	18000	22000

TABLE 19— METAL-CLAD SWITCHGEAR WEIGHTS, LBS.

Circuit	Cont.	के स्वकार करावृत्	Server De	pth	End Panels
Breaker :	Current,"	Breaker Weight	Indoor	Outdoor	
Type	A. S.		58"	85″	
5HK75	1200	550	1325	1690	
5HK250	1200	560	1325	1690	545
5HK250	2000	580	1458	1823	
5HK350	1200	750	1400	1790	
5HK350	2000	760	1533	1923	590
			83"	90~	
7.5HK500	1200	995	2170	2675	
7.5HK500	2000	1005	2411	2916	775
15HK500	1200	925	2170	2675	•
15HK500	2000	1005	2411	2916	
			91"	98~	
15HK750	1200	1345	2260	2778	<b>83</b> 5
15HK750	2000	1355	2501	3019	
- <del></del>	AUXI	LIARY EQU	IPMENT	<u></u>	

5HK-Potential transformer, drawout unit with 3 PT's-216 lbs. 15HK-Potential transformer, drawout unit with 3 PT's-515 lbs. 5 & 15 kV-Stationary-mounted, control-power transformers to 15 kVA-305 lbs.

5HK-Drawout fuse unit-160 lbs. 15HK-Drawout fuse unit-295 lbs.

## OUTGOING SECTION

TABLE 21 — LOW-VOLTAGE SWITCHGEAR WEIGHTS, LBS.

	Frame	Switchgear Depth, in.			
Type Unit	Width,	Indoor		Outdoor	
	inches	58	68	973/4	1073/4
*K-225, K-6 & 6S,	18	750	850	1300	1420
K-DON 6 & 6S		900	1000	1450	1570
K-16 & 16S, K-2 & 2S, K-DON 16 & 16S	24	1000	1200	1650	1880
*K-3 & 3S,	20	1550	1750	2300	2535
K-4 & 4S	30	1600	1800	2350	2585
Auxiliary Units	18	700	800	1250	1370
(Bus Transition)	24	800	900	1450	1580
Includes Bus	30	900	1000	1650	1785
End Panels	11/2		-	1000 Per Swbd	1125 Per Swbd
Overhead Lifting Device		100 Per Switchboard		đ	
†Terminal Block Pans	_	110			
Main Dun	18		65		
Main Bus Barriers	24		90		
Switchgear only Door not	30	110			

\*Switchgear only. Does not include breakers. For breaker weights, see Table 23. †For electrically operated circuit breakers.

TABLE 22—TRANSITION UNIT WEIGHTS, LBS.

14"		151/2"		
Switchgea	r Depth			
58″	68"	Indoor	Outdoor	
400	450	425	475	

TABLE 23-CIRCUIT BREAKER WEIGHTS, LBS.

Туре	Manual Operation	Electrical Operation
K-225	102	123
K-6 & 6\$	112	133
K-16 & 16S	185	206
K-2 & 2\$	204	225
K-DON 6 & 6S	142	163
K-DON 16 & 16S	264	285
K-3 & 3S	520	548
K-4 & 4S	533	561

# ARRANGEMENTS-0076

### **PYOHIGH**

INST.

COMPT. A

8

45

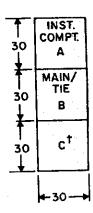
## TABLE 24

Compartment Can Be Fiften With				
Quan.	Туре			
1	K-4000	Compt. B		
1*	Drawout Fuse	Compt. A		
1	KP, HP, HR, CF (KP & HP PLUC	or CR G-IN ONLY)		
2	HM or CM			
4	KM, HK or CJ			
6	JJ, JL, HJ or HL			
12	FJ or CE			
20	EF, EH or HE			

<sup>\*</sup> Fuse size 6000A. 4000A maximum continuous current rating.

† Power Co. metering compt. 40".

### THREE-HIGH



#### TABLE 25

Each 30" Wide x 30" Righ Compartment Can Be Fitted With			
Quan.	Туре		
1.	K-2000	Compt. C	
1.	K-3000	Compt. C	
1	K-3000	Compt. B	
10	Drawout Fuses	Compt. B	
1	KP, HP, HR, CP (KP & HP PLUG	or CR IN ONLY)	
2	KM, HM, CJ or	CM	
4	JJ, JL, HJ or HL		
8	FJ or CE		
12	EH, EF or HE		

- When used with drawout fuse units.

  Fuse sizes 5000-4000A (K-2000).

  Fuse sizes 4000-6000A (K-5000).
- 5000A maximum continuous current rating.
- \* Can be equipped with any lower rated breaker.

## FOUR-HIGH

**1** 30 €

TABLE 26

22 <u>1</u>	Α
22 1	В*
72 - 12	С
22 1	D
	24-

Each 24" Wide x 22½" High Compartment Can Be Fitted With			
Quan.	Туре		
1	K-16		
ī	KD-16		
1	K-2		
1	KP, HP or HR (KP & HP Plug-in only)		
2	JJ, JL, KM, HJ, HK, HL, CJ		
4	FJorCE		
8	EF, EH or HE		

#### LEGEND

K-6 = K-225, K-600& K-600S

K-16 = K-1600 & K-1600S

K-2 = K-2000 & K-2000

KD-6 = K-DON-600& K-DON-600S

 $\mathsf{KD\text{-}16} = \mathsf{K\text{-}DON\text{-}1600}$ 

& K-DON-1600S

## TABLE 27

22 ½	Α	
22 1 2	8	
22 2	С	
22 12	D	
	418→	

Each 18" Wide x 22½" High Compartment Can Be Fitted With		
Quan.	Туре	
1	K-6	
1	KD-6	
1,	JJ, JL, KM, HJ, HK, HL or CJ	
3	FJ or CE	
6	EF, EH or HE	

#### NOTES:

All frames may be fitted with the same size circuit breaker in each compartment except as follows:
1—Only one K-2000 breaker in each 24" wide frame.

\*2-Main and Tie must be located in compartment B.

Preferred arrangement for the same size breakers in each 18" or 24" W compartment is as follows:

No. of same size circuit breakers	Compartment
1	В
2	B, C
3	B, C, D

## TABLE 28 - K-6, K-16 AND K-2 ARRANGEMENTS

Compt	<del>,</del>		*****	•	, A	Type I	Breake	r	• • • • • •		7		. A.	
A Dumpe	K-16	K-6	K-6	K-6	K-16	K-6	K-6	_				_		_
R	K-2	K-2	K-2	K-2	K-2	K-2	K-2	K-2	K-2	-K-2	K-2_	K-2	_	_
<del>-</del> -	K-16	K 16	K-16	K-6	K-16	K-16	K-6	K-16	K-16	K-6	K-16	K-6	K-2	K-2
	K-16	K-16	K-6	K-6	<b>-</b>		<u> </u>	K-16	K-6	K-6		<u> </u>	K-16	K-6

## TABLE 29 — K-6 AND K-16 ARRANGEMENTS

Compt.				Тур	e Brea	ker			
A	K-6	K-6	K-6	K-6	K-6	_			
В	K-16	K-16	K-16	K-16	K-16	K-16	K-16		K-16
C	K-16	K-16	K-6	K-16	K-6	K-16	K-6	K-16	K-6
D	K-16	K-6	K-6			K-6	K-6	K-6	

## TABLE 30- KD-6 AND K-16 ARRANGEMENTS

į	Compt.	_ <del></del>	<del></del>		T	ype Br	eaker			
٠	<u> </u>	KD-6	KD-6	KD-6	KD-6	KD-6	_			
	3	K-16	K-16	K-16	K-16	K-16	K-16	K-16		K-16
1	c	K-16	K-16	KD-6	K-16	KD-6	K-16	KD-6	K-16	KD-6
ł	D	K-16	KD-6	KD-6			KD-6	KD-6	KD-6	

## TABLE 31 --- KD-6 AND KD-16 ARRANGEMENTS

Compt.					e Brea	ker			
A	KD-6	KD-6	KD-6	KD-6	KD-6		-	1	
B	KD-16	KD-16	KD-16	KD-16	KD-16	KD-16	KD-16		KD-16
	KD-16	KD-16	KD-6	KD-16	KD-6	KD-16	KD-6	KD-16	KD-6
D	KD-16		KD-6		_			KD-6	_

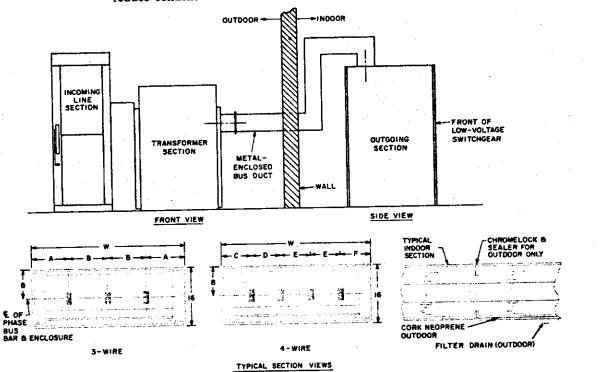
## TABLE 32 — K-16, K-2 AND KD-6 ARRANGEMENTS

Compt				Тур	e Brea	ker		·	
Α	KD-6	KD-6	KD-6	KD-6	KD-6	_		<u></u>	
В	K-2	K-2	K-2	K-2	K-2	K-2	K-2	K-2	
C	K-16	K-16	KD-6	K-16	KD-6	K-16	KD-6	KD-6	K-2
D	K-16	KD-6	KD-6	_		KD-6	KD-6		KD-6

## METAL-ENCLOSED BUS DUCT

I-T-E low-voltage metal-enclosed bus duct is available in continuous current ratings of 600A through 3000A at 600 volts. Standard construction includes silver-plated aluminum bus mounted on polyester-glass bus supports. Outdoor bus duct is weatherproofed and is provided with heaters to reduce condensation.

- Indoor or outdoor construction
- ☐ 3- or 4-wire
- s Polyester-glass bus supports
- a Silver-plated aluminum bus
- a Removable access cover



THERE SECTION

TABLE 33 - INDOOR-OUTDOOR 600-3000 Amperes

	7, 445,748 - 344,4	er er er er. Er er er er	Di	mension	S.			Current Rating, A	Housing Material	Removable Cover
Туре	W	A	В	, c.	ם	₩ <b>E</b>	F	600-2500	12 Ga. Steel	
3-Wire	22	6	5					3000*	12 Ga. Steet	500 : 500 !
4-Wire 50%-100% Neutral	27	_	_	6	5	5	6	600-2500 3000*	12 Ga. Steel	600-1600A 12 Ga. Steel
4-Wire Split Phase 50% Neutral	39		_	6	7	9	8	3000	11 Ga. Steel	2000-3000A ⅓″ Aluminum
4-Wire Split Phase 100% Neutral	43	_	_	8	9	9	8	3000	11 Ga. Steel	
3-Wire Split Phase	34	8	9	_	-	-	-	3000	11 Ga. Steel	1/8" Aluminum

<sup>\*</sup> Copper only

TABLE 33A—WEIGHTS

		MAGINET SERVICE	Weights	(lbs/3 Phase F	t)	
		Aluminum Bus			Copper Bus	
Capacity (Amps)	3-Wire	4-Wire 50% NEUT.	4-Wire 100% NEUT.	3-Wire	4-Wire 50% NEUT.	4-Wire 100% NEUT.
600 800 1000 1200 1600 2000 2500 3000	40 41 41 41 46 42 50 63	45 46 46 46 51 46 56 69	45 46 47 48 53 48 59 77	44 48 46 49 55 62 70 85	50 54 53 56 63 69 78 95	50 55 54 58 66 76 86 107

# SELECTION AND APPLICATION

# NOMING LINE SECTION

## AIR INTERRUPTER SWITCHES

TABLE 34 — AIR INTERRUPTER SWITCH RATINGS (Fused or Unfused)

TABLE 34	— All foltage R	100	ANOI 11 ANOI		Acceptance	ent Rating	<b>6</b>	Interru	nting Life ( Number	n Close-f of Interri	Open Duty options	Cycle	Fault Clo Spring	sing With Operator
Nominal kV	Max. Design	Withs 60 Cycle	Impulse	Con- tinuous Current,	At k¥	10 Cycle Momentary Rms Asym.	4 Sec. Short-Time Rms Sym. kA	At kY	Power Factor	200A	400A	600A	Unfused Rms Asym. kA	Fosad
		kŸ	kV 60	600	5.5	<b>AA</b>		5.5		1000	1000	750	40	Fuse Inter-
7.2/13.8	5.5 14.5	19 36	95	1200 600 1200	14.5	61	38	14.5	0.8	800	400	300		rupting Rating

35 - CL-14 CURRENT-LIMITING FUSE RATINGS, (50/60 Hertz) Non-Disconnect Type

Max. Design, kV	System, kV		eres Asym.	Nom. Equiv. 3-Phase MVA	Single Barrel	Double Barrel	Triple Barrel
5.5	2.4 4.16 4.8	60,000	96,000	250 430 500	10E Thru 400E	-	_
15.5	6.9 7.2 11.5 12.0 12.47 13.2 13.8 14.4	40,000	64,000	480 500 800 830 860 910 955	10E Thru 100E	125E	150E 200E

## TABLE 36 A - POWER FUSE SELECTION® \*

TABLE	36A - PU	AA ET	C FUS	JE GE			10 mg - 2/0 - 6 - 5			e xe e	****			, S4.9	1.2.2	o six		17	7	2	<b>黎</b> ·
ુ છેલું	malValge al		2.5.1					.16:32			7.7		442.4	95 (12) A	i mag Ngjeri	use Si		1113	F	use Siz	8
	nsformera	7		use Si		1. 40.	4, 22	use Siz		11	33.	133%   133%	Max	F.L		133%	Max	ři.	Min.	133%	Nax
SAYA®	Impedance@		Min	133%	Mac		Mine	100	Max	300	Min	100	30E	9	15E	15E	20E	9	15E	15E	20E
112.5	4.5	27	30E	40E	65E	16	20E	20E	30E	14	20E	20E		<u> </u>	-	20E	25E	12	15E	20E	25E
150	4.5	36	40E	50E	80E	21	25E	30E	40E	18	25E	25E	40E	12	15E				20E	25E	40E
225	4.5	54	65E	80E	100E	31	40E	40E	65E	27	30E	40E	50E	19	25E	25E	40E	18		┝──┤	50E
300	5.0	72	80E	100E	1258	42	50E	65E	80E	36	40E	50E	80E	25	30E	40E	50E	24	30E	40E	
<b>—</b>	5.0	120	150E	200E	200E	69	80E	100E	125E	60	65E	80E	100E	42	50E	65E	80E	40	50E	65E	80E
500	<del> </del>	<del>                                     </del>	200E	250E	300E	104	125E	150£	150E	90	100E	125E	150E	63	80E	100E	100E	60	80E	80E	100E
750	5.75	180	<del> </del>	<del> </del>	300E	139	200E	200E	200€	120	150E	-	150E	84	100E		100E	80	100E	<u> </u>	100E
1000	8.0	241	300E	<del> </del>	<del>} −</del>	╂	200E		250E	120	150E	200E	200E	84	100E	125E	150E	80	100E	125E	150E
1000	5.75	241	300E	<del> </del>	400E	1-	+	<del>                                     </del>	400E	├	200E	250E	300E	126	150E	200E	200E	120	150E	200E	200E
1500	5.75	361	400E	1=	<u> </u>	208	250E	<del> </del>		1-	300E	<del>                                     </del>	400E	1-	200E		200E	160	200E	200E	200E
2000	5.75	482	<u> </u>		<u> </u>	278	+	+	400E	╂	<del> </del>	<del> </del>	400E	╁┈╌	+	<del>                                     </del>	1_	201	1_	1_	[-]
2500	5.75	602	<u> </u>			348	4008		<u> </u>	300	<del> </del> -	400E	4000	251	+-	+=		241		_	1-1
3000	5.75	722	_	<u> </u>	<u></u>	416		二	上二	362	400E					the trai	nsforme		hown a	bove sh	ould be

Minimum fuse size shown will clear transformer magnetizing Inrush current. 155% fuse size permits overload operation of transformer up to 153% of rating. Maximum fuse size provides transformer fault protection for phase-phase. 3-phase and phase-ground faults on secondary windings of standard 3-phase transformers. Suffix E denotes NEMA standard fuse rated 30°C rise above 40°C average ambient.
When referring a CL-14 fuse as a replacement for a CL-13 it is important.

The self-cooled kVA rating of the transformer as shown above should be used in selection of fuse size on forced-air cooled transformer applications. Also, on such applications, the 133% fuse size must be chosen for proper coordination.
 Per cent impedance on self-cooled kVA base.

The above and average ambient.

\*When selecting a CL-14 fuse as a replacement for a CL-13, it is important to carefully check these selection tables. Although the CL-14 and CL-13 are physically interchangeable, several internal changes have resulted in either larger or smaller fuse "E" rating requirements at several kVA and voltage ratings.

#### TABLE 36B-POWER FUSE SELECTION® \* ·

							100	Ü.											7			10 A	ani.		
			estra v	40.2			ek f	se Si						60.		<b>4</b> 4 4 4 4	24 JEC				er e			ose S	
					4	9		18.4	- Selver	3.3	E. Same	J	******	in the second	4 700	A STORY	arene le co	5 v. 42	1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1	MATTER		15.072	-	Control of	15 E.
112.5	4.5	5.7	10E	10E	10E	5.4	10E	10E	10E	5.2	10E	10E	10E	4.9	10E	10E	10E	4.7	10E	10E	10£	4.5	10E	10E	10E
150	4.5	7.5	10E	10E	1 <b>5</b> E	7 :	10E	10E	15E	7	10E	10E	15E	6.6	10E	10E	15E	6.2	10E	10E	15E	6	10E	10E	10E
225	4.5	11.3	15£	15E	25E	10.8	15E	15E	20E	10.4	15E	15 <b>E</b>	20E	9.8	10E	158	20E	9.4	15E	15E	20E	9	15E	158	20E
300	5.0	15.1	20E	20E	30E	14.4	20€	20E	30E	14	15 <b>E</b>	20E	30E	13	15E	20E	30E	12.6	15E	20E	25E	12	15E	20E	25E
500	5.0	25.1	30E	40E	50E	24	30E	40E	50E	23	25E	30E	50E	22	25E	30E	50E	21	25€	30E	40E	20	25E	30E	40E
750	5.75	37.7	50E	50E	80E	36	40E	50E	80E	35	40E	50E	65E	33	40E	50E	65E	32	40E	50E	65E	30	40E	40E	65E
1000	8.0	50.3	65£	80£	80E	48	65E	65E	308	46	50E	65E	65E	44	50E	65E	65E	42	50E	65E	65E	40	50E	65E	65E
1000	5.75	50.3	65E	80E	100E	48	65E	65E	100E	46	50£	65E	80E	44	50E	65E	80E	42	50E	65E	80E	40	50E	65E	80E
1500	5.75	75.4	100E	100E	125E	72	30E	100E	125E	70	308	100E	125E	66	80E	100E	100E	63	80E	100E	100E	60	65E	80E	100E
2000	5.75	101	125E	150E	150E	96	125E	150E	150E	92	100E	125E	150E	88	100E	125E	150E	84	100E	125E	150E	80	100E	125E	150E
2500	5.75	126	125E	200E	2 <b>0</b> 0E	120	150E	200E	200E	116	150E	150E	200E	109	125E	150E	150E	105	125E	150E	150E	100	125E	150E	150E
3000	5.75	151	200E	200E	200E	144	200E	200E	200E	139	200E	200E	200E	131	150E	200E	200E	125	150E	200E	200E	120	150E	200E	200E

<sup>\* 123</sup> See notes at bottom of page 32.

#### **FUSE CURVES**

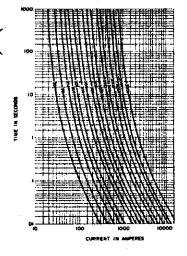


Figure 1—Minimum Melt Time-Current Characteristic Curves. For Type CL-14 Current-Limiting Fuse Units—Voltage Rating

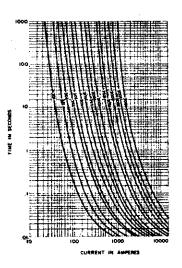


Figure 2—Total Clearing Time-Current Characteristic Curves. For Type CL-14 Current-Limiting Fuse Units—Voltage Rating 4.8KV.

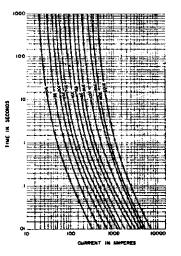


Figure 3—Minimum Melt Time-Current Characteristic Curves. For Type CL-14 Current-Limiting Fuse Units—Voltage Rating 14.4KV.

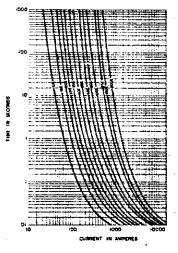


Figure 4—Total Clearing Time-Current Characteristic Curves. For Type CL-14 Current-Limiting Fuse Units—Voltage Rating 14.4KV.

## OIL CUTOUTS

#### TABLE 37 — FUSE INTERRUPTING RATINGS

	Fuse Inter	rupting Rating	kVA Li	mitations
Nominal Full Winding Voltage	Amperes (rms) Asymmetrical	Equivalent MVA Symmetrical	Fused	Unfused
2.4	10,000	42	500	750
4.16	10,000	72	750	1000
13.8	4,000	99	1000	2000

#### **METAL-CLAD SWITCHGEAR**

For application information, see I-T-E Bulletin 8.2-1

### LIQUID SWITCH

#### TABLE 38 — RATINGS

Voltage	Maximum Continuous	Interrupting Capacity, A			
Rating, kY	Gurrent Rating, A	Oil-filled	Askarel-filled		
5	400	400	0		
15	400	400	0		

When liquid switch is askarel-filled, it has no interrupting capacity. It can break magnetizing currents of up to 10A for five times without replacement.

# TRANSFORMER SECTION

TABLE 39 — STANDARD TRANSFORMER RATINGS

War - Order	Primary	W.	KAY	SECON	DARY	Standard	N E Sound L	N E M A Sound Level, db	
TYPE	Yoltaga Delta	3-Phase Self- Cooled	3-Phase Ferced-Air Coaled	208Y/120 240 delta	480Y/277 480 deita	impedance*	Self- Coaled	Forced- Air Cooled-	
Liquid- Immersed Oil or Askarel 65°C Rise †	2400 4160 4800 6900 7200 12000 12470 13200 13800	112½ 150 225 300 500 750 1000 1500 2000 2500		X X X X X	x x x x x x x	2.25‡ 3.0‡ 4.5 5.0 5.75 5.75 8.0 5.75 5.75 5.75	55 55 55 56 58 58 58 60 61 62	— — — — 67 67 67 67	
Ventilated- Dry 150°C Rise	2400 4160 4800 6900 7200 12000 12470 13200 13800	112½ 150 225 300 500 750 1000 1000 1500 2000 2500		X X X X X	x x x x x x x x x x	3.0‡ 3.5‡ 4.5 5.0 5.75 5.75 8.0 5.75 5.75 5.75	50 55 55 55 60 64 64 64 65 66 68		
Sealed-Dry Gas- Filled 150°C Rise	2400 4160 4800 6900 7200 12000 12470 13200 13800	300 500 750 1000 1000 1500 2000 2500		x x x	X X X X X X	5.0 5.0 5.75 5.75 8.0 5.75 5.75 5.75	57 59 63 63 63 64 65 66	-	

TABLE 40 ---LIGHTNING ARRESTERS

kV Rating of Arrester	Line to Line kV Ungrounded System	Line to Line kV Grounded System		
Sta	tion and Intermedi	ate Type ①		
3	2.4	4.16		
6	4.8	7.2		
9	7.2	12.47		
12	11.5	13.8		
15	13.8	18.0		
	Distribution Ty	pe ②③		
3	3.0	4.5		
6	6.0	9.0		
ğ	9.0	12.8		
12	12.0	15.0		
15	15.0	18.0		

- 1) For use with liquid-immersed transformers.
- 2 For use with sealed-dry transformers.
- 3 Distribution type arresters with special characteristics are furnished as standard on ventilated. dry transformers.

- Standard impedance tolerance is ±7½%.
   Average ambient temperature of 50°C.
   Transformers with impedances of 4.0% or less are designed to withstand 25 times normal current for two

#### TABLE 41 — TEMPERATURE GUARANTEES

Transformer Type	Ambient*	Rise†	Hot Spot Rise
Liquid-immersed	30°C 30°C	65°C 150°C 150°C	80°C 180°C 180°C

Altitudes must not exceed 1000 meters or 3300 feet.

- Aftitudes must not exceed took interes of 500 feets.

  The temperature of the cooling air (ambient temperature) must not exceed 40°C and the average temperature of the cooling air for any 24-hour period must not exceed 30°C.

  Degrees rise is the average winding temperature rise by resistance. See NEMA Standard TR-i and ANS C57.12.00.

TABLE 42 - DIELECTRIC TESTS

Trans- former Type	Voltage Class, kV	Applied Test 60 Cycle All kVA Ratings	Basic Impulse Levels 1.2 x 50 ms	induced Test 7200 Cycles, All kVA Ratings
Liquid- Immersed or Sealed- Dry	1.2 2.5 5.0 8.66 15.0	10 kV 15 kV 19 kV 26 kV 34 kV	30 kV 45 kV 60 kV 75 kV 95 kV	Twice normal voltage
Ventilated- Dry	1.2 2.5 5.0 8.66 15.0	4 kV 10 kV 12 kV 19 kV 31 kV	10 kV 20 kV 25 kV 35 kV 50 kV	Twice normal voltage

TABLE 43 --- STANDARD HIGH-VOLTAGE TAPS

Rated Voltage		Rated kVA HV Taps, Volts				
2400	2520	2460	2340	2280		
4160	4360	4260	4055	3950		
4800	5040	4920	4680	4560		
6900	7245	7070	6730	6555		
7200	7560	7380	7020	6840		
12000	12600	12300	11700	11400		
12470	13095	12780	12160	11845		
13200	13860	13530	12870	12540		
13800	14400	14100	13500	13200		

# OUTGOING SECTION—K-LINE\* CIRCUIT BREAKERS

## TABLE 44 - K-LINE CIRCUIT BREAKER RATINGS

18 4 C	ind (1 P	1000 A	Symme	rical Control	Sym- metrical
			interru Rating	pting	Close and Latch & 30-Cycle Short-
Circuit Breaker Type	A-C Volts	Frame Size, A	Instan- taneous Trip, A	Delayed Trip, A	Time Rating, A
K-225 K-600 K-1600 K-2000 K-3000 K-4000	208 and 240	225 600 1,600 2,000 3,000 4,000	25,000 42,000 65,000 85,000 85,000 130,000	14,000 22,000 50,000 55,000 65,000 85,000	14,000 22,000 50,000 55,000 65,000 85,000
K-225 K-600 K-1600 K-2000 K-3000 K-4000	480	225 600 1,600 2,000 3,000 4,000	22,000 30,000 50,000 65,000 65,000 85,000	14,000 22,000 50,000 55,000 65,000 85,000	14,000 22,000 50,000 55,000 65,000 85,000
K-225 K-600 K-1600 K-2000 K-3000 K-4000	600	225 600 1,600 2,000 3,000 4,000	14,000 22,000 42,000 55,000 65,000 85,000	14,000 22,000 42,000 55,000 65,000 85,000	14,000 22,000 42,000 55,000 65,000 85,000

Recommended maximum continuous current rating of largest feeder breaker in per cent of transformer (self-cooled) rated current, when primary power fuses are included is 40% for current-limiting type and 50% for non-current-limiting type.

TABLE 45 - K-LINE S CIRCUIT BREAKER RATINGS

			Symme Interru Rating	Sym- metrical Close and Latch & 30-Cycle	
© Circuit Breaker Type	A-C Volts	Frame Size, A	Instan- taneous Trip, A	Delayed Trip, A	Short- Time Rating, A
K-600S K-1600S K-2000S K-3000S K-4000S	208 and 240	600 1,600 2,000 3,000 4,000	42,000 65,000 85,000 85,000 130,000	22,000 50,000 55,000 65,000 85,000	22,000 50,000 55,000 65,000 85,000
K-600S K-1600S K-2000S K-3000S K-4000S	480	600 1,600 2,000 3,000 4,000	30,000 50,000 65,000 65,000 85,000	22,000 50,000 55,000 65,000 85,000	22,000 50,000 55,000 65,000 85,000
K-600S K-1600S K-2000S K-3000S K-4000S	600	600 1,600 2,000 3,000 4,000	22,000 42,000 55,000 65,000 85,000	22,000 42,000 55,000 65,000 85,000	22,000 42,000 55,000 65,000 85,000

Recommended maximum continuous current rating of largest feeder breaker in per cent of transformer (self-cooled) rated current, when primary power fuses are included is 40% for current-limiting type and 50% for non-current-limiting type.

TABLE 46—CIRCUIT BREAKER CONTROL-POWER REQUIREMENTS

			Average Shunt- Closing-Motor Trip Current		Relay nt, A	Closing-Circuit Voltage	Jrip-Circuit Voltage	Recommended Control Circuit
Breaker Type	Yoltage :	Current, A	A FOA	Anti-Pump	Release	Range, Volts	Range, Velts	Fuse Size, A
K-225 K-600, S K-1600, S K-2000, S K-DON-600, S K-DON-1600, S	120 V ac 240 V ac 48 V dc 125 V dc 250 V dc	10 5 25 10 5	6.5 1.15 3.14 1.3 .65	.15 .075 .11 .06 .03	1.5 .75 1.33 .7 .3	104-127 208-254 38-56 100-140 200-280	50-127 208-254 28-56 70-140 140-280	10 10 15 10 10
K-3000, S and K-4000, S	120 V ac 240 V ac 48 V dc 125 V dc 250 V dc	10 5 25 10 5	10.0 1.84 5.0 2.0 1.0	.15 .075 .11 .06 .03	4.0 1.84 5.0 2.0 1.0	104-127 208-254 38-56 100-140 200-280	50-127 208-254 28-56 70-140 140-280	10 10 15 10 10

## TABLE 47—UNDERVOLTAGE TRIP DEVICE

Nominal Control	Current at	Minimum Pick-up	Dropout Voitage Value, Voits		
Voltage	Rated Volts, A	Voltage Value, Volts	Minimum	Maximum	
120 V ac	0.50	102	36	72	
240 V ac	0.20	204	72	144	
480 V ac	0.10	408	144	288	
48 V dc	0.32	41	15	29	
125 V dc	0.20	106	38	75	
250 V dc	0.10	212	75	150	

# SELECTION OF LOW-VOLTAGE POWER CIRCUIT BREAKERS IN LOW-VOLTAGE DRAWOUT SWITCHGEART

SELECTION OF BREAKER TRIPPING

CHARACTERISTICS

The degree of service continuity available from a lowvoltage distribution system depends on the degree of coordination between circuit-breaker tripping characteristics.

Three methods of tripping coordination are in general use, each representing a different degree of service continuity and

These methods, or systems, combine breaker ratings and tripping characteristics as follows:

FULLY-RATED SYSTEM

A fully-rated system is one in which both the main and feeder breakers have adequate interrupting capacity for the fault current available at the point of application.

All breakers are equipped with long-time delay and instantaneous overcurrent trips. Ordinarily only the breaker nearest the fault will open. The main breaker will trip, however, when the fault current exceeds its instantaneous trip setting, and service continuity may be lost.

CASCADED SYSTEM

A cascaded system is one in which only the main breaker has adequate interrupting capacity. Not recommended.

SELECTIVE SYSTEM

A selective system is one in which both the main and feeder breakers have adequate interrupting capacity for the fault current available at the point of application.

## USE OF APPLICATION TABLES

Application Tables 48A and 48B provide for proper selection of the circuitbreaker type required. They should be used as follows:

Use Table 48A for a fully-rated system

Use Table 48B for a selective system Having chosen the right table, refer to that part of it which covers the

system voltage.

TABLE 48A—FULLY RATED SYSTEM (Electro-Mechanical Trip Device Only)

Manually-charged, stored-energy-closed circuit breakers may be applied within their 600 v, 480 v, or 240 v interrupting rating, provided their instantaneous trips are set below their short-time ratings. Note: For solid-state trip devices any available amp tap may be used regardless of voltage within the short-circuit current rating of the circuit breaker. breaker.

TABLE 48B—SELECTIVE SYSTEM (Electro-Mechanical Trip Device Only)

The manually-charged, stored-energy-closed circuit breakers with delayed trip may be applied within their shorttime ratings. Note: For solid-state trip devices any available amp tap may be used re-gardless of voltage within the short circuit current rating of the circuit

The main breaker is equipped with overcurrent trip devices having long-time delay and short-time delay functions. The feeder breakers are equipped with overcurrent trip devices having long-time delay and instantaneous functions unless they are required to be selective with other protective devices nearer the load. In this case, the feeders are equipped with trip devices having both long-time and short-time delay.

In a selective system, only the breaker nearest the fault trips. Service continuity is thus maintained through all other

breakers.

The main breaker trips only on a bus fault.

The selective system offers a maximum of service continuity, with a slightly higher initial cost than the fully-rated or cascaded systems.

SELECTION OF BREAKER TYPE

The following three basic factors determine the selection of a breaker after a decision has been reached on the type of system required:

System voltage and frequency

Continuous current

Available fault current

Selection and application information is for low-voltage power circuit breakers equipped with OD direct-acting, electro-mechanical overcurrent trip devices. In general, however, these application rules apply to breakers with POWER-SHIELD solid-state overcurrent trip devices except for differences in available ampere taps and long-time, short-time and instantaneous nick-up settings. pick-up settings.

Look for the horizontal line listing an available fault current nearest the one required at the point of application (let the nearest one be higher, rather than lower than the exact fault current needed) .

Then select the circuit-breaker type listed where the Available Fault Current line crosses the vertical column headed with the wording: Load Continuous

Current Rating.

Available

Fault Current,

Symmetrical

**RMS Amperes** 

System Voltage

and

Frequency

**Load Continuous Current Rating** 

501 to 630V 25-60 Hertz	14000 22000 42000 55000 65000 85000		225		K-600	K-1600	ㄷ	2005	
251 to 500V 50-60	22000 30000 50000 65000		.225 L		K-600	K-1600	1		×.4000
Up to 250V 50-60 Hertz	25000 25000 42000 65000 85000		(-225		K-600	X-160C	K 2000	K.3000	× 4000
System Voltage and Frequency	Available Fault Current, Symmetrical RMS Amperes	Short- Time Delay Band	15 35 15 25		Soutinuous Cri		7 2 2 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3		
	14000	Minimum Intermediate Maximum	T	K-225	K-600	K-1600	K-2000	K.3000	K-4000 K-4000 K-4000
	22000	Minimum Intermediate Maximum	. '		K-600	K-1600	K-2000	K-3000 K-3000	\$ ×
Up to	42000*	Minimum Intermediate				K-1600	K-2000	K-3000	8
600V 50-60 Hertz	55000	Maximum Minimum Intermediate		<del></del>		K-2000		к-3000	K-4000
	65000	Maximum Minimum Intermediate Maximum					K.	3000	4-1000
	85000	Minimum Intermediate Maximum	- Target			. a	· ·		K-4000

## K-DON® CIRCUIT BREAKERS

#### .sle 49 - K-DON BREAKER RATINGS

Circuit Breaker Type	rrame Sze, A	Yoltage A C	Maximum Continuous Current, A	Maximum Interrupting Symmetrical Rating Rms Amperes	Range of Circuit Breaker Pickup, A	Amp-trap Centinuous Rating, A
K-DON-600	600	up to 600	600	200,000	40-600	300-1200
K-DON-1600	1600	up to 600	1600	200,000	120-1600	300-2500
K-DON-600S	600	up to 600	600	200,000	40-600	300-1200
K-DON-1600S	1600	up to 600	1600	200,000	200-1600	600-2500

The following step by step procedure is to be used as a guide for proper circuit breaker and fuse selection.

#### A. CIRCUIT-BREAKER SELECTION

- 1—Determine the system short-circuit capacity in symmetrical rms amperes.
- 2—Determine from Table 50 columns 3, 4 and 5 respectively the approximate continuous current rating and the time-delay and instantaneous overcurrent trip settings.
- 3—Select from Tables 51 or 52, columns 1, 2, 3 and 4 respectively the frame size, proper coil rating, time-delay and instantaneous settings as follows:

- (a) When there is a choice of breaker frame size the larger will provide maximum flexibility in case of load growth.
- (b) The coil rating should be equal to or greater than the value determined in Table 50, column 3.
- (c) Time-delay setting should be set at a value nearest to that determined in Table 50, column 4.
- (d) Instantaneous setting should be set at a value nearest to that determined in Table 50, column 5. However, this value may have to be adjusted downward to coordinate with Amp-trap to be selected in step B.

#### TABLE 50 — CIRCUIT-BREAKER APPLICATION

50	1 8	2	\$ 18 18 18 18 18 18 18 18 18 18 18 18 18	4 4	5
	Type of application	Purpose of Circuit Breaker	Continuous Gurrent Rating of		ngs of Trip Device
	ippiivation		Circuit Breaker	Time Delay	Instantaneous
	Service entrance (general)	<ul> <li>(a) To protect source transformer windings from overheating, due to overload of fault current flow.</li> <li>(b) To protect circuit conductors from effects of overcurrent flow.</li> <li>(c) To provide safe and rapid means for connecting and disconnecting of load circuit.</li> </ul>	Based upon 125% of the transformer current rating	125% of the transformer current rating	1000% of circuit-breaker current rating
	Service feeder (general)	(a) To protect circuit conductors from effects of overcurrent flow.     (b) To protect connected electrical equipment from effects of fault current flow.	Based upon 115% of estimated load current	115% of estimated load current	1000% of circuit-breaker current rating
G	Individual motor circuit	(a) To protect motor windings from overheating due to overcurrent or fault current flow.     (b) To protect circuit conductors and other connected electrical equipment from overload or fault current flow.     (c) To provide safe and rapid means of connecting and disconnecting motor circuit.	Based upon 115% of rated full- load current of motor	115% of rated full- load current of motor	1000% of circuit-breaker current rating
JITS (GENERAL)	Group motor circuit	(a) To protect circuit conductors from overheating.     (b) To protect circuit conductors, motor windings and other connected electrical equipment from fault current flow.     (c) To provide safe and rapid means of connecting and disconnecting common motor circuit from supply source.	Based upon 115% of largest motor full-load current plus sum of other motor currents	100% of circuit-breaker current rating	1000% of circuit-breaker current rating
ARANCH CIRCUITS	Combined motor and lighting circuit	(a) To protect circuit conductors from overheating. (b) To protect circuit conductors, motor windings and other connected electrical equipment from fault current flow. (c) To provide safe and rapid means of connecting and disconnecting common load circuit from supply source.	Based upon 115% of largest motor full-load current plus sum of other motor and lighting load currents	100% of circuit-breaker current rating	1000% of circuit-breaker current rating
	Lighting circuit	(a) To protect circuit conductors from effects of overload or fault current flow.  (b) To provide safe and rapid means of connecting and disconnecting lighting circuit from supply source.	Based upon 125% of estimated maximum lighting current	100% of circuit-breaker current rating	1000% of circuit-breaker current rating

<sup>\*</sup>Table 51 is to be used for K-DON breakers with electro-mechanical overcurrent trip devices; Table 52 is for K-DON breakers with solid-state overcurrent trip device.

<sup>†</sup>Registered Trademark-Chase-Shawmut Co.

## K-DON® CIRCUIT BREAKERS

### 8. AMP-TRAPT SELECTION

Table 51 or 52 is to be used for selecting the correct fuse sizes to coordinate with the instantaneous setting of the overload device to provide proper coordination between the circuit breaker and fuse. It was developed to provide the greatest range of coordination possible, taking advantage of maximum fuse sizes whose let-thru current can be withstood by the circuit breaker.

Figure 6, Page 41, is a second aid in the selection of the proper Amp-Trap fuse sizes. However, Fig. 6 is not to be used as the only criterion if, as in the case of molded-case circuit breakers, there is an 12t limitation in the equipment to be protected by the fuse (See Figure 7).

There are two basic considerations in selecting an Amp-Trap fuse size.

- 1-The peak let-thru current must not exceed 2.3 times the symmetrical short-circuit withstand of the equipment to be protected by the K-DON circuit breaker.
  - a. If the equipment protected by the circuit breaker has a symmetrical short-circuit withstand rating at least equal to that of the circuit breaker,\* fuse size selection may be made by using Table 51 or 52.
  - b. If the equipment protected by the circuit breaker has a symmetrical short-circuit withstand rating less than the circuit breaker, Fig. 6 must be used to determine the maximum fuse size.

Draw a vertical line on Fig. 6 representing the available symmetrical RMS amperes. Establish the intersection of this line with the peak amperes that the equipment is capable of withstanding. The fuse size represented by the fuse let-thru curve passing below this intersection is the maximum fuse size that should be used. Of course, the smallest fuse size, consistent with coordination, provides the best protection.

2-The second consideration is that the fuse size coordinates with the circuit-breaker overload time-current characteristic. Proper application of Table 51 or 52 and their associated notes will assure coordination and, therefore, avoid needless fuse replacements for current levels within the interrupting rating of the breaker.

For application using special instantaneous settings, a breaker-fuse coordination curve should be drawn.

Fuse curves are normally plotted with time as the ordinate and current in amperes as the abscissa. However, the abscissa of the overcurrent device time-current curves is the ratio of actual current to current tap or to coil rating or to pickup setting. There are so many combinations of settings as to render it completely impractical to publish general coordination curves for fuses and overcurrent trip

When it is desired to plot specific coordination curves, the following procedure is suggested.

Replot the overcurrent device curve using actual amperes as the abscissa based on pick-up settings selected. The curves may be moved right or left to accommodate settings not plotted on published curves. A transparent overlay is helpful in this procedure.

- b. Enter the fuse melting time-current curve from Figure 7. Page 41, on this newly plotted overcurrent device curve and examine for proper coordination.
- c. When fuse size is dictated by protection needs, the fuse curve should be plotted first and the overcurrent device settings are then determined by trial and error, by replotting the overcurrent device curves.

Maximum allowable fuse sizes listed in Tables 51 or 52 are based on an available RMS symmetrical short-circuit current of 200kA. If available current is less than 200kA larger fuse sizes may be used based on let-thru of Figure 6 as illustrated in the following table. Note that this does not apply to K-DON breakers equipped with solid-state trip.

Frame Size	600	600	1600
Avail. kA	130	85	100
Max. Fuse Size, Amps.	1600	2000	3000

- When fused circuit breakers are used on high-inrush circuits such as motor starting, for extended periods, the maximum allowable fuse size from Tables 51 or 52 should be used regardless of instantaneous setting. Otherwise these fuses and other unblown fuses, after a short-circuit, may have melting times less than "when new". In this case, fuse replacement should be considered if the coordination is critical.
- C. APPLYING LOW-VOLTAGE POWER CIRCUIT BREAKERS WITH SEPARATELY MOUNTED CUR-RENT LIMITING FUSES

(Note that this applies to the K-2000, K-3000 and K-4000 only. Lower rated breakers (not K-225) will be coordinated in the same manner as the K-DON breakers in Tables 51 or

The interrupting capability of the proper combination of low-voltage power circuit breakers and current-limiting fuses is appreciably higher than the capability of the circuit breaker alone. The following guidelines are offered for combining Chase-Shawmut Amp-Trap current-limiting fuses, NEMA Class L, with modern I-T-E low-voltage power circuit breakers:

- 1-Avoid or at least minimize overlap of time-current characteristics (fuse vs. overcurrent device) at currents less than the circuit-breaker interrupting rating to keep needless fuse blowing to a minimum. Adding a short-time element often helps to obtain coordination.
- 2-The total clearing time of the fuse must be equal to or less than the total clearing time of the circuit breaker at a current equal to the interrupting rating of the circuit breaker at the voltage of the application.
- 3—The peak let-through current of the fuse must not exceed 2.3 times the withstand rating of the circuit breaker.
- 4—The fuses should preferably be on the source side of the circuit breaker. When this is not possible, the two should be located as close as practical to each other, and the installation should minimize the exposure to a fault between the breaker and the fuse.

In order to obtain selective protection when fuses are applied in series, it is necessary that the fuse nearer the source have a current rating at least two times that of the fuse nearer the load, providing that both fuses are Chases Shawmut Class L. The two-times ratio is applied to fuse ratings up to 2000As; but for fuse ratings of 2500A to 6000A the ratio may be reduced to 1½ times.

† Registered Trademark-Chase Shawmut Co.

K-2000 — 85,000A, Sym. K-3000 — 130,000A, Sym.

K-4000 - 130,000A, Sym.

<sup>\*</sup> K-DON-600, 42,000A Sym; K-DON-1600, 65,000A Sym.

TABLE 51 -K-DON COORDINATION (ELECTRO-MECHANICAL OD-3) K-DON COORDINATION (SOLID-STATE SS-3)

Instan-taneous Coordinating
Fuse Size, A
(See Note 1) Long-Time Pickup Breaker Circuit Coil 🗈 Pickup. Breaker Rating, Settings, Settings,@ Type A A in . Min. Max. 40, 50, 60, 70 or 90 70, 90, 100, 125 or 160 K-DON-600 120, 150, 175, 200, 225 or 285 250, 300, 350, 400 or 500 See Note 2 400, 500, 600 or 750\* See Note 2 See Note 2 120, 150, 175, 200, 225 or 285 250, 300, 350, 400 or 500 K-DON-1600 400, 500, 600, 800 or 1000 See Note 2 800, 1000, 1200, 1600 or 2000\* See Note 2 See Note 2

#### NOTES TO TABLES 51 AND 52:

TABLE 52 ---

Circuit Breaker Type		Breaker AMPERE TAP Settings, A	Long-Time Pickup Settings, CX Ampere Tap) A	Instantaneous Pickup Settings, (X Ampere Tap) A	Coordin Fuse Si (See Notes Mia.	ze, A
1		2	3	4	5	1
	ш	50, 70, 100	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, 10 or 12	300	1200
	SENSOR RANGE	150	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, 10 or 12	300 400	1200 1200
-6008	SEN	225	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, 10 or 12	400 600	1200 1200
K-DON-600S	ш	250	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, 10 or 12	600 800	1200 1200
: :	SENSOR RANGE	400	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, 10 or 12	800 1000	1200 1200
	SEN	600	0.7, 0.8, 0.9, 1.0, 1.1†	4, 5, 6, 8, 10 or 12	1200 See N	1200 lote 2
	ш	250	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, e10 or 12	600 800	2500 2500
	OR RANGE	400	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, 10 or 12	800 1000	2500 2500
16008	SENSOR	600	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, 10 or 12	1200 1600	2500 2500
K-DON-1600S	NGE	600	0.7, 0.8, 0.9, 1.0, 1.1	4, 5, 6, 8, 10 or 12	1200 1600	2500 2500
	SENSOR RAN	1000	0.7, 0.8, 0.9,	4, 5, 6, 8, 10 or 12	2000 2500	2500 2500
ŀ	SEN	1600	0.7, 0.8, 0.9, 1.0, 1.1†	4, 5, 6, 8, 10 or 12	2500 See 1	2500 Note 2

<sup>†</sup> Setting above maximum ampere tap rating and breaker frame size is available for coordination, if needed, but is not thermally self-protecting.

- When the selected settings and indicated fuse size will not coordinate, the following applies:
  - a. Determine the degree of overlap by drawing a breaker-fuse coordination curve.

  - b. If the degree of overlap is not deemed critical (low probability of needless fuse blowing), accept the overlap.

    c. If the degree of overlap is deemed critical, utilize a short-time delay element in conjunction with the long-time and instantaneous elements to achieve coordination.
- For the solid-state device the coordinating fuse size is based on the ampere-tap setting. If a higher tap setting is planned for future load growth, the maximum fuse size for the sensor range should be used to maintain proper coordination.

Setting above maximum breaker frame size is available for coordination, if needed, but is not thermally self-protecting.

The minimum fuse size column indicates the minimum fuse size that will coordinate with the instantaneous trip setting directly along side it at the 100% long-time pickup setting. Even though a lower fuse size might appear to coordinate by use of minimum or intermediate time bands or lower instantaneous setting or lower long-time pickup setting, a fuse size lower than listed is not recommended.

The maximum fuse for the frame size will not coordinate with the instantaneous trip setting listed. (See Note 4.)

The instantaneous setting selected should not be less than five nor more than fifteen times the long-time pickup setting selected.

## SELECTION AND APPLICATION

Tables 53 and 54 can be used along with the notes of Table 51 and 52 to assure coordination. Table 53 is to be used when applying separately fused circuit breakers with electro-mechanical overcurrent trips.

TABLE 53—
COORDINATION OF SEPARATELY MOUNTED FUSES AND BREAKERS (Electro-Mechanical)

Circuit Breaker Type	Breaker Coil Rating, A	Long-Time Pickup Settings, A	Instantaneous Pickup Settings, A	Coordinating Fuse Size (See Table 51, Note 1) Min. Max.
K-2000	2000	1200, 1600, 1800, 2000 or 2500*	10,000 15,000 20,000 30,000	3000 3000 See Note A See Note A See Note A
K-3000	3000	1600, 2000, 2500, 3000 or 3800*	10,000 20,000 28,000 36,000	4000 6000 6000 6000 See Table 51, Note 2 See Table 51, Note 2
K-4000	4000	2000, 3000, 3500, 4000 or 5000*	20,000 30,000 40,000 48,000	6000 6000 See Table 51, Note 2 See Table 51, Note 2 See Table 51, Note 2

Setting above coll rating is available for coordination, if needed, but is not thermally self protecting.

Table 54 is for separately fused circuit breakers with solid-state overcurrent trip devices.

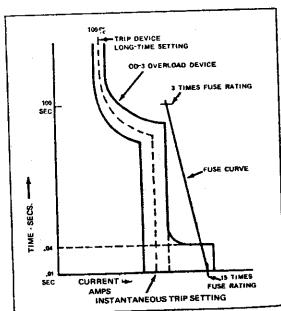
TABLE 54—
COORDINATION OF SEPARATELY MOUNTED FUSES AND
BREAKERS (Solid-State)

Circuit Breaker Type		Breaker AMP- ERE TAP Set. A	Long-Time Pickup Settings, (X Ampere Tap) A	Instantaneous Pickup Settings, (X Ampere Tap) A	Coordinating Fuse Size (See Table 51, Note 1) Min. Max.
K-2000S	GE	800 1200 2000 2000	0.7, 0.8, 0.9, 1.0, 1.1†	4, 5, 6, 8, 10, 12 4, 5, 6, 8, 10, 12 4, 5, 6 8, 10, 12	2000 3000 3000 3000 3000 3000 See Note A
K-3000S	1	2000 3000 3000	0.7, 0.8, 0.9, 1.0, 1.1†	4, 5, 6, 8, 10, 12 4, 5, 6, 8 10, 12	5000 6000 6000 6000 See Table 51, Note 2
K-4000S	SENSOR	3000 3000 4000 4000	0.7, 0.8, 0.9, 1.0, 1.1†	1	6000 6000 See Table 51, Note 6 6000 6000 See Table 51, Note 6

<sup>†</sup> Setting above maximum ampere-tap rating is available for coordination, if needed, but is not thermally self protecting.

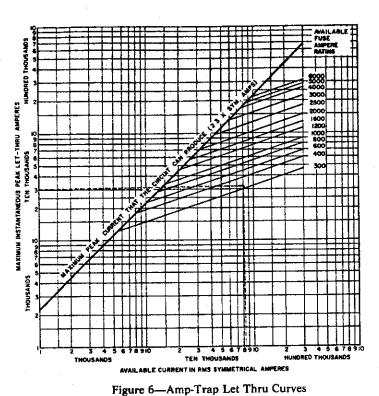
To illustrate the use of Fig. 6—Amp Trap Let-Thru Curves, assume a fault current of 80,000 Amp symmetrical using a 300 Amp current-limiting fuse. Enter table at 80,000 Amp sym. and project to the intersection of this line with the curve for the 300 Amp fuse; then project this point horizontally to a value of 30,000 peak let-thru amp. To obtain the fault current let-thru amp sym., divide the peak let-thru value by 2.3.

$$\frac{30,000}{23}$$
 = 13043 Amp sym.



T I Brooker Amp Trai

A. Maximum fuse sizes listed are based on an available RMS symmetrical short-circuit. current of 200kA. However, if the available current is only 115kA, a 4000A fuse may be used with the K-2000S breaker frame size for coordination with a higher instantaneous setting.



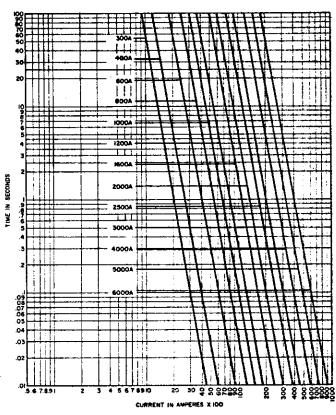


Figure 7-Melting Time-Current Characteristic Curves

TABLE 55— PROTECTION OF MOLDED-CASE CIRCUIT BREAKERS IN SWITCHGEAR, MOTOR CONTROL CENTERS AND PANELBOARDS\*

Molded Case Circuit Breaker		K-001	K-DON-600		H1600	
Туре	Trip Rating, A	Maximum Coll Rating, A	Maximum Amp-Trap Rating, A	Maximum Coil Rating, A	Maximum Amp-Trap Rating, A	
EF	15-100	225	300	1	-	
	70-150	400	400		_	
FJ	175-225	400	400	400	400	
	70-125				1000	
JL	150-225	600	1000	<b>8</b> 0 <b>0</b>		
	250-400	_				
****	250-275	600	1000	800	1000	
KM	300-800	_		800	1000	
	15-50	500	900			
HE	70-100	600	800	800	800	
	125					
HJ	150-175	600	1200	800	1200	
	225-400	Ī .	l	<u> </u>		
НМ	400-800	_		800	1200	

TABLE 56—PROTECTION OF LOW-IMPEDANCE BUS DUCT SYSTEMS\*

Bus Duct	K DO	H-600	K-DON-1	600
Ampere Rating	Maximum Coil Rating, A	Maximum Amp-Trap Rating, A	Maximum Coil Rating, A	Maximum Amp-Trap Rating, A
		Plug-In Type		
225	400	300		
400	600	1200		-
600	600	2500	800	2500
800	_	_	1600	2500
1000			1600	2500
1200			1600	2500
1350			1600	2500
1600	_	T -	1600	2500
		Feeder-Type		
800	_		1600	2500
1000			1600	2500
1200			1600	2500
1350		T -	1600	2500
1600	_	T	1600	2500

<sup>\*</sup>Based on available short-circuit current of 100,000 amperes at 480 volts. For available fault currents above 100,000 amperes symmetrical, consult I-T-E district sales office.

# OD—ELECTRO-MECHANICAL OVERCURRENT TRIP DEVICE

GENERAL-PURPOSE, DUAL-MAGNETIC DIRECT-ACTING OVERCURRENT TRIP DEVICE (OD-3 AND OD-300)

This device combines long-time delay (50-125% of coil rating) and instantaneous (500-1500% of coil rating). It can be used in almost any feeder application including welding and motor circuits.

## DUAL-SELECTIVE, DIRECT-ACTING OVERCUR-RENT TRIP DEVICE (OD-4 AND OD-400)

This device combines long-time delay (80-160% of coil rating) and short-time delay (400-1000% of coil rating). Its prime application is for use on selective-tripping systems where service continuity is of major significance.

SPECIALIZED-SELECTIVE AND GENERAL-PUR-POSE, DUAL-MAGNETIC DIRECT-ACTING OVER-CURRENT TRIP DEVICES (OD-5, OD-500, OD-6 AND OD-600)

The OD-5 and OD-500 combine long-time delay (80 to 160% of coil rating), short-time delay (400-1000% of coil rating) and instantaneous (500-1500% of coil rating). The OD-5 and 500 is a modified selective device. The addition of the instantaneous trip allows it to be applied above the shorttime rating while sacrificing only a minor degree of selectivity.

The OD-6 and OD-600 are similar to the OD-3 and OD-300 general-purpose devices except for the more limited range of the long-time pickup.

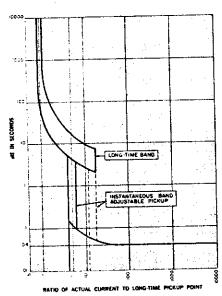


Figure 8—General Purpose Types OD-3 and OD-300

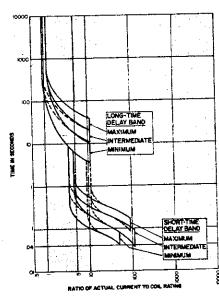


Figure 9-Dual Selective Types OD4 and OD400

4.000

K-3000

K-4000

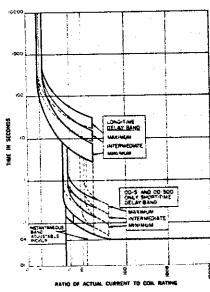


Figure 10-Specialized Selective Types OD-5, 500 and OD-6, 600

4000

4000

**Direct-Acting Trip Devices** 

#### Note: Each individual OD device operates within ±10% of its pickup setting. This narrow ±10% band will always fall within the wider bands shown in Figures 8, 9,

and 10.

			:			Ratings with	
			Maxi		De	layed Trip (00-4	)
Circuit Breaker A-C	A-C Volts	Frame Size, A	mum Coil Rating, A	Inst. Trip, A (OD-3)	Mini- mum Band, A	Inter- mediate Band, A	Maxi- mum Band, A
K-225 K-600 K-1600 K-2000 K-3000 K-4000	208 and 240	225 600 1,600 2,000 3,000 4,000	225 600 1,600 2,000 3,000 4,000	40 225 400 800 3000 4000	90 150 300 300 3000 4000	90 150 300 300 3000 4000	150 250 500 500 3000 4000
K-225 K-600 K-1600 K-2000 K-3000 K-4000	480	225 600 1,600 2,000 3,000 4,000	225 600 1,600 2,000 3,000 4,000	20 125 400 400 3000 4000	90 150 300 300 3000 4000	90 150 300 300 3000 4000	150 250 500 500 3000 4000
K-225 K-600 K-1600 K-2000 K-3000	600	225 600 1,600 2,000 3,000	225 600 1,600 2,000 3,000	20 40 225 400 3000	90 150 300 300 300	90 150 300 300 3000	250 250 500 500 3000

ፈርርር

4,000

TABLE 57 — OD ELECTRO-MECHANICAL APPLICATION PARAMETERS

TABLE 58 -DUAL-MAGNETIC, DUAL-SELECTIVE AND INSTAN-TANEOUS ELECTRO-MECHANICAL OVERCURRENT-TRIP-DEVICE CHARACTERISTICS

Circuit	Trip	Characteristic		
Breaker Type	Device Type	Long-Time	Short-Time *	Instantaneous
	OD-3	50-125%		500-1500%
	OD-4	80-160%	400-1000%	
K-225 K-600	OD-5	80-160%	400-1000%	500-1500%
K-1600	OD-6	80-160%		500-1500%
K-2000	OD-7			500-1500%
	OD-8			80-250%
	OD-300	50-125%		500-1200%
	OD-400	80-160%	400-1000%	
к-3000	OD-500	80-160%	400-1000%	500-1200%
K-4000	OD-600	80-160%		500-1200%
	OD-700			500-1200%
	OD-800			80-250%

<sup>\*</sup> Special 200-500% short-time pick-up settings for specialized coordination applications are also available.

**CABLE 60 ---**TYPES OD-4, 400 THRU OD-8, 800 COIL RATINGS

Circuit Breaker Type	OD-4,400 ○ Coil Ratings, 3 A	Circuit Breaker Type	OD-5,500, 6,600, 7,700 and 8,800 Coil Ratings, A®
K-225	90 100	K-225	15 20
K-225	125		30 40
K-225 K-600	150 175 200 225	K-225 K-600	50 70 90 100 125
K-600	250	K-225 K-600	150 175
W 600	300 350 400	K-1600	200 225
K-600 K-1600		1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	K-600-1600
K-2000	450 500 600	K-600 K-1600	300 350 400
K-1600 K-2000	800 1000 1200	K-2000	450 500 600
K-2000	1600 2000	K-1600 K-2000	800 1000 1200
<del></del>	0500 -	14 0000	1600
K-3000	2500 ° 3000	K-2000	2000 2500
K 4000		K-3000	3000
K-4000	4000	K-4000	4000

<sup>©</sup> Refer to Table 57 for application parameters.

© Refer to I-T-E district sales office for application parameters.

\* Adjustable down to 1600A

Adjustable down to 1600A.

TABLE 59 -TYPE OD-3 AND OD-300 DUAL-MAGNETIC ELECTRO-MECHANICAL OVERCURRENT-TRIP-DEVICE PICK-UP

Circuit Breaker	Maximum () Continuous	Adjustable Long-Time Delay Pickup Points, A	Adjustable Instantaneous
ж Тур <del>о</del>	Coil Rating, A	Pickup Points, A	Pickup Points, J
K-225	20	12 15 18 20 25	75 125 200 300
K-225 K-600	40	20 25 30 40 50	150 250 400 600
K-225 K-600	70	40 50 60 70 90	250 500 750 1100
K-225 K-600	125	70 90 100 125 160	450 800 1200 1900
K-225 K-600 K-1600	225	120 150 175 200 225 285	750 1500 2400 3400
K-600 K-1600 K-2000	400	250 300 350 400 500	1250 2000 4000 6000
K-600	600	400 500 600 750*	2500 4000 6000 9000
K-1600 K-2000	800	400 500 600 800 1000	2500 5000 8000 12000
K-1600 K-2000	1600	800 1000 1200 1600 2000*	5000 10000 16000 24000
K-2000	2000	1200 1600 1800 2000 2500*	10000 15000 20000 30000
к-3000	3000	1600 2000 2500 3000 3800*	10000 20000 28000 36000
K-4000	4000	2000 3000 3500 4000 5000*	20000 30000 40000 48000

① Refer to Table 57 for application parameters.

Setting above maximum breaker frame size is available for coordination, if needed, but is not thermally self-protecting.

# POWER-SHIELD \* —SOLID-STATE TRIP DEVICE

rigure 11—General Purpose (SS-3) Time-Current Characteristics

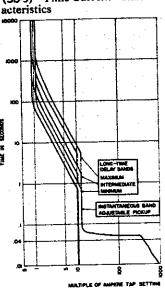


Figure 12 — Dual Selective (SS-4 and SS-5) Time-Cur-

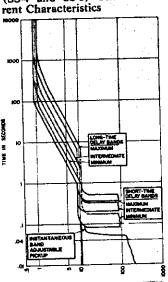


Figure 13 — Ground Time-Current Characteristics

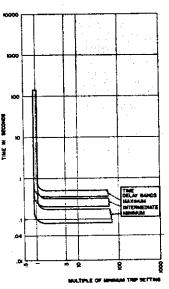


Figure 14—General Purpose (SS-13) Time-Current Characteristics (special)

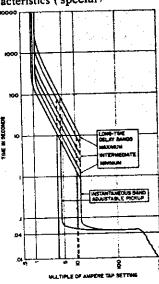


TABLE 61 — STANDARD TYPES

Type	Designation	Trip Functions
SS-3: SS-4: SS-5:	General Purpose Dual Selective Triple Selective	Long-time; Instantaneous Long-time; Short-time Long-time; Short-time; Instantaneous
SS-3G SS-4G SS-5G		Same as SS-3, with Ground (3- or 4-wire) Same as SS-4, with Ground (3- or 4-wire) Same as SS-5, with Ground (3- or 4-wire)

Special longer long-time delays (SS-13, SS-14, SS-15) are also available for special coordination.

TABLE 63 - TIME-DELAY CHARACTERISTICS

Trip Function	Time-Delay Band	Time Delay
Long-Time *	Maximum Intermediate Minimum	15 seconds† 5 seconds† 2 seconds†
Short-Time	Maximum Intermediate Minimum	0.35 seconds§ (21 cycles) 0.20 seconds§ (12 cycles) 0.08 seconds§ (4.8 cycles)
Instantaneous	Maximum Intermediate Minimum	No Intentional Delay
Ground	Maximum Intermediate Minimum	0.35 seconds§ (21 cycles) 0.20 seconds§ (12 cycles) 0.08 seconds§ (4.8 cycles)

<sup>†</sup> Measured at six (6) times ampere-tap setting and at the lower limit of maximum, intermediate or minimum long-time time delay bands.

• Special long-times for SS-13,-14 and-15 are 30, 10 and 4 seconds.

# TABLE 62 — PHASE AMPERE TAP AND GROUND PICK-UP RANGES

5 W 19 (1) 19 1		Available	~~~~	Pick-Up	Ranget	COLUMN SERVICES
Circuit Breaker Type		Ampere Tap	Long- Time	Short- Time npere Tap	instan- taneous	Ground Amperes
7-25 2.36		Sattings, A	IIII ES AI	uhere 14h	Setung	
K-600S		50 70 100 150 225	0.7 0.8 0.9 1.0 1.1*	2 3 4 6 8	4 5 6 8 10 12	100 300 600
		250 400 600	1.1	10 10	10 12	1200
		250 400 600	0.7 0.8 0.9	2 3 4 6 8 10	4 5 6 8 10	100 300 600 1200
K-1600S	lange	600 1000 1600	00		10 12	300 600 900 1200
K-2000S	Sensor Range	800 1200 2000	0.7 0.8 0.9 1.0 1.1*	2 3 4 6 8 10	4 5 6 8 10 12	300 600 900 1200
K-3000S	1	2000 3000	0.7 0.8 0.9 1.0 1.1*	2 3 4 6 8 10	5 6 8 10 12	500 800 1000 1200
K-4000S		3000 4000	0.7 0.8 0.9 1.0 1.1*	2 3 4 6 8 10	4 5 6 8 10 12	500 800 1000 1200

<sup>\*</sup> Setting above maximum ampere tap rating and breaker frame size is available for coordination, if needed, but is not thermally self-protecting.

<sup>§</sup> Measured at the lower limit of maximum, intermediate, or minimum short-time and ground time delay bands at any point above pick-up.

<sup>†</sup> The tolerance on all calibrated pick-up settings for long-time, short-time, instantaneous and ground functions is ±10% through the temperature range of -20°C to 55°C.

# GROUND-SHIELD® GROUND-FAULT PROTECTION APPLICATION

### HME-CURRENT CHARACTERISTICS

The time-current curves shown in Figures 15 & 16 are designed to provide maximum protection against ground faults with minimum disturbance to unfaulted circuits. Use GR-5 relay for all individual loads (such as motors and transformers) and for high-resistance grounded systems. Use GR-200 relay for main, feeder and branch circuits on solidly or low-resistance ground systems.

#### INTERRUPTER TYPES

Common interrupting devices which can be used with ground-fault relays are (1) high-voltage power circuit breakers, (2) low-voltage power circuit breakers, (3) molded-case circuit breakers, (4) service protectors, (5) contactors, and (6) certain load-break, switch-fuse combinations. First, care should be taken to insure that the switch interrupting rating is sufficient to handle ground faults of all magnitudes which would be cleared faster than the associated fuse maximum clearing curve. Also, it is necessary that the interrupter switch be equipped with a fast shunt-tripping mechanism and ability to interrupt the ground fault within several cycles from energization of trip coil. Circuit breaker and fuse combinations equipped with shunt-trip coils are well adapted to the GROUND-SHIELD Protection System.

### BASIC NEED FOR GROUND-SHIELD

The basic need for ground-fault protection in low-voltage systems is illustrated in Figure 17. Shown is a 1000 kVA service ransformer with a 1600-ampere main breaker (with typical ng-time and short-time characteristics) and fuse. A 1500A ground fault (Point I) on the 480Y/277 grounded neutral system would not be detected by this breaker. A 4000A ground fault (Point II) could persist for about 33 seconds even if the

minimum long-time band were used. An 8,000 ampere ground fault (Point III) would be cleared within about .2 to .4 seconds by the short-time device, assuming it is present, otherwise, between 8 to 20 seconds would elapse before the fault is cleared. For the assumed 8,000A fault, even though the current values are the calculated result using all source, circuit and arc impedances, the actual RMS current values passing through the circuit breaker can be considerably lower. This is because of the spasmodic nature of the fault caused by (1) arc elongating blow-out effects, (2) physical flexing of cables and some bus structures due to mechanical stresses, (3) self-clearing attempts and arc re-ignition, and (4) shifting of the arc terminals from point to point on the grounded enclosure (as well as on the faulted conductors for non-insulated construction). All of these effects tend to reduce the RMS value of fault currents. Figure 17 also illustrates that a ground fault which would normally produce 8,000A under stabilized conditions and which results in an effective value of only 4000A (Point II) would have a max. clearing time of 33 seconds instead of the normally expected max. of .4 seconds.

Other fault interrupting devices such as fuses (Note from Figure 17 that a 1600A fuse takes 5 minutes to clear a 4000A fault) which have far slower operating times as low fault currents, have even a greater need for supplementary ground-fault protection. Most of these devices have time-current characteristics which delay tripping for about 100 seconds for fault currents 200% to 300% of normal continuous-current rating.

Note the interrupting time for a curve C, GR-200 relay would be about .2 seconds on a 4000 ampere ground fault and less than .4 seconds on a 1500 ampere ground fault.

GROUND-SHIELD ground fault sensing and relaying

GROUND-SHIELD ground fault sensing and relaying equipment is UL listed.

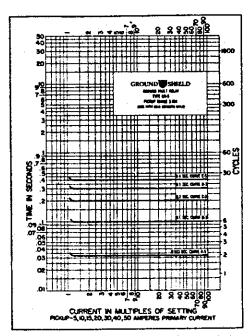


Figure 15—GR-5 Time-Current Characteristics and ard pick-up range, 5-50A
Optional pick-up range, 2-40A or 20-200A

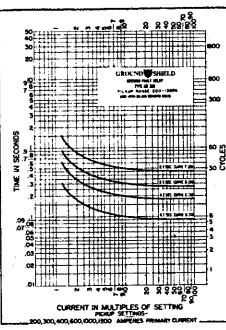


Figure 16—GR-200 Time-Current Characteristics Standard pick-up range, 200-1200A Optional pick-up range, 120-1200A

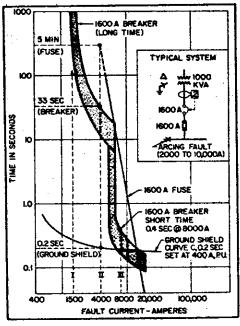


Figure 17—Ground-Shield System Coordination Curves

# MOLDED-CASE CIRCUIT BREAKERS

MOLDED-CASE BREAKER RATINGS

Max. Amperes C Max. Voltage	DED-CASE BREAKE Circuit Breaker Frame	Current Continuous	A-C Volts	Maximum Interrupting Rating Sym. Rms Amperes	3-Pole Circuit Breaker (not including mounting) Size, inches
100 Amp	EH†	15–150	240 480	18,000 14,000	W 4½ H 6 D 3½
480 Volt	EF†	15–100	240 480 600	18,000 14,000 14,000	W 4½ H 6 D 3½
100 Amp	HE†	15–100	240 480 600	65,000 25,000 18,000	W 4½ H 6 D 3½
600 Volt	CE† Cordon	15-100	240 480 600	200,000 200,000 100,000	W 4½ H 9 D 4%s
225 Amp	FJ†	70–225	240 480 600	22,000 18,000 14,000	W 4½ H 10 D 4½
600 Volt	nt.	250-400	240 480 600	42,000 30,000 22,000	W 9 H 11 D 4½6
	JL*	70–400	240 480 600	42,000 30,000 22,000	W 9 H 11 D 41/6
400 Amp 600 Volt	нл	125-400	240 480 600	65,000 35,000 25,000	W 9 H 11 D 41/16
	CJ Cordon	125-400	240 480 600	200,000 200,000 100,000	W 9 H 15%6 D 5%6
<u> </u>	LL	450-600	240 480 600	42,000 30,000 22,000	W 9 H 11 D 41/4
450-600 Amp 600 Volt	HL	450-600	240 480 600	65,000 35,000 25,000	W 9 H 11 D 41/6
	км	250-800	240 480 600	42,000 30,000 22,000	W 9 H 15½ D 4½
800 Amp 600 Volt	нм	400-800	240 480 600	65,000 35,000 25,000	W 9 H 22 D 53/4
300 1011	CM Cordon	400-800	240 480 600	200,000 200,000 100,000	W 9 H 26 <sup>2</sup> % <sub>2</sub> D 6 <sup>7</sup> / <sub>8</sub> W 9
1200 Amp 600 Volt	КР	600-1200	240 480 600	42,000 30,000 22,000	H 15½ D 4¾
1200 Amp 600 Volt	нк	700-1200	240 480 600	65,000 50,000 42,000	H 15½ D 4¾
300 1010	HP	600–1600	240 480 600	65,000 50,000 42,000	W 9 H 15½ D 4¾
1600 Amp 600 Volt	CP Cordon	600-1600	240 480 600	200,000 200,000 100,000	W 9 H 211/16 D 43/4
	HR	1800-2000	240 480 600	65,000 50,000 42,000	W 9 H 15½ D 4¾
2000 Amp 600 Volt	CR Cordon	1800-2000	240 480 600	200,000 200,000 100,000	W 9 H 21%6 D 43%

Non-interchangeable trip.

70, 90 and 100 ampere breakers have interrupting ratings of 30,000 amperes asymmetrical, 25,000 amperes symmetrical at 240 volts ac; 25,000 amperes

TABLE 65A
LOW-VOLTAGE POWER CIRCUIT BREAKER APPLICATION — 208 VOLTS

Transfermer Rating, 3-ph NYA	frieury	Herma)		Short-Coronit Correst Total	100		<u>akar Recommended</u>	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
and importance Per Cont	System Max, Short- Circuit sys	Continues Current, A	Transformer Alone	Symmetrical Ampa Mater Loads	Combined	Main Breaker	Feeder with	Feeder with 22 Selection Trip
112.5 2.25%§	50,000 100,000 150,000 250,000 500,000 Unlimited	312	13,160 13,480 13,640 13,760 13,840 13,870	600	13,770 14,080 14,240 14,330 14,440 14,470	K-600 K-600S	K-225 K-600S	K-225 K-600\$
150 3.00%§	50,000 100,000 150,000 250,000 500,000 Unlimited	416	11,280 11,580 11,640 11,820 12,000 13,870	800	12,080 12,380 12,440 12,620 12,800 14,670	K-600 K-600\$	K-225 K-600S	K-225 K-600S
225 4.5%	50,000 100,000 150,000 250,000 500,000	625	12,640 13,120 13,360 13,600 13,760	1200	13,840 14,320 14,560 14,800 14,960	K-1600 K-1600S	K-225 K-600S	K-225 K-600\$
300 5.0%	Unlimited 50,000 100,000 150,000 250,000 500,000 Unlimited	834	13,890 14,880 15,680 16,000 16,240 16,400 16,680	1700	15,090 16,580 17,380 17,700 17,940 18,100 18,380	K-1600 K-1600S	K-225 K-600S	K-600S K-600S
500 5.0%	50,000 100,000 150,000 250,000 500,000 Unlimited	1388	23,120 25,200 26,000 26,640 27,200 27,760	2800	25,920 28,000 28,800 29,440 30,000 30,560	K-1600 K-1600S †	K-600 K-600S	K-1600 K-1600S
750 5.75%	50,000 100,000 150,000 250,000 500.000 Unlimited	2080	28,640 32,000 33,360 34,400 35,280 36,170	4200	32,840 36,200 37,560 38,600 39,480 40,370	K-3000 K-3000S	K-600 K-600S	K-1600 K-1600S
1000 5.75%	50,000 100,000 150,000 250,000 500,000 Unlimited	2780	35,840 41,120 43,360 45,200 46,720 48,350	5600	41,440 46,720 48,960 50,880 52,320 53,950	K-3000 K-3000S	K-600 K-600S K-1600 K-1600S	K-1600 K-1600S

TABLE 65B

240 VOLTS

112.5 2.25%§	50,000 100,000 150,000 250,000 500,000 Unlimited	271	9,600 11,680 11,840 11,920 12,020 12,050	1100	10,700 12,780 12,940 13,020 13,120 13,150	K-600 K-600S	K-225 K-600S	K-225 K-600S
150 3.00%§	50,000 100,000 150,000 250,000 500,000 Unlimited	361	11,280 11,460 11,650 11,800 11,910 12,030	1400	12,680 12,860 13,050 13,200 13,310 13,430	K-600 K-600S	K-225 K-600\$	K-225 K-600S
225 4.5%	50,000 100,000 150,000 250,000 500,000 Unlimited	541	10,930 11,460 11,630 11,790 11,990 12,020	2200	13,130 13,660 13,830 13,990 14,190 14,220	K-500 K-600S †	K-225 K-600\$	K-225 K-600S K-600 K-600S
300 5.0%	50,000 100,000 150,000 250,000 500,000 Unlimited	722	12,880 13,600 13,920 14,080 14,320 14,440	2900	15,780 16,500 16,820 16,980 17,220 17,340	K-1600 K-1600S	K-225 K-600S	K-1600 K-1600S
500 5.0%	50,000 100,000 150,000 250,000 500,000 Unlimited	1203	20,080 21,840 22,560 23,120 23,600 24,060	4800	24,880 26,640 27,360 27,920 28,400 28,860	K-1600 K-1600S	K-225 K-600S K-600 K-600S	K-1600 K-1600S
750 5.75%	50,000 100,000 150,000 250,000 500,000 Unlimited	1804	24,960 27,760 28,880 29,920 30,640 31,380	7200	32,160 34,960 36,080 37,120 37,840 38,580	K-2000 K-2000S †	K-600 K-600S	K-1600 K-1600S
1000 5.75%	50,000 100,000 150,000 250,000 500,000 Unlimited	2406	31,120 35,680 37,520 39,120 41,360 41,840	9600	40,720 45,280 47,120 48,720 50,960 51,440	K-3000 K-3000S	K-600 K-600S K-1600 K-1600S	K-1600 K-1600S

<sup>\*§21</sup> See Page 49 for note references

# SYSTEM APPLICATION

TABLE 66 - LOW-VOLTAGE POWER CIRCUIT BREAKER APPLICATION - 480 VOLTS

71 x - 1 2 2 2 2 2 2			12 6 15 ME 31 31 35	Current Tales	Service Service Services	San San Strain	CONTRACTOR CONTRACTOR	Serge om 12 of 1960 Store of 1960
Transformer	Primery System	ternet Less		MS Symmetrical Ampere		· 2000年8月1	a de selo mar e	等於法 医心肠
ating, 3-ph NVA and Imperiment Per Cent	Max. Shert- Circuit 174	Centine MeS Carrest, A	Franciscours Aless	100% Meter Lead	Combined	Main Breaker	Feeder with Instant. Trip	Fooder with Telestive Trip
12.5 2.25%§	50,000 100,000 150,000 250,000 500,000	135	5,720 5,840 5,880 5,960 6,000	500	6,220 6,340 6,380 6,460 6,500	K-225 K-600S	K-225 K-600S	K-225 K-600S
150 3.0%§	50,000 100,000 150,000 250,000 500,000	180	5,400 5,790 5,865 5,895 5,955 6,000	700	6,100 6,490 6,565 6,595 6,655 6,700	K-225 K-600S	K-225 K-600S	K-225 K-600S
225 4.5% \( \)	Unlimited 50,000 100,000 150,000 250,000 500,000	271	5,460 5,720 5,800 5,900 5,960 6,020	1100	6,560 6,820 6,900 7,000 7,060 7,120	K-600 K-600\$	K-225 K-600S	K-225 K-600S
300 5.0%	50,000 100,000 150,000 250,000 500,000	361	6,480 6,800 6,960 7,040 7,120 7,220	1400	7,880 8,200 8,360 8,440 8,520 8,620	K-600 K-600S	K-225 K-600S	K-225 K-600S
500 5.0%	Unlimited 50,000 100,000 150,000 250,000	601	10,000 10,960 11,280 11,600	2400	12,400 13,360 13,680 14,000 14,240	K-1600 K-1600S	K-225 K-600S	K-225 K-600S
0.070	500,000 Unlimited		11,840 12,020		14,420		K-600	or K-600S
750 5.75%	50,000 100,000 150,000 250,000 500,000	902	12,400 13,840 14,480 14,960 15,360 15,690	3600	16,000 17,440 18,080 18,560 18,960 19,290	K-1600 K-1600S	K-225 K-600S	K-600S
	Unlimited 50,000		15,600		20,400 22,720		K-225 K-600	K-600, \$
1000 5.75%	100,000 150,000 250,000 500,000	1203	17,920 18,800 19,600 20,240 20,920	4800	23,600 24,400 25,040 25,720	K-1600S	K-600 K-600S	K-1600 K-1600S
1000	50,000 100,000 150,000 250,000 500,000	1203	12,030 13,350 13,980 14,315 14,555 15,040	4800	16,830 18,150 18,750 19,115 19,355 19,840	K-1600 K-1600S	K-225 K-600S	K-600 K-600S
	Unlimited 50,000		20,640		27,840 32,160		K-600, \$	٠
1500 5.75%	100,000 150,000 250,000 500,000 Unlimited	1804	24,960 26,800 28,480 29,840 31,370	7200	34,000 35,680 37,040 38,570	K-2000 K-2000s †	K-1600 K-1600S	K-1600 K-16009
2000 5.75%	50,000 100,000 150,000 250,000 500,000	2406	24,720 30,560 34,080 36,720 38,960 41,840	9600	34,320 40,160 43,680 46,320 48,560 51,440	K-3000\$	K-1600 K-1600S	
	Untimited 50,000		27,900		39,900 48,300		K-1600 K-1600S	K-1600 K-1600
2500 5.75%	100,000 150,000 250,000 500,000	3010	36,300 40,400 44,500 48,100	12000	52,400 56,500 62,100 64,350	K-4000 K-4000S	K-2000 K-2000 K-2000\$	K-3000 K-3000

<sup>\*§‡†</sup> See Page 49 for note references.

## SELECTION AND APPLICATION

# FABLE 67 — LOW-VOLTAGE POWER CIRCUIT BREAKER APPLICATION — 600 VOLTS

Transfermen	Primary	lene i		Short-Circuit Current Tatal	( ) ( ) ( ) ( ) ( )	~~.	imum Framo Size Air Chr Breater Recommonded	
Transfermer Bation, 3-ph NA and Impadance Per Cent	System Mar. Short Circuit 174	Leat Coatinoper Current, A		ANTE CONTRACTOR OF CO.				
		and the second second	Transfermer Alone	Hotor Load	Combined	Mole Breaker	Feeder with Instant, Trip	Freder with Selective Trip
112.5 2.25%§	50,000 100,000 150,000 250,000 500,000 Unlimited	108	4,580 4,680 4,720 4,760 4,780 4,800	400	4,980 5,080 5,120 5,160 5,180 5,200	K-225 K-600\$	K-225 K-600S	K-225 K-600S
150 3.00%§	50,000 100,000 150,000 250,000 500,000 Unlimited	144	4,500 4,650 4,695 4,740 4,770 4,800	600	5,100 5,250 5,295 5,340 5,370 5,400	K-225 K-600\$	K-225 K-600S	K-225 K-600S
225 4.5%	50,000 100,000 150,000 250,000 500,000 Unlimited	217	4,380 4,590 4,670 4,730 4,770 4,820	900	5,280 5,490 5,570 5,630 5,670 5,720	K-225 K-600S †	K-225 K-600\$	K-225 K-600S
300 5.0%	50,000 100,000 150,000 250,000 500,000 Unlimited	289	5,160 5,450 5,560 5,640 5,710 5,780	1200	6,360 6,650 6,760 6,840 6,910 6,980	K-600 K-600S	K-225 K-600S	K-225 K-600S
500 5.0%	50,000 100,000 150,000 250,000 500,000 Unlimited	481	8,020 8,740 9,020 9,250 9,430 9,620	1900	9,920 10,640 10,920 11,150 11,330 11,520	K-600 K-600S	K-225 K-600S	K-225 K-600S
50 5.75%	50,000 100,000 150,000 250,000 500,000 Unlimited	722	9,960 11,110 11,550 11,930 12,240 12,560	2900	12,860 14,010 14,450 14,830 15,140 15,460	K-1600 K-1600S	K-225 K-600S	K-225 K-600S
	50,000		12,410 14,250		16,210 18,050		K-225	or K-600S
1000 5.75%	100,000 150,000 250,000 500,000 Unlimited	962	14,980 15,640 16,170 16,730	3800	18,780 19,440 19,970 20,530	K-1600 K-1600S	K-600 K-600S	K-1600 K-1600S
1500 5.75%	50,000 100,000 150,000 250,000 500,000 Unlimited	1444	16,500 19,920 21,390 22,740 23,870 25,110	5800	22,300 25,720 27,190 28,540 29,670 30,910	K-2000 K-2000\$	K-1600 K-1600S	K-600 K-600s
2000 5.75%	50,000 100,000 150,000 250,000 500,000 Unlimited	1924	19,730 24,830 27,180 29,370 31,280 33,630	7700	27,430 32,530 34,880 37,070 38,980 41,330	K-2000 K-2000S	K-1600 K-1600S	K-600 K-600S
2500 5.75%	50,000 100,000 150,000 250,000 500,000 Unlimited	2406	22,380 29,160 32,430 35,640 38,500 41,840	9600	31,980 38,760 42,030 45,240 48,100 51,440	K-3000 K-3000\$	K-1600 K-1600S K-2000 K-2000S	K-1600 K-1600S K-2000 K-2000S

<sup>\*</sup> The transformer main secondary breakers are in most cases determined by continuous current instead of fault current. For this reason breakers in the M column are usually larger than those listed in the I column. The values listed in the M column allow a breaker continuous rating approximately 25% above the transformer self-cooled full-load current. If the transformer has a fan cooled rating a main secondary breaker larger than indicated by column M may be required.

<sup>§</sup> Short-circuit currents are calculated with impedances shown applying to liquid-immersed transformers only. Refer to Table 39, Page 34, for ventilated-dry type impedances.

Motor load contribution for 208 volts is based on 50%. 240 volt application table is based on 100% motor load contribution.

<sup>†</sup> These circuit breakers are applied at less than 25% above transformer full-load rating. If 25% is required, use the next larger frame size.

# SHORT-CIRCUIT CURRENTS IN LOW-VOLTAGE SYSTEMS

To determine the interrupting-capacity requirements of low-voltage, air-magnetic power circuit breakers it is necessary to obtain information, at the point of application, of the short-circuit condition of every part of a distribution system. A set of 32 curves (available on request) provides a graphical means of determining the value of short-circuit currents and the corresponding power factor for various sizes of transformers and various voltages, in combination with different sizes and lengths of cable. In Table 70 is given the multiplying factor to use in obtaining the asymmetrical values of current at different power factors.

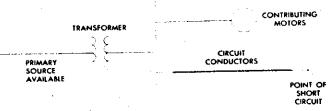


Figure 18

In the study diagrammed above, these basic characteristics are assumed:

- 1. Primary source available is 500 MVA at the primary of the transformer, with a source circuit X/R ratio of 25.
- 2. Transformer kVA covers a range of six standard sizes; 500, 750, 1000, 1500, 2000, 2500.
- 3. Distribution voltages of 208, 240, 480, and 600 v are assumed; 3-phase, 60 Hertz.
- 4. Minimum transformer impedances are 5.0% up through 500 kVA and 5.75% for 750 kVA and higher, less the standard allowable tolerance of -7½%. X/R ratios are selected from typical data furnished by several transformer manufacturers from which the characteristics in Table 68 (following) are calculated. The data is based on liquid-immersed, self-cooled transformers. Dry-type transformers generally have higher resistance, and the results of this study should be conservative for systems in which they are used.
- 5. Motor impedance is based on an equivalent reactance of 25 and an X/R ratio of 6.
- 6. Feeder conductors chosen are at least 115% of the size normally required for the standard frame sizes of low-voltage, air-magnetic power circuit breakers. Calculations in this study are based on 3-phase conductors, of minimum insulation thickness, in magnetic ducts. Table 69 gives the conductor sizes and alternate arrangements for which this study can be used.
- 7. Short-circuit duty can be read direct from the set of 32 curves. The short-circuit current available, in symmetrical amperes, and the corresponding short-circuit power factor are shown for any distance, in circuit feet, from the terminals of the transformer up to 5000 ft. These values include the current contributed by the connected motors.
- 8. Asymmetrical short-circuit currents, if desired, can be found from the symmetrical values above by using a multiplying factor read from Figure 19 and corresponding to the short-circuit power factor at the point of fault. Use the multiplying factor from Curve M<sub>A</sub> to find the average 3-phase asymmetrical amperes and Curve M<sub>M</sub> to find the

- maximum asymmetrical amperes in one phase with the greatest possible offset. For accurate values of  $M_A$  and  $M_M$ , use the values in Table 70.
- 9. Short-circuit current at the terminals of transformers may be determined from Table 71. This gives the symmetrical rms amperes, the 3-phase average asymmetrical rms amperes, and the maximum obtainable asymmetrical rms amperes in one phase at the terminals.

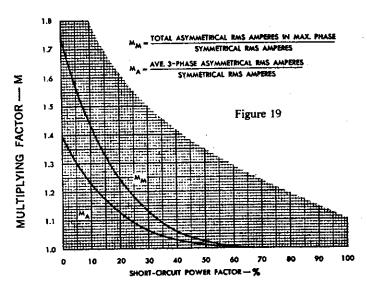
TABLE 68 — TRANSFORMER CHARACTERISTICS

Transformer Rating kVA	X/R	R (%)	X (%)	Z{%} *
500	3.4	1.3	4.4	4.5
750	3.9	1.3	5.1	5.3
1000	4.2	1.2	5.1	5.3
1500	5.2	1.0	5.2	5.3
2000	6.1	.85	5.2	5,3
2500	6.5	.80	5.2	5.3

Minimum value takes impedance tolerance into account.

TABLE 69 - CIRCUIT CONDUCTORS

Circuit Rating Amperes	Conductor Size	Conductor Insulation	Alternate Conductor Sizes
50	# 4 AWG	Type R	
100	# 0 AWG	Type R	
225	250 MCM	Type RH	
400	2-250 MCM	Type RH	<u> </u>
600	2-500 MCM	Type RH	3-# 4/0 AWG
600	2-500 MCM	Type RH	4-# 2/0 AWG
1600	4-750 MCM	Type RH	3-2000 MCM
1600	4-750 MCM	Type RH	5-400 MCM
1600	4-750 MCM	Type RH	6-300 MCM



Multiplying Factors to obtain short-circult asymmetrical current from symmetrical values, at an instant ½ cycle (60 cycle basis) after initiation of a fault.

TABLE 70 - SHORT-CIRCUIT MULTIPLYING FACTORS

CA COME.		Multiply	ing Factor			Meltiply	ag Factor
Short-Circuit Power Factor Per Cent	Short Circuit X/R Ratio	Maximum 1-Phase RMS Ampères at Ya Cycle (Curve M.)	Average 3-Phase RMS Amperes at 1/2 Cycle (Curve M.)	Short-Circuit Power Factor Per Cent	Short Circuit X/R Ratio	Maximum 1-Phase RMS Amperes at: 1/2 Cycle (Curve Max	Average 3-Phase RMS Amperes at 1/2 Cycle (Curve M.)
0	00	1.732	1.394	29	3.3001	1.139	1.070
1	100.00	1.696	1.374	30	3.1798	1.130	1.066
2	49.993	1.665	1.355	31	3.0669	1.121	1.062
3	33.322	1.630	1.336	32	2.9608	1.113	1.057
4	24.979	1.598	1.318	33	2.8606	1.105	1.053
5	19.974	1.568	1.301	34	2.7660	1.098	1.049
6	16.623	1.540	1.285	35	2.6764	1.091	1.046
7	14.251	1.511	1.270	36	2.5916	1.084	1.043
8	12.460	1.485	1.256	37	2.5109	1.078	1.039
8.5	11.723	1.473	1.248	38	2.4341	1.073	1.036
9	11.066	1.460	1.241	39	2.3611	1.068	1.033
10	9.9501	1.436	1.229	40	2.2913	1.062	1.031
11	9.0354	1.413	1.216	41	2.2246	1.057	1.028
12	8.2733	1.391	1.204	42	2.1608	1.053	1.026
13	7.6271	1.372	1.193	43	2.0996	1.049	1.024
14	7.0721	1.350	1.182	44	2.0409	1.045	1.022
15	6.5912	1.330	1.171	45	1.9845	1.041	1.020
16	6.1695	1.312	1.161	46	1.9303	1.038	1.019
17	5.7967	1.294	1.152	47	1.8780	1.034	1.017
18	5.4649	1.277	1.143	48	1.8277	1.031	1.016
19	5.1672	1.262	1.135	49	1.7791	1.029	1.014
20	4.8990	1.247	1.127	50	1.7321	1.026	1.013
21	4.6557	1.232	1.119	55	1.5185	1.015	1.008
22	4.4341	1.218	1.112	60	1.3333	1.009	1.004
23	4.2313	1.205	1.105	65	1.1691	1.004	1.002
24	4.0450	1.192	1.099	70	1.0202	1.002	1.001
25	3.8730	1.181	1.093	75	0.8819	1.0008	1.0004
26	3.7138	1.170	1.087	80	0.7500	1.0002	1.00005
27	3.5661	1.159	1.081	85	0.6198	1.00004	1.00002
28	3.4286	1.149	1.075	100	0.0000	1.00000	1.00000

# GUIDE SPECIFICATIONS FOR SECONDARY UNIT SUBSTATIONS

NOTE: Blue color and italics denotes information to be supplied by purchaser regarding either:  Choice of alternates Addition of optional features Specific information	OIL FUSE CUTOUTS  This section shall consist of 3-gang-operated oil fuse cutouts, mounted in an air-filled terminal chamber directly connected to the transformer tank wall. Cut-outs are to be 2-position and rated amperes continuous at kV.
SCOPE These specifications cover a complete (indoor) (outdoor) secondary unit substation from the incoming line terminals to the outgoing feeder terminals.	size cable to enter from (above) (below) and terminate in clamp-type lugs per phase or (1-5/C) (2-3/C) (3-1/C) (6-1/C) pothead(s), Pothead(s) to be provided with fitting for cables with following specifications: kV size, insulation, O.D. over insulation, O.D. conductor, O.D. overall.
SECTIONS  The substation will have the following sections:  1. Incoming line section with ( ) incoming primary circuit(s).  2. Transforming section consisting of ( ) transformer(s).  3. Outgoing section which will provide for ( ) outgoing feeders provided with low-voltage power circuit breaker(s).  GENERAL ARRANGEMENT  The accompanying sketch No	AIR TERMINAL CHAMBER  This section shall consist of a full-height air terminal chamber directly connected to the high-voltage side of the transformer. It shall be rated kV. size cable to enter from tabove) (below) and terminate in clamp-type lugs per phase or (1.5/C) (2.3/C) (3.1/C) (6.1/C) pothead(s). Pothead(s) to be provided with fitting for cables with the following specifications: kV size, insulation, O.D. over insulation, O.D. conductor, O.D. overall.
RATINGS The ratings of the substation will be: Self-Cooled ratingkVA	METAL-CLAD SWITCHGEAR
Fan-Cooled rating	( )—Metal-clad switchgear unit.  ( )—(4.16) (7.2) (13.8) kV air circuit breaker, amp, 3-pole, electrically-operated, stored-energy.  State Control Voltage Requirements.
( ) outgoing (3) (4)-wire circuit(s)volts INCOMING LINE SECTION	( )—Set of insulated main bus, amp.
(2-POSITION, ON-OFF) (3-POSITION, LINE 1-OFF-LINE 2) (FUSED) (UNFUSED) AIR INTERRUPTER SWITCH(ES)	Current transformers,
This section shall consist of a floor-mounted, formed welded metal enclosure close-coupled to the transformer section and equipped with:	( )—Breaker control switch with red and green indicating lights.
<ul> <li>( ) —3-pole, 2-position, gang-operated, load-interrupter switch, type HPL-C, rated 600 amperes, kV, interrupting capacity 600 amperes.</li> <li>( ) —3-pole, 2-position selector switch, interlocked and in series with the air interrupter switch.</li> </ul>	( )—Ammeter, 0 scale. ( )—Ammeter transfer switch.
()—Power fuses, current-limiting type CL-14 kV, amperes continuous, to be located between the switch and the transformer. The fuse door to be inter- locked with the switch handle to prevent opening while the switch is in the closed position.	<ul> <li>( )—Voltmeter.</li> <li>( )—Voltmeter transfer switch.</li> <li>( )—Drawout potential transformers, ————— -120 volt ratio.</li> </ul>
( )—Lightning arresters rated (3) (6) (9) (12) (15) kV.  size cable to enter from (above) (below) and terminate in	size cable to enter from (above) (below) and terminate in clamp-type lugs per phase or (1-3 °C) (2-3/C) (3-1/C) (6-1/C) pothead(s). Pothead(s) to be provided with fitting for cables with the following specifications: kV size, insulation, O.D. over insulation, O.D. conductor, O.D. overall.
overall.  LIQUID (INTERRUPTER) (DISCONNECT) SWITCH(ES)	TRANSFORMER SECTION LIQUID-IMMERSED TYPES (OIL) (ASKAREL)— (OA) (OA/FA)
This section shall consist of non-fused, oil-insulated, load-interrupter switch, mounted on transformer tank. This switch to be 3-pole (2) (5) -position device rated amperes continuous at kV.	Transformer shall be (Oil) (Askarel)-insulated, 3-phase, 60 Hertz, (self-cooled) (forced-air cooled) with a temperature rating not to exceed a 65°C rise above 30°C average ambient.
This section shall consist of non-fused, askarel-insulated, disconnecting switch, mounted on transformer tank. The switch shall be capable of breaking transformer magnetizing current and the askarel shall be of the type designed for this operation. This switch to be 3-pole (2) (5) -position device rated amperes continuous at kV.	RatedkVA, with delta primary ofkV and a secondary ofvolts (Delta) (Wye). Provide four (4) approximately 2½% full capacity taps in the high-voltage winding, two above and two below normal, brought out to an externally-operated, deenergized tap changer. Tap changer handle to be capable of being locked in any tap position.
size cable to enter from (above) (below) and terminate in (1-5/C) (2-5/C) (3-1/C) (6-1/C) pothead(s). Pothead(s) to be provided with fitting cables with the following specifi-	Transformer base construction to be of the fabricated type and suitable for using rollers or skidding in any direction.
cations: kV size, insulation, O.D. over insulation, O.D. conductor, O.D. overall.	Transformer to be factory tested as prescribed by ANSI and NEMA Standards. All NEMA standard accessories are to be provided.

VENTILATED-DRY TYPE—(AA) (AA/FA)  Transformer shall be a ventilated-dry type, indoor construction, 3-phase, 60 Hertz, (self-cooled) (forced-air cooled) with a tempera- ture rating not to exceed a 150°C rise above 30°C average ambient.
Rated kVA, with a delta primary of kV and a secondary of volts (Delta) (Wye). Provide four (4) approximately 2½% full capacity taps in the high-voltage winding, two above and two below normal, brought out through studs, complete with bolted flexible links for deenergized tap-changing operation, made accessible through a removable panel on the transformer enclosure.
Transformer base construction to be of the fabricated type and suitable for using rollers or skidding in any direction.
Transformer to be factory tested as prescribed by ANSI and NEMA standards. All NEMA standard accessories are to be provided.
Necessary winding-temperature equipment for control of fans.
Shall have provision for future fan cooling.
SEALED-DRY, GAS-FILLED—TYPE AA Transformer shall be sealed-dry type, gas-filled, 3-phase, 60 Hertz, self-cooled, with a temperature rating not to exceed a 150°C rise above a 30°C average ambient.
Rated kVA, with a delta primary of kV and a secondary of volts (Delta) (Wye). Provide four (4) approximately 2½% full capacity taps in the high-voltage winding, two above and two below normal, brought out to an externally-operated, deenergized tap changer. Tap changer cover to be capable of being bolted in any tap position.
Transformer base construction to be of the fabricated type and suitable for using rollers or skidding in any direction.
Transformer to be factory tested as prescribed by ANSI and NEMA Standards. All NEMA standard accessories are to be provided.
OUTGOING SECTION  This section shall consist of one metal-enclosed (indoor) (outdoor) switchgear assembly, drawout type, rated 600 V a-c and arranged for volt service on a volt 3-phase (3) (4)-wire (grounded) (ungrounded) system. It shall be designed, factory assembled and tested in accordance with the latest applicable IEEE, NEMA, and ANSI requirements.
SWITCHGEAR (indoor) (outdoor)  Switchgear shall consist of sufficient vertical frames to house the number of circuits specified below, with a minimum number of empty spaces remaining. Each individual frame shall be divided into a front breaker section and a rear bus section isolated by steel panels. In addition, each circuit-breaker compartment shall be

### SWITCHGEAR (outdoor only)

be light gray, ANSI No. 61.

Switchgear shall be of the walk-in weatherproof type with gasketing throughout. Sufficient filtered louvers and screened vents shall be provided to afford adequate ventilation. Sufficient strip heaters shall be provided. Interior lighting and convenience outlets shall be furnished in the aisle space. A manually-operated lifting device running the full length of the walk-in aisle shall be provided for easy handling of breakers. Suitable undercoating shall be applied to prevent corrosion. All exterior surfaces shall receive one additional finish coat of oven baked, corrosion-resistant acrylic enamel paint. The color of the finish coat shall be dark gray, ANSI No. 24.

completely isolated from adjacent compartment by steel panels. All surfaces shall be phosphate treated and painted with an oven baked, corrosion-resistant epoxy enamel finish. Color of finish shall

#### BUS

A single main bus shall extend through all frames of the switchboard, with interconnections to the circuit breakers in each individual frame. All bus shall be silver-plated aluminum. The main bus shall be of the same current rating as the main circuit breaker or the power source. It shall be braced to withstand stresses resulting from the maximum short-circuit current available. Minimum bracing to be 50,000 amperes symmetrical.

# DISCONNECTING DEVICES & DRAWOUT MECHANISM

The breakers shall be of the drawout type, provided with self-aligning disconnecting devices, with the disconnecting fingers mounted on the breaker for ease of maintenance. The drawout mechanism shall hold the circuit breaker rigidly in the fully-connected, test and fully-disconnected positions. Interlocks shall be provided that will prevent moving the circuit breaker from the fully-connected, test or fully-disconnected positions, unless the breaker is open. Interlocks shall prevent closing the breaker between any of these positions. Provision shall be made for padlocking the breaker open and in any of the positions noted above.

#### CIRCUIT BREAKERS

Air circuit breakers shall be three pole, each pole equipped with a (electro-mechanical direct-acting) (solid-state) overcurrent tripping device providing adjustable long-time overcurrent and (short-time) and/ortinstantaneous) short-circuit protection (with) (with-out) ground protection. Solid-state device shall have (boad alarm) (target). All (manually) (electrically) operated breakers shall be equipped with (manual) (motor) charged stored-energy closing mechanism to provide quick-make operation.

The drawout mechanism shall be designed so that the breaker can be racked to any position without opening the door, for maximum protection to operating personnel. A hasp on the breaker escutcheon shall be provided that can receive up to three padlocks when the breaker is in the open position, positively preventing unauthorized closing or racking of the breaker. A manual trip button and external breaker position indicator shall be provided. THE FOLLOWING EQUIPMENT SHALL BE SUPPLIED:

main secondary breaker(s), amp maximum
V ac, (manually) (electrically) operated.
tie breaker(s), amp maximum continuous
current, amp interrupting capacity at V ac, (manually) (electrically) operated.
feeder breaker(s), amp maximum continuous
current amp interrupting capacity at v ac,
(manually) (electrically) operated.
feeder breaker(s), amp maximum continuous current, amp interrupting capacity at V ac, (manually) (electrically) operated.
space(s) for future breaker(s), maximum con-
tinuous current, amp interrupting capacity at V ac, (manually) (electrically) operated.
control-power transformer(s) for electrically operated breaker(s).
TRANSFORMER SECONDARY METERING
voltmeter (s), with 3-phase transfer switch.
ammeter with 3-phase transfer switch.
waithour meter(s), (two) (three)-element, (with) (without) demand attachment.
current transformer(s),/5 or suitable rating.
potential transformer(s), suitable rating.
FEEDER METERING
ammeter(s), with 3-phase transfer switch.
watthour meter(s), (two) (three) element.
current transformer(s),/5 or suitable rating.

#### BUS DUCT—Switchgear Tie

Bus shall be non-segregated phase, metal-enclosed (indoor) (out-door), rated 600 Volts \_\_\_\_\_\_ amperes, 3-phase, (3) (4)-wire, 60 Hertz and shall consist of silver-plated aluminum conductors, insulated supports and housing.